

Malarkey IND
Stormwater Management
3540 Essex Drive
Franklin, Indiana

Drainage Memorandum

Prepared For:
Cooper & Associates
2200 Ellis Drive
New Lenox, IL 60451

Prepared By:
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Original: October 10th, 2024

Kimley»Horn

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1.0. Project Summary

| | |
|-----------------------|---|
| Project Name: | Malarkey IND – Final Buildout |
| Location: | 3540 Essex Drive, Franklin, Johnson County, Indiana |
| Type: | Drainage Memorandum |
| Reviewing Agency: | City of Franklin & Johnson County |
| Storm Sewer Modeling: | Storm and Sanitary Analysis (SSA), Rational Method |
| Receiving Body: | Graham Arm |

2.0. Introduction

Kimley-Horn and Associates, Inc. has been retained by Cooper & Associates LLC to prepare construction documents and provide civil engineering services for the proposed industrial development for Malarkey Roofing Products as the Owner and end user (Project). The Project includes the development of approximately 138 acres of agricultural land to the north and west of Essex Drive in Franklin, Indiana. The Project includes the planned construction of an approximately 357,600 SF industrial building with associated drives, parking, rail spur, and substantial outdoor product storage spaces. The Project also includes a 4,110 LF roadway extension of Essex Drive, connecting to Paul Hand Blvd. The extension will become the east frontage of the Malarkey site and will include sanitary sewer and water main extensions along with three entrances. A 90' right of way will be dedicated to the City for Essex Drive. Utility services will be brought from extended infrastructure off Essex Drive and Paul Hand Blvd where applicable. Stormwater detention and quality measures will be provided in the form of an interconnected wet & dry detention ponds at the east and south sides of the site. The Project will be broken down into two phases: the first being the mass grading and pond excavation, and the second being the final buildout and Essex Drive extension.

This Drainage Memorandum focuses on the final buildout condition by confirming assumptions made during the mass grading phase and presenting storm sizing based on the City of Franklin Stormwater Management Ordinance and Johnson County Stormwater Technical Standards Manual (Version 1.0 - 2023), whichever is more stringent.

3.0. Existing Conditions

The site is a combination of Basin 1, Basin 2 and Basin 3 as described by the master planned drainage report submitted concurrently with the mass grading phase. Per the drainage report, each basin was assumed to be a curve number (CN) of 95 and have a time of concentration (TC) of 10 minutes. In addition, there will be significant off-site drainage entering the site from the north through a 12" culvert under Paul Hand. The 12" culvert is also planned to be replaced with a 4'x3' box culvert which has already been factored in accordingly in terms of inline capacity. Several excerpts are included in **Appendix D**. The full Drainage Report can be found in **Appendix G**.

Aerial Photograph

An aerial photograph of the Project Site has been included in **Appendix A** for reference.

FEMA

The Project Site is located on the Flood Insurance Rate Map number 18081C0139E (dated 1/29/2021) and 18081C0137D (date 8/2/2007) concluded that the site lies in Zone X which is the area of minimal flood hazard and outside the 100-Yr Flood Hazard zones. See **Appendix B** for the FEMA FIRMette.

Soil Characteristics

The Natural Resources Conservation Service (NRCS) Web Soil Survey of Johnson County, Indiana, indicates Brookston silty clay loam and Crosby silt loam on site. A soil map can be found in **Appendix C**.

4.0. Proposed Conditions

Proposed Hydrology

The developed site will maintain the master planned drainage assumptions set forth in the master drainage report. Each on-site basin was assumed to have a curve number (CN) of 95 and a time of concentration (TC) of 10 minutes. As shown in the Proposed Curve Number Exhibit, the calculated composite CN of each basin, when factoring in the proposed impervious and pervious areas, is summarized in the table below. Note that some areas within the basins have been deferred to future developments however are assumed in full buildout condition in this report. Ultimately, this development meets the intention of the master plan, and no additional measures are required. See table below for a summary of calculated values. Refer to Appendix E for the Curve Number Exhibit and accompanying calculations.

| | Acreage (AC) | Composite Curve Number (C) | Time of Concentration (TC) in minutes |
|----------------|-------------------------|---------------------------------------|--|
| Basin 1 | 47.48 | 95 | 10.7 |
| Basin 2 | 11.23 | 87 | 10.4 |
| Basin 3 | 74.10 | 93 | 10.4 |

Proposed Hydraulics

The proposed storm sewer conveyance system was designed to meet the City requirements using Storm and Sanitary Analysis (SSA), an extension of Civil 3D. The HGL of the 10-year storm was kept below the proposed rim elevations of each structure. Rainfall intensities and 'c' values are to be taken from the City of Franklin Stormwater Management Ordinance. The storm sewers are to be designed to maintain a minimum full flow velocity of 2.5 ft/s. See Appendix G for calculations.

Stormwater Quality

Stormwater quality treatment for the project site has already been accounted for as part of the interconnected detention pond design. See the drainage report in Appendix XX.

5.0 Appendices

Appendix A: Aerial Photograph



Appendix B: FEMA Flood Insurance Rate Map

NOTES TO USERS

This map is for use in administering the National Flood Insurance Program. It does not necessarily identify all areas subject to flooding, particularly from local drainage sources of small size. The community map repository should be consulted for possible updated or additional flood hazard information.

To obtain more detailed information in areas where Base Flood Elevations (BFEs) and/or floodways have been determined, users are encouraged to consult the Flood Profiles and Floodway Data and/or Summary of Stillwater Elevations tables contained within the Flood Insurance Study (FIS) Report that accompanies this FIRM. Users should be aware that BFEs shown on the FIRM represent rounded whole-foot elevations. These BFEs are intended for flood insurance rating purposes only and should not be used as the sole source of flood elevation information. Accordingly, flood elevation data presented in the FIS Report should be utilized in conjunction with the FIRM for purposes of construction and/or floodplain management.

Boundaries of the floodways were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway widths and other pertinent floodway data are provided in the Flood Insurance Study Report for this jurisdiction.

Certain areas not in Special Flood Hazard Areas may be protected by flood control structures. Refer to Section 2.4 "Flood Protection Measures" of the Flood Insurance Study Report for information on flood control structures for this jurisdiction.

The projection used in the preparation of this map was Indiana State Plane East Zone FIPS zone 1301. The horizontal datum was NAD 83, GRS 1980 ellipsoid. Differences in datum, spheroid, projection or UTM zones used in the production of FIRMs for adjacent jurisdictions may result in slight positional differences in map features across jurisdiction boundaries. These differences do not affect the accuracy of this FIRM.

Flood elevations on this map are referenced to the North American Vertical Datum of 1988. These flood elevations must be compared to structure and ground elevations referenced to the same vertical datum. For information regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1988, visit the National Geodetic Survey website at <http://www.ngs.noaa.gov> or contact the National Geodetic Survey at the following address:

NGS Information Services
NOAA/NGS12
National Geodetic Survey
SSMC-3, #9202
1315 East-West Highway
Silver Spring, Maryland 20910-3262
(301) 713-3242

To obtain current elevation, description, and/or location information for bench marks shown on this map, please contact the Information Services Branch of the National Geodetic Survey at (301) 713-3242, or visit its website at <http://www.ngs.noaa.gov>.

Base map information shown on this FIRM was derived from the 2005 Indiana Orthophotography (IndianaMap Framework Data www.indianemap.org). This information was photogrammetrically compiled at a scale of 1:2400 from aerial photography dated spring 2005. Aerial Photography shown on the FIRM is from 2018 provided by Johnson County.

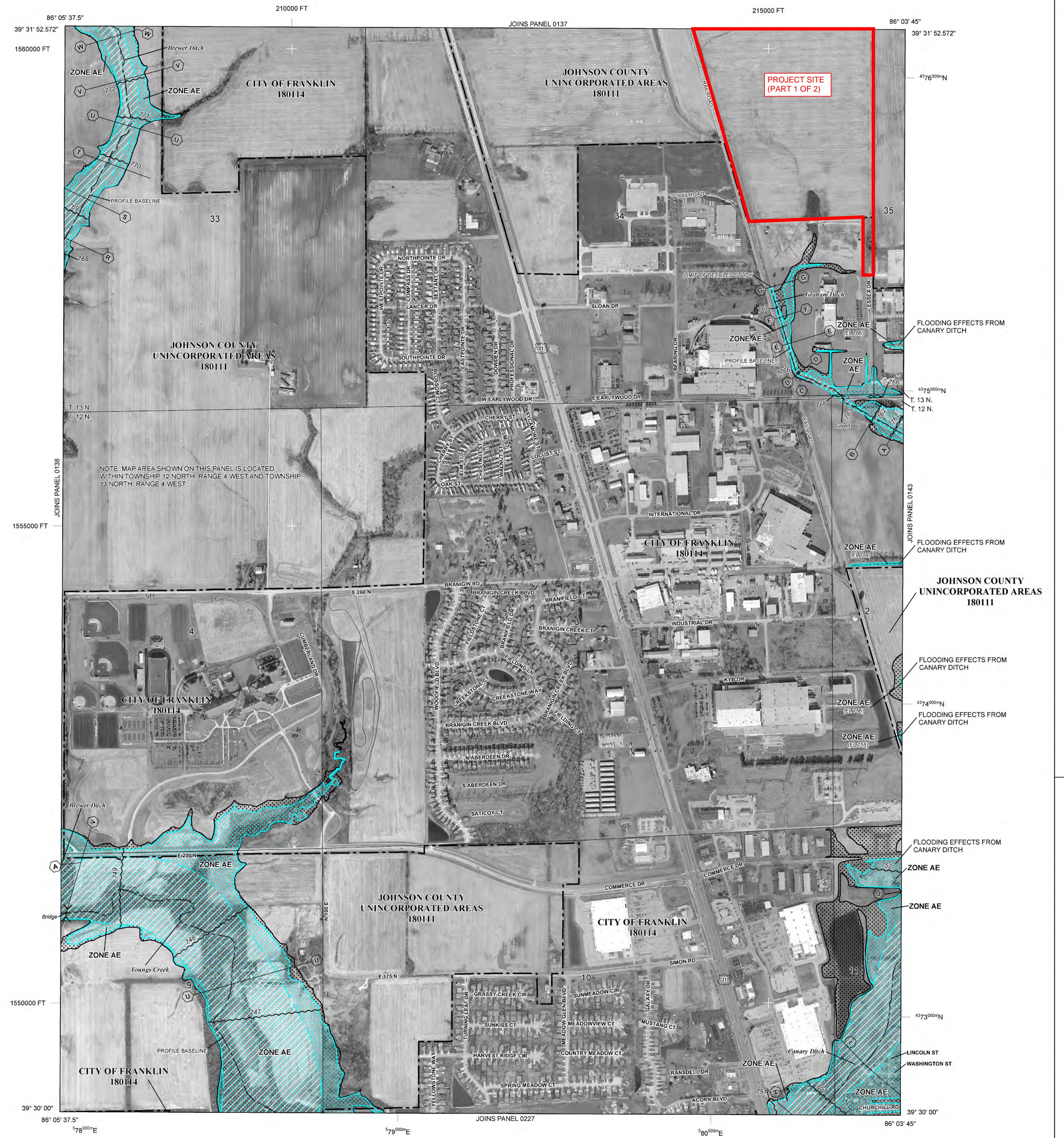
The profile baselines depicted on this map represent the hydraulic modeling baselines that match the flood profiles in the FIS report. As a result of improved topographic data, the profile baseline, in some cases, may deviate significantly from the channel centerline or appear outside the SFHA.

Corporate limits shown on this map are based on the best data available at the time of publication. Because changes due to annexations or de-annexations may have occurred after this map was published, map users should contact appropriate community officials to verify current corporate limit locations.

Please refer to the separately printed Map Index for an overview map of the county showing the layout of map panels; community map repository addresses; and a listing of communities table containing National Flood Insurance Program dates for each community as well as a listing of the panels on which each community is located.

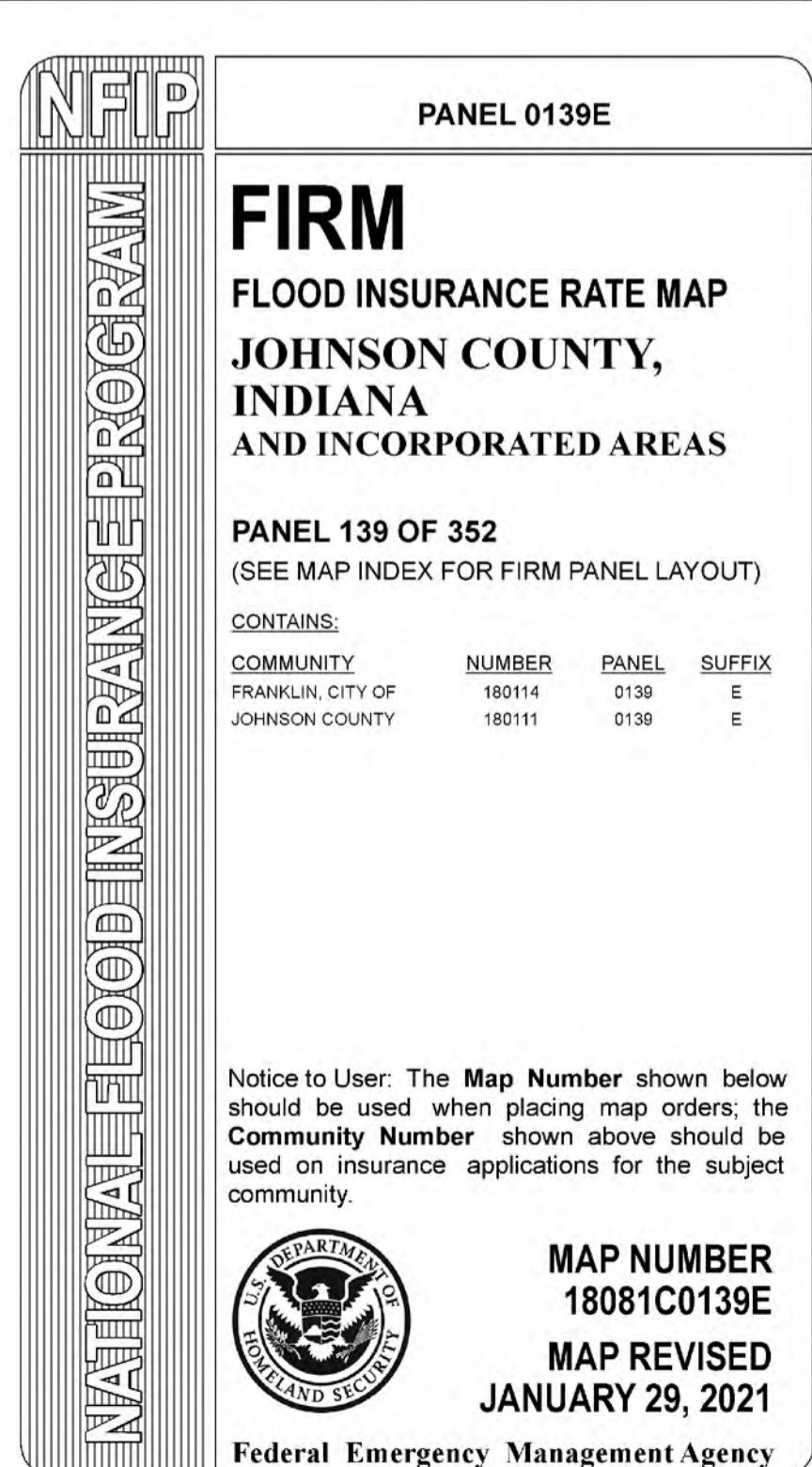
For information on available products associated with this FIRM visit the Map Service Center (MSC) website at <http://msc.fema.gov>. Available products may include previously issued Letters of Map Change, a Flood Insurance Study Report, and/or digital versions of this map. Many of these products can be ordered or obtained directly from the MSC website.

If you have questions about this map, how to order products, or the National Flood Insurance Program in general, please call the FEMA Map Information eXchange (FMIX) at 1-877-FEMA-MAP (1-877-336-2627) or visit the FEMA website at <http://www.fema.gov/business/nfip>.



LEGEND

| | |
|--|---|
| | SPECIAL FLOOD HAZARD AREAS (SFHAs) SUBJECT TO INUNDATION BY THE 1% ANNUAL CHANCE FLOOD |
| | The 1% annual chance flood (100-year flood), also known as the base flood, is the flood that has a 1% chance of being equaled or exceeded in any given year. The Special Flood Hazard Area is the area subject to flooding by the 1% annual chance flood. Areas of Special Flood Hazard include Zones A, AE, AH, AO, AR, A99, V, and VE. The Base Flood Elevation is the water-surface elevation of the 1% annual chance flood. |
| | ZONE A No Base Flood Elevation determined. |
| | ZONE AE Base Flood Elevation determined. |
| | ZONE AH Flood depths of 1 to 3 feet (usually areas of ponding); Base Flood Elevation determined. |
| | ZONE AO Flood depths of 1 to 3 feet (usually sheet flow on sloping terrain); average depths determined. For areas of alluvial fan flooding, velocities also determined. |
| | ZONE AR Special Flood Hazard Areas formerly protected from the 1% annual chance flood by a flood control system that was subsequently decertified. Zone AR indicates that the former flood control system is being restored to provide protection from the 1% annual chance or greater flood. |
| | ZONE A99 Area to be protected from 1% annual chance flood by a Federal flood protection system under construction, no Base Flood Elevation determined. |
| | ZONE V Coastal flood zone with velocity hazard (wave action); no Base Flood Elevation determined. |
| | ZONE VE Coastal flood zone with velocity hazard (wave action); Base Flood Elevation determined. |
| | FLOODWAY AREAS IN ZONE AE |
| | OTHER FLOOD AREAS |
| | ZONE X Areas of 0.2% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 foot or drainage areas less than 1 square mile; and areas protected by levees from 1% annual chance flood. |
| | ZONE X OTHER AREAS Areas determined to be outside the 0.2% annual chance floodplain. |
| | ZONE D COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS |
| | OTHERWISE PROTECTED AREAS (OPAs) |
| | CBRS areas and OPAs are normally located within or adjacent to Special Flood Hazard Areas. |
| | 1% Annual Chance Floodplain Boundary |
| | Floodway boundary |
| | Zone D boundary |
| | CBRS and OPA boundary |
| | Boundary dividing Special Flood Hazard Area Zones and boundary dividing Special Flood Hazard Areas of different Base Flood Elevations, flood depths, or flood velocities. |
| | Base Flood Elevation line and value; elevation in feet* |
| | *Referenced to the North American Vertical Datum of 1988 |
| | Cross section line |
| | Transect line |
| | Culvert |
| | Bridge |
| | Geographic coordinates referenced to the North American Datum of 1983 (NAD 83) Western Hemisphere |
| | 500-foot ticks; Indiana State Plane East Zone |
| | 3100000 FT 489000m N |
| | 1000-meter Universal Transverse Mercator grid values, zone 16 |
| | DX5510 M1.5 |
| | River Mile |
| | MAP REPOSITORIES Refer to Map Repositories list on Map Index |
| | EFFECTIVE DATE OF COUNTYWIDE FLOOD INSURANCE RATE MAP August 2, 2007 |
| | EFFECTIVE DATE(S) OF REVISION(S) TO THIS PANEL January 29, 2021 - to increase Base Flood Elevations and to change Special Flood Hazard Areas. |



NOTES TO USERS

This map is for use in administering the National Flood Insurance Program. It does not necessarily identify all areas subject to flooding, particularly from local drainage sources of small size. The community map repository should be consulted for possible updated or additional flood hazard information.

To obtain more detailed information in areas where Base Flood Elevations (BFEs) and/or floodways have been determined, users are encouraged to consult the Flood Profiles and Floodway Data and/or Summary of Stillwater Elevation tables contained within the Flood Insurance Study (FIS) report that accompanies this FIRM. Users should be aware that BFEs shown on the FIRM represent rounded whole-foot elevations. These BFEs are intended for flood insurance purposes and should not be used as the sole source of flood elevation information. Accordingly, flood elevation data presented in the FIS report should be utilized in conjunction with the FIRM for purposes of construction and/or floodplain management.

Coastal Base Flood Elevations: shown on this map apply only landward of 0' North American Vertical Datum of 1988 (NAVD 88). Users of this FIRM should be aware that coastal flood elevations are also provided in the Summary of Stillwater Elevation table in the Flood Insurance Study report for this jurisdiction. Elevation shown in the Summary of Stillwater Elevation table should be used for construction and/or floodplain management purposes when they are higher than the elevations shown on this FISM.

Boundaries of the floodways were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway widths and other pertinent floodway data are provided in the Flood Insurance Study report for this jurisdiction.

Certain areas not in Special Flood Hazard Areas may be protected by flood control structures. Refer to Section 2.4 "Flood Protection Measures" of the Flood Insurance Study report for information on flood control structures for this jurisdiction.

The projection used in the preparation of this map was Indiana State Plane East zone 3826 (FIPSZONE 1301). The horizontal datum was NAD83. Differences in datum, spheroid, projection or state plane zones used in the production of FIRMs for adjacent jurisdictions may result in slight positional differences in map features across jurisdiction boundaries. These differences do not affect the accuracy of this FISM.

Flood elevations on this map are referred to the North American Vertical Datum of 1988. These flood elevations must be compared to structure and ground elevations referenced to the same vertical datum. For information regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1988, visit the National Geodetic Survey website at <http://www.ngs.noaa.gov/> or contact the National Geodetic Survey at the following address:

NGS Information Services
NOAA, NINGIS2
National Geodetic Survey
SSMC-3, #9202
1315 East-West Highway
Silver Spring, Maryland 20910-3282
(301) 713-3242

To obtain current elevation, description, and/or location information for bench marks shown on this map, please contact the Information Services Branch of the National Geodetic Survey at (301) 713-3242, or visit its website at <http://www.ngs.noaa.gov/>.

Base Map information shown on this FISM was derived from the Johnson County Computer Services from photography dated 2001 and from USGS digital orthophoto quadrangles dated 1998 or later.

This map reflects more detailed and up-to-date stream channel configurations than those shown on the previous FISM for this jurisdiction. The floodplains and floodways that were transferred from the previous FISM may have been adjusted to conform to these new stream channel configurations. As a result, the Flood Profiles and Floodway Data tables in the Flood Insurance Study report (which contains authoritative hydraulic data) may reflect stream channel distances that differ from what is shown on this map.

Corporate limits shown on this map are based on the best data available at the time of publication. Because changes due to annexations or de-annexations may have occurred after this map was published, map users should contact appropriate community officials to verify current corporate limit locations.

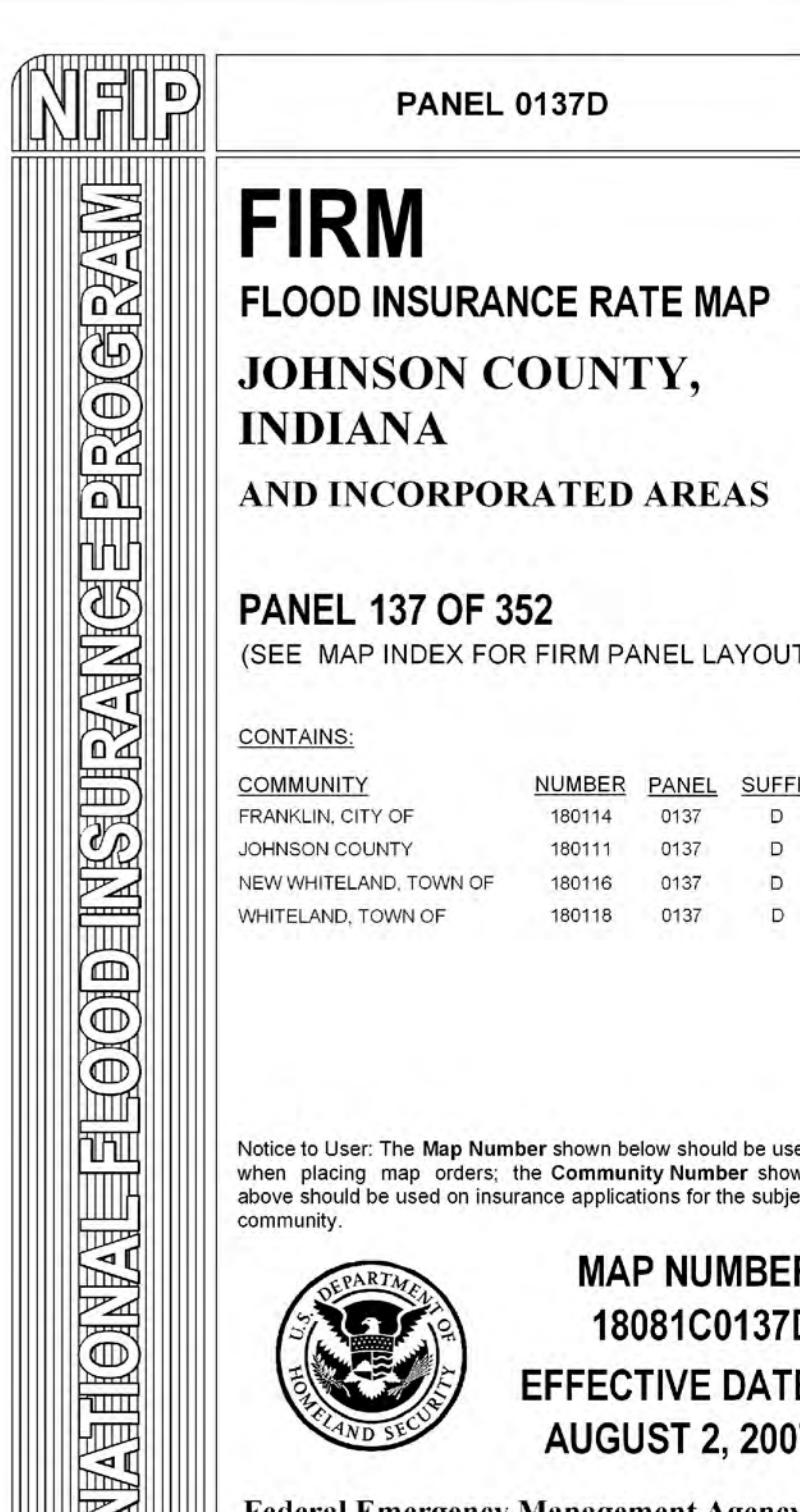
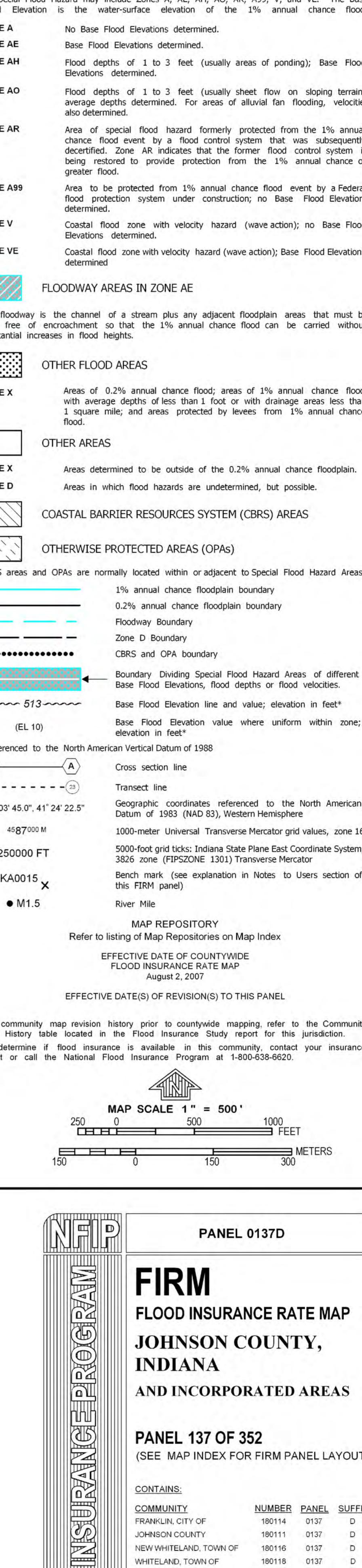
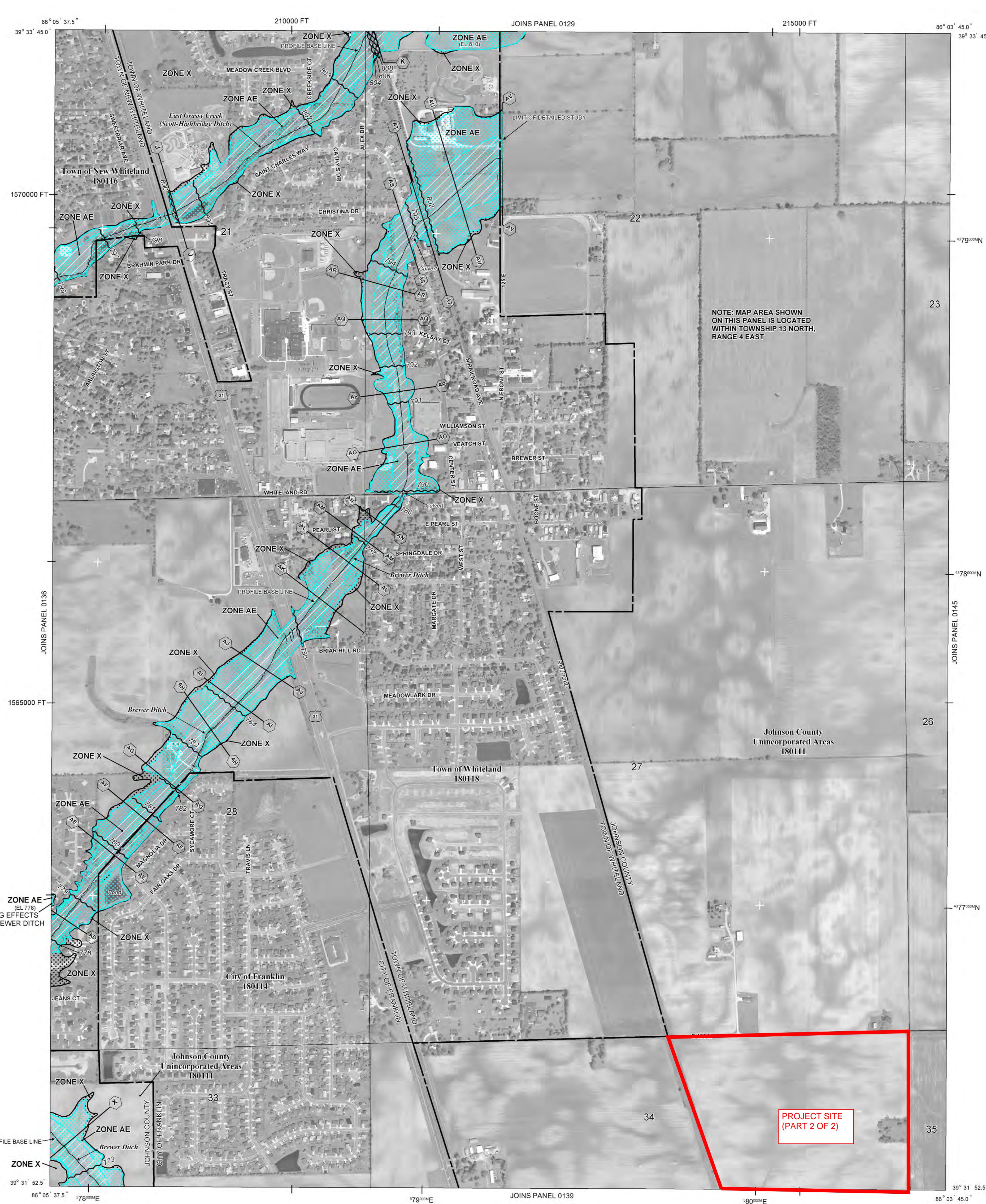
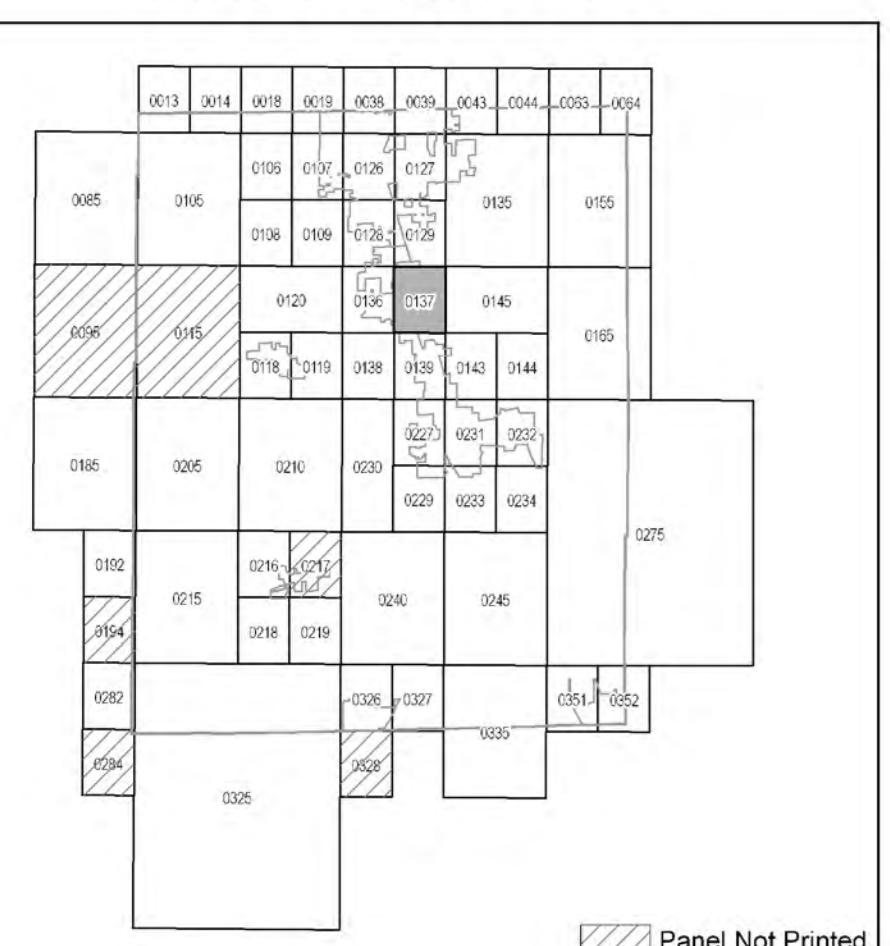
Please refer to the separately printed Map Index for an overview map of the county showing the layout of map panels, community map repository addresses, and a listing of communities, table containing National Flood Insurance Program dates for each community as well as a listing of the panels on which each community is located.

Contact the FEMA Map Service Center at 1-800-358-9616 for information on available products associated with this FISM. Available products may include previously issued Letters of Map Change, a Flood Insurance Study report, and/or digital versions of this map. The FEMA Map Service Center may also be reached by Fax at 1-800-358-9620 and its website at <http://msc.fema.gov/>.

If you have questions about this map or questions concerning the National Flood Insurance Program in general, please call 1-877-FEMA MAP (1-877-336-2627) or visit the FEMA website at <http://www.fema.gov/business/nfip/>.

The profile base lines depicted on this map represent the hydraulic modeling baselines that match the flood profiles in the FIS report. As a result of improved topographic data, the profile base line, in some cases, may deviate significantly from the channel centerline or appear outside the SFHA.

PANEL INDEX

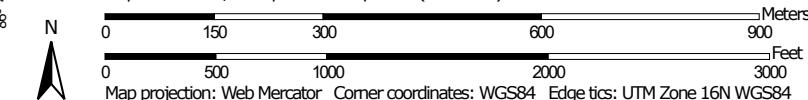


Appendix C: Soil Map

Hydrologic Soil Group—Johnson County, Indiana



Map Scale: 1:10,400 if printed on A portrait (8.5" x 11") sheet.



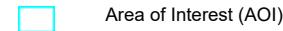
Map projection: Web Mercator Corner coordinates: WGS84 Edge tics: UTM Zone 16N WGS84



Natural Resources
Conservation Service

Web Soil Survey
National Cooperative Soil Survey

7/30/2024
Page 1 of 4

MAP LEGEND**Area of Interest (AOI)****Soils****Soil Rating Polygons**

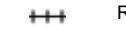
| | |
|--|----------------------------|
| | A |
| | A/D |
| | B |
| | B/D |
| | C |
| | C/D |
| | D |
| | Not rated or not available |

Soil Rating Lines

| | |
|--|----------------------------|
| | A |
| | A/D |
| | B |
| | B/D |
| | C |
| | C/D |
| | D |
| | Not rated or not available |

Soil Rating Points

| | |
|--|-----|
| | A |
| | A/D |
| | B |
| | B/D |

C**C/D****D****Not rated or not available****Water Features****Streams and Canals****Transportation****Rails****Interstate Highways****US Routes****Major Roads****Local Roads****Background****Aerial Photography****MAP INFORMATION**

The soil surveys that comprise your AOI were mapped at 1:15,800.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service

Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Johnson County, Indiana

Survey Area Data: Version 31, Sep 1, 2023

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Jun 15, 2022—Jun 21, 2022

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.



Hydrologic Soil Group

| Map unit symbol | Map unit name | Rating | Acres in AOI | Percent of AOI |
|------------------------------------|--|--------|--------------|----------------|
| Br | Brookston silty clay loam, 0 to 2 percent slopes | B/D | 99.8 | 38.5% |
| CrA | Crosby silt loam, fine-loamy subsoil, 0 to 2 percent slopes | C/D | 110.0 | 42.5% |
| CsB2 | Crosby-Miami silt loams, 2 to 4 percent slopes, eroded | C/D | 11.7 | 4.5% |
| FxC2 | Fox complex, 6 to 12 percent slopes, eroded | B | 7.3 | 2.8% |
| MnB2 | Miami silt loam, 2 to 6 percent slopes, eroded | C | 22.3 | 8.6% |
| YclA | Crosby silt loam, fine-loamy subsoil-Urban land complex, 0 to 2 percent slopes | C/D | 7.9 | 3.0% |
| Totals for Area of Interest | | | 259.0 | 100.0% |

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition

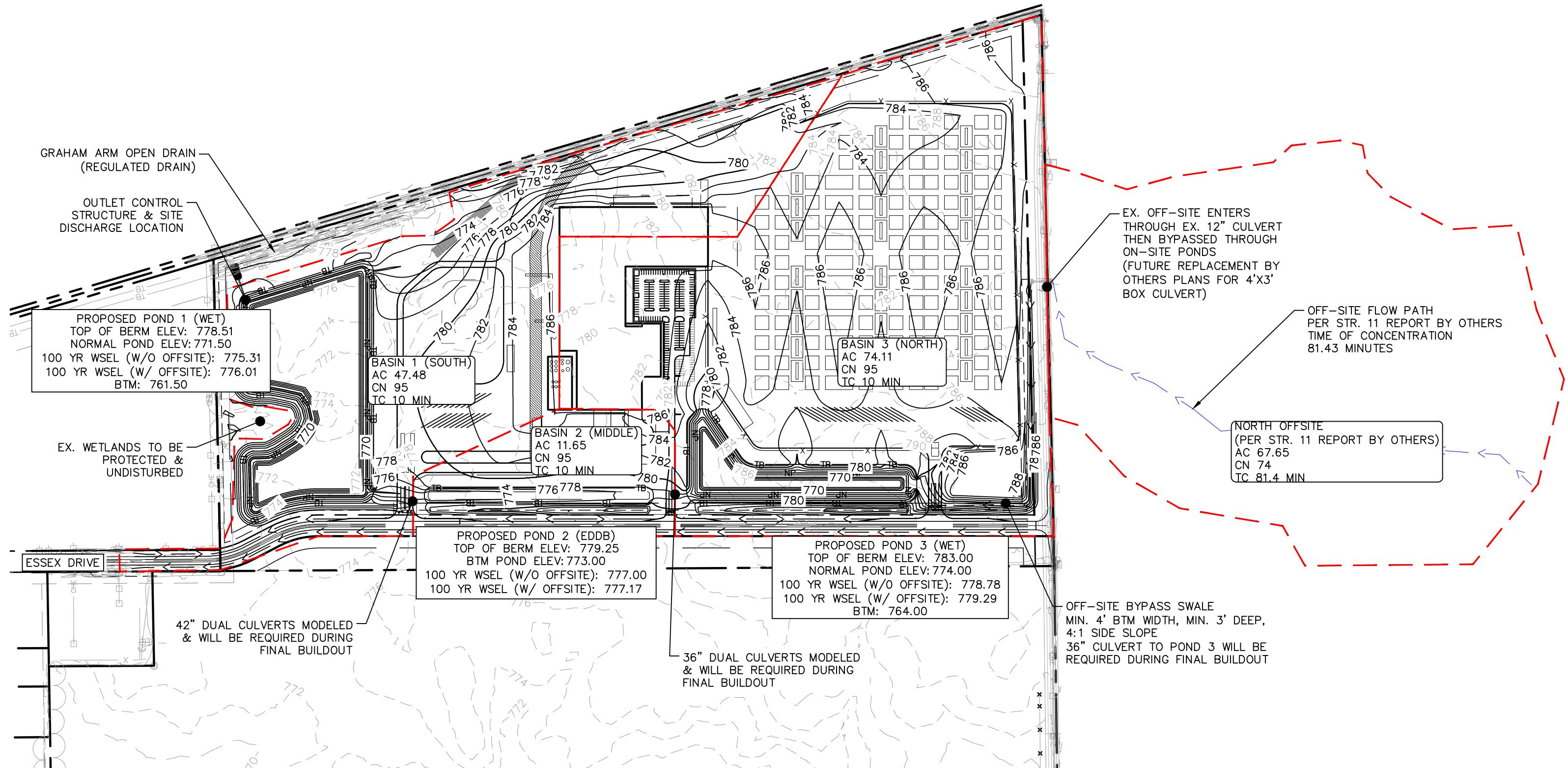
Component Percent Cutoff: None Specified

Tie-break Rule: Higher

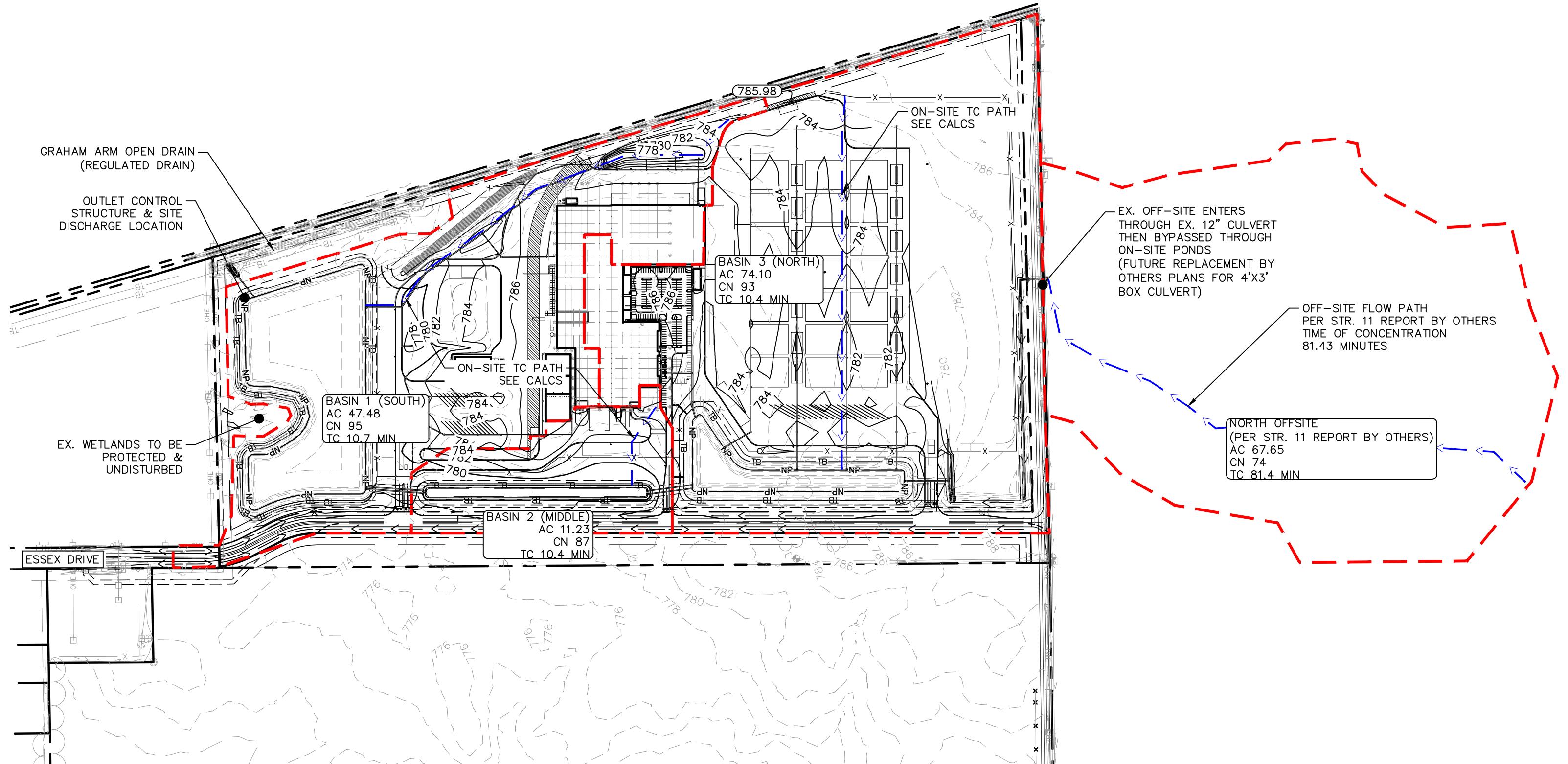
Appendix D: Master Plan Map

NOTES:

1. SCHEMATIC SITE LAYOUT IS SHOWN FOR DRAINAGE MASTER PLANNING PURPOSES ONLY. FINAL LAYOUT IS SUBJECT TO CHANGE.
2. PROPOSED GRADING CONTOURS SHOWN ARE FOR MASS GRADING PURPOSES. IT IS THE INTENTION TO REPLACE INTERIM SWALES CONNECTING PONDS WITH EQUALIZING CULVERTS PROPERLY SIZED TO CONVEY DRAINAGE AS PRESENT IN THIS DRAINAGE REPORT.
3. 2' & 10' CONTOUR INTERVALS SHOWN FOR CLARITY
4. OFF-SITE CONTOURS/ACREAGE ARE FROM LIDAR RECORDS



Appendix E: Curve Number Exhibit



Kimley»Horn

| | |
|----------|--------------|
| PROJECT: | Malarkey IND |
| BY: | AMM |
| DATE: | 10-Oct-24 |

| Site Soil | | |
|------------------|--------|-------|
| Hydrologic Group | % | |
| A | 0.0% | 0.0% |
| B | 0.0% | 11.2% |
| C | 0.0% | 30.7% |
| D | 100.0% | 58.1% |
| Total | 100.0% | |

| Cover | Type | Condition | Soil Group Weighted Runoff Coefficient | Soil Group Weighted CN | |
|-----------------|--------------|-----------------------------|--|------------------------|---------------------------------|
| | | | C | Actual Soil Group | Next Less Impervious Soil Group |
| Fully Developed | Impervious | Paved | 0.85 | 98 | 98 |
| Fully Developed | Impervious | Rooftop | 0.90 | 98 | 98 |
| Fully Developed | Open Space | Good Condition (>75% Cover) | 0.30 | 80 | 80 |
| Water | Pond or Lake | - | 1.00 | 100 | 100 |

| Basin | Area (ac) | | | | | Weighted C | Weighted CN | Weighted CN |
|---------|--------------------|----------------------|--|--------------|-------|------------|-------------------|---------------------------------|
| | Impervious - Paved | Impervious - Rooftop | Open Space - Good Condition (>75% Cover) | Pond or Lake | Total | | Actual Soil Group | Next Less Impervious Soil Group |
| Basin 1 | 23.9356 | 5.4952 | 8.7200 | 9.33 | 47.48 | 0.78 | 95 | 95 |
| Basin 2 | 3.5838 | 0.1905 | 6.7400 | 0.72 | 11.23 | 0.53 | 87 | 87 |
| Basin 3 | 48.3186 | 3.3720 | 19.8500 | 2.56 | 74.10 | 0.71 | 93 | 93 |



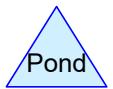
Basin 3 (North) -
Buildout



Basin 2 (Middle) -
Buildout



Basin 1 (South) -
Buildout



Routing Diagram for Malarkey IND_Huff_R1
Prepared by Kimley-Horn & Associates, Printed 10/4/2024
HydroCAD® 10.20-3c s/n 02344 © 2023 HydroCAD Software Solutions LLC

Summary for Subcatchment 20S: Basin 3 (North) - Buildout

Runoff = 24.65 cfs @ 15.44 hrs, Volume= 20.424 af, Depth= 3.30"

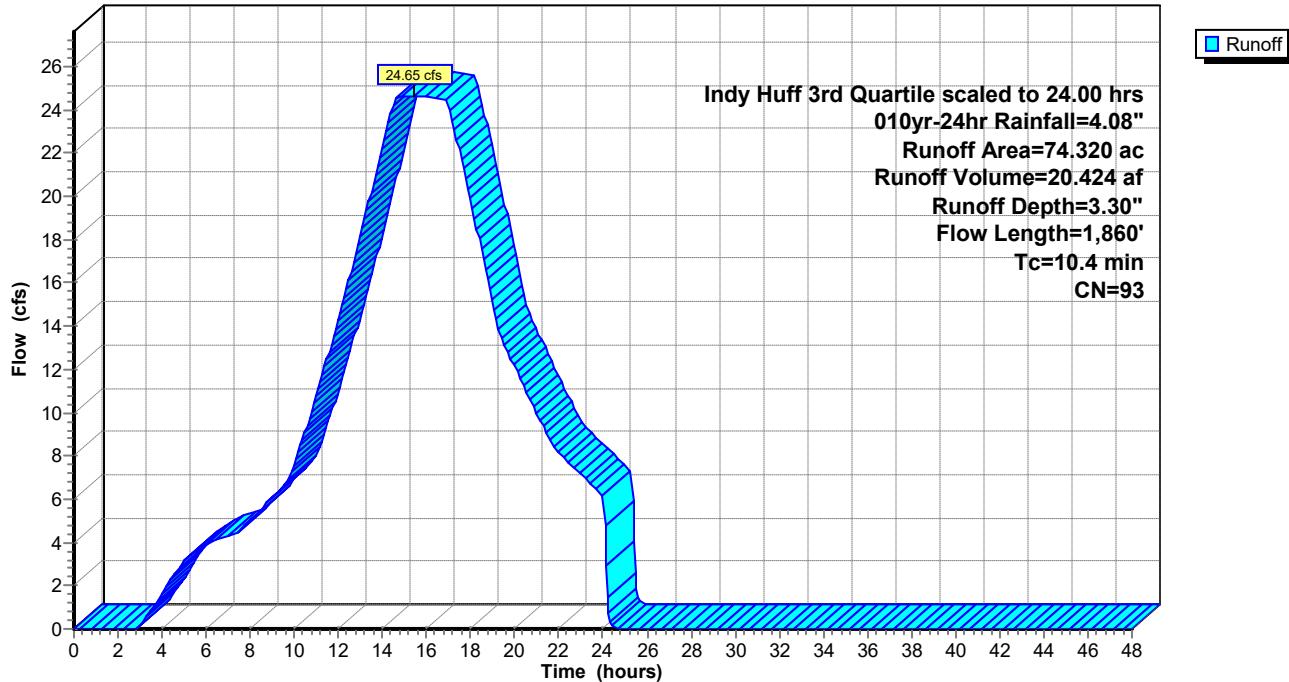
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs
 Indy Huff 3rd Quartile scaled to 24.00 hrs 010yr-24hr Rainfall=4.08"

| Area (ac) | CN | Description |
|-----------|----|-----------------------|
| * 74.320 | 93 | From Excel |
| 74.320 | | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|-------------|------------------|------------------|----------------------|-------------------|---|
| 2.8 | 20 | 0.0200 | 0.12 | | Sheet Flow, Grass: Short n= 0.150 P2= 2.93" |
| 1.4 | 80 | 0.0100 | 0.95 | | Sheet Flow, Smooth surfaces n= 0.011 P2= 2.93" |
| 0.8 | 100 | 0.0100 | 2.03 | | Shallow Concentrated Flow, Paved Kv= 20.3 fps |
| 5.4 | 1,660 | 0.0030 | 5.17 | 36.53 | Pipe Channel, RCP_Round 36" 36.0" Round Area= 7.1 sf Perim= 9.4' r= 0.75' n= 0.013 |
| 10.4 | 1,860 | Total | | | |

Subcatchment 20S: Basin 3 (North) - Buildout

Hydrograph



Summary for Subcatchment 21S: Basin 2 (Middle) - Buildout

Runoff = 3.35 cfs @ 16.85 hrs, Volume= 2.536 af, Depth= 2.71"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs
 Indy Huff 3rd Quartile scaled to 24.00 hrs 010yr-24hr Rainfall=4.08"

| Area (ac) | CN | Description |
|-----------|----|-------------|
|-----------|----|-------------|

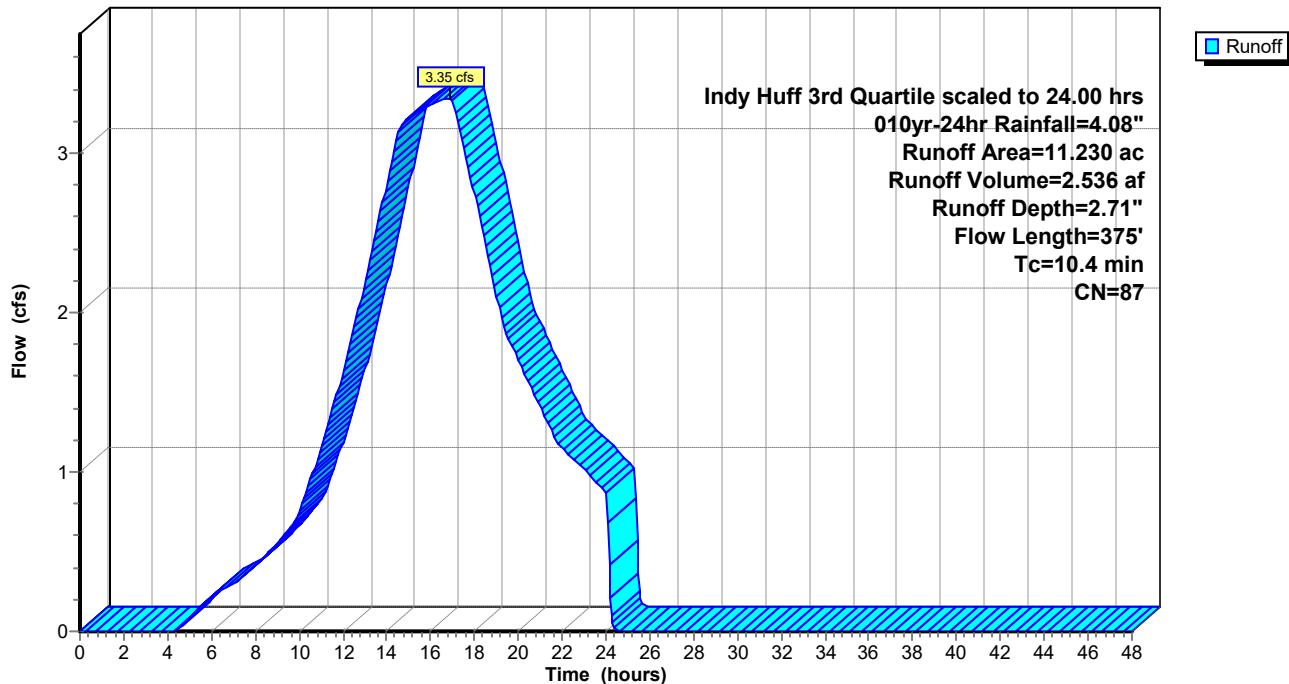
| | | |
|----------|----|------------|
| * 11.230 | 87 | From Excel |
|----------|----|------------|

| | |
|--------|-----------------------|
| 11.230 | 100.00% Pervious Area |
|--------|-----------------------|

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|-------------|------------------|------------------|----------------------|-------------------|--|
| 6.9 | 75 | 0.0300 | 0.18 | | Sheet Flow, Grass: Short n= 0.150 P2= 2.93" |
| 0.9 | 110 | 0.0100 | 2.03 | | Shallow Concentrated Flow, Paved Kv= 20.3 fps |
| 2.6 | 190 | 0.0300 | 1.21 | | Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps |
| 10.4 | 375 | Total | | | |

Subcatchment 21S: Basin 2 (Middle) - Buildout

Hydrograph



Summary for Subcatchment 22S: Basin 1 (South) - Buildout

Runoff = 16.48 cfs @ 14.77 hrs, Volume= 14.034 af, Depth= 3.51"

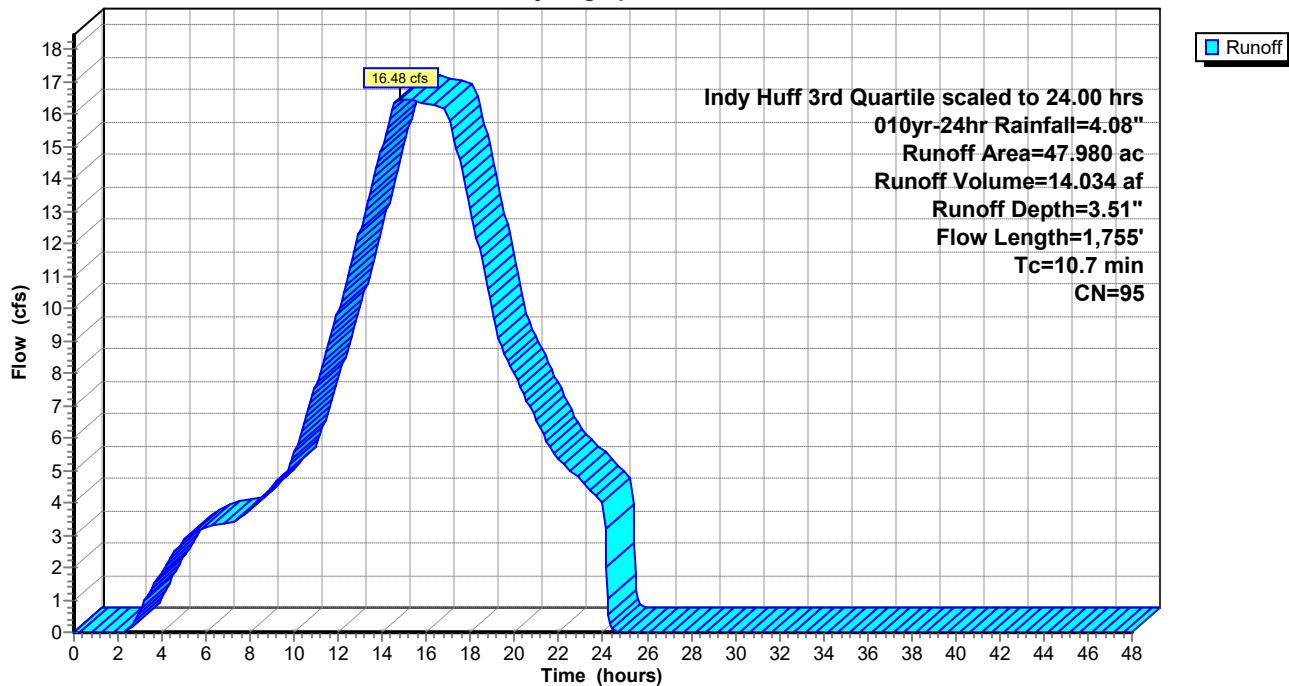
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs
 Indy Huff 3rd Quartile scaled to 24.00 hrs 010yr-24hr Rainfall=4.08"

| Area (ac) | CN | Description |
|-----------|--------|-----------------------|
| * | 47.980 | 95 |
| 47.980 | | 100.00% Pervious Area |

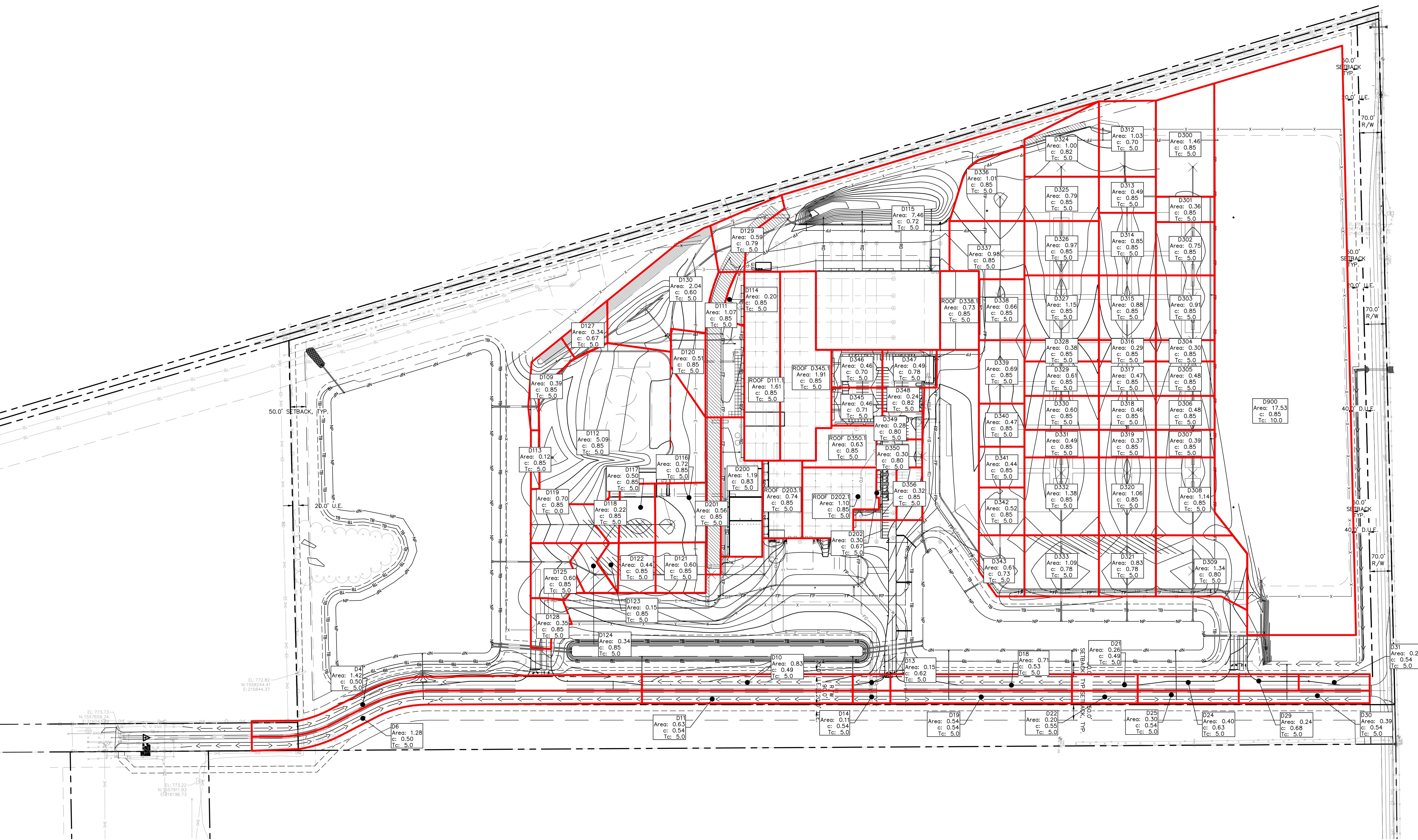
| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|-------------|------------------|------------------|----------------------|-------------------|--|
| 5.9 | 50 | 0.0200 | 0.14 | | Sheet Flow, Rail Shoulder Area Grass: Short n= 0.150 P2= 2.93" |
| 0.4 | 55 | 0.1100 | 2.32 | | Shallow Concentrated Flow, Swale Bank Short Grass Pasture Kv= 7.0 fps |
| 0.4 | 400 | 0.0100 | 17.92 | 6,022.73 | Trap/Vee/Rect Channel Flow, Btm Swale to D104 Bot.W=20.00' D=7.00' Z= 4.0 ' Top.W=76.00' n= 0.022 |
| 4.0 | 1,250 | 0.0030 | 5.17 | 36.53 | Pipe Channel, D104 to Pond1 36.0" Round Area= 7.1 sf Perim= 9.4' r= 0.75' n= 0.013 |
| 10.7 | 1,755 | Total | | | |

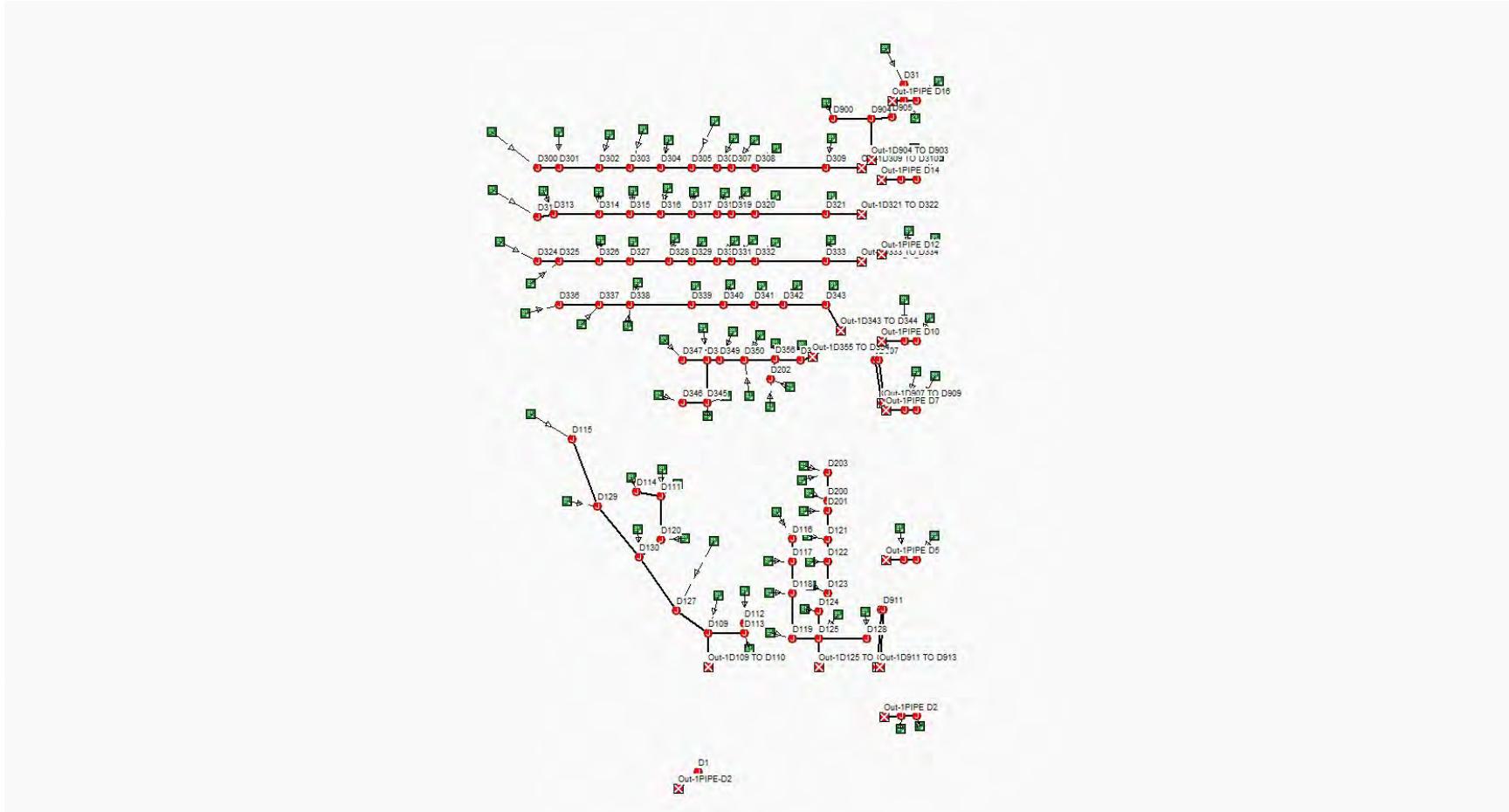
Subcatchment 22S: Basin 1 (South) - Buildout

Hydrograph



Appendix F: Storm Sewer Design Calculations





Malarkey IND - Franklin, IN
Storm Sewer Catchment Area Analysis

| Catchment Area | Pervious (ac) | Impervious (ac) | Total (ac) | c | CN |
|----------------|---------------|-----------------|------------|------|----|
| D109 | 0.0000 | 0.39 | 0.39 | 0.85 | 98 |
| D111 | 0.0000 | 1.07 | 1.07 | 0.85 | 98 |
| D112 | 0.0000 | 5.09 | 5.09 | 0.85 | 98 |
| D113 | 0.0000 | 0.12 | 0.12 | 0.85 | 98 |
| D114 | 0.0000 | 0.20 | 0.20 | 0.85 | 98 |
| D115 | 1.7486 | 5.71 | 7.46 | 0.72 | 92 |
| D116 | 0.0000 | 0.72 | 0.72 | 0.85 | 98 |
| D117 | 0.0000 | 0.50 | 0.50 | 0.85 | 98 |
| D118 | 0.0000 | 0.22 | 0.22 | 0.85 | 98 |
| D119 | 0.0000 | 0.70 | 0.70 | 0.85 | 98 |
| D120 | 0.0000 | 0.51 | 0.51 | 0.85 | 98 |
| D121 | 0.0000 | 0.60 | 0.60 | 0.85 | 98 |
| D122 | 0.0000 | 0.44 | 0.44 | 0.85 | 98 |
| D123 | 0.0000 | 0.15 | 0.15 | 0.85 | 98 |
| D124 | 0.0000 | 0.34 | 0.34 | 0.85 | 98 |
| D125 | 0.0000 | 0.60 | 0.60 | 0.85 | 98 |
| D127 | 0.1100 | 0.23 | 0.34 | 0.67 | 90 |
| D128 | 0.0000 | 0.35 | 0.35 | 0.85 | 98 |
| D129 | 0.0680 | 0.52 | 0.59 | 0.79 | 95 |
| D130 | 0.9251 | 1.11 | 2.04 | 0.60 | 87 |
| D201 | 0.0000 | 0.56 | 0.56 | 0.85 | 98 |
| D202 | 0.0985 | 0.20 | 0.30 | 0.67 | 90 |
| D300 | 0.0000 | 1.46 | 1.46 | 0.85 | 98 |
| D301 | 0.0000 | 0.36 | 0.36 | 0.85 | 98 |
| D302 | 0.0000 | 0.75 | 0.75 | 0.85 | 98 |
| D303 | 0.0000 | 0.91 | 0.91 | 0.85 | 98 |
| D304 | 0.0000 | 0.30 | 0.30 | 0.85 | 98 |
| D305 | 0.0000 | 0.48 | 0.48 | 0.85 | 98 |
| D306 | 0.0000 | 0.48 | 0.48 | 0.85 | 98 |
| D307 | 0.0000 | 0.39 | 0.39 | 0.85 | 98 |
| D308 | 0.0000 | 1.14 | 1.14 | 0.85 | 98 |
| D309 | 0.0000 | 1.34 | 1.34 | 0.85 | 98 |
| D312 | 0.2883 | 0.74 | 1.03 | 0.70 | 91 |
| D313 | 0.0000 | 0.49 | 0.49 | 0.85 | 98 |
| D314 | 0.0000 | 0.85 | 0.85 | 0.85 | 98 |
| D315 | 0.0000 | 0.88 | 0.88 | 0.85 | 98 |
| D316 | 0.0000 | 0.29 | 0.29 | 0.85 | 98 |
| D317 | 0.0000 | 0.47 | 0.47 | 0.85 | 98 |
| D318 | 0.0000 | 0.46 | 0.46 | 0.85 | 98 |
| D319 | 0.0000 | 0.37 | 0.37 | 0.85 | 98 |
| D320 | 0.0000 | 1.06 | 1.06 | 0.85 | 98 |
| D321 | 0.1032 | 0.73 | 0.83 | 0.78 | 95 |
| D324 | 0.0589 | 0.94 | 1.00 | 0.82 | 97 |

| | | | | | |
|------|--------|------|------|------|----|
| D325 | 0.0000 | 0.79 | 0.79 | 0.85 | 98 |
| D326 | 0.0000 | 0.97 | 0.97 | 0.85 | 98 |
| D327 | 0.0000 | 1.15 | 1.15 | 0.85 | 98 |
| D328 | 0.0000 | 0.38 | 0.38 | 0.85 | 98 |
| D329 | 0.0000 | 0.61 | 0.61 | 0.85 | 98 |
| D330 | 0.0000 | 0.60 | 0.60 | 0.85 | 98 |
| D331 | 0.0000 | 0.49 | 0.49 | 0.85 | 98 |
| D332 | 0.0000 | 1.38 | 1.38 | 0.85 | 98 |
| D333 | 0.1350 | 0.96 | 1.09 | 0.78 | 95 |
| D336 | 0.0000 | 1.01 | 1.01 | 0.85 | 98 |
| D337 | 0.0000 | 0.98 | 0.98 | 0.85 | 98 |
| D338 | 0.0000 | 0.66 | 0.66 | 0.85 | 98 |
| D339 | 0.0000 | 0.69 | 0.69 | 0.85 | 98 |
| D340 | 0.0000 | 0.47 | 0.47 | 0.85 | 98 |
| D341 | 0.0000 | 0.44 | 0.44 | 0.85 | 98 |
| D342 | 0.0000 | 0.52 | 0.52 | 0.85 | 98 |
| D343 | 0.0000 | 0.61 | 0.61 | 0.85 | 98 |
| D345 | 0.1193 | 0.34 | 0.46 | 0.71 | 92 |
| D346 | 0.1290 | 0.33 | 0.46 | 0.70 | 91 |
| D347 | 0.0600 | 0.43 | 0.49 | 0.78 | 95 |
| D348 | 0.0135 | 0.23 | 0.24 | 0.82 | 97 |
| D349 | 0.0255 | 0.25 | 0.28 | 0.80 | 96 |
| D350 | 0.0375 | 0.26 | 0.30 | 0.78 | 95 |
| D356 | 0.0000 | 0.32 | 0.32 | 0.85 | 98 |
| | | | | | |
| | | | | | |
| | | | | | |
| | | | | | |
| | | | | | |

c' (RATIONAL) CN (TR-55)

| | | |
|------------|------|----|
| Pervious | 0.3 | 74 |
| Impervious | 0.85 | 98 |

INLET CALCULATION COMPUTATION

Date: 8-Oct-24
 Designed By: Malarkey IND - Franklin
 Project:

50 % Clogging Factor
 3 Weir Coefficient

$$Q = CA\sqrt{2gh}$$

Weir Equation Per INDOT = $Q = CPd^{1.5}$

* 50% Clogging Factor Applied

| Structure No. | Location: NOBLESVILLE, INDIANA | | | | Storm Event: | | | | 10 Year | | Notes | |
|---------------|--------------------------------|------------------------|--|-------------------------|--------------------|------------------------------------|----------------------------------|-------------------|--------------------|--------------|-------------------------------|---|
| | Runoff Coefficient (C) | Rainfall Intensity (i) | *Clear Opening Area (A) (in ²) | Orifice Coefficient (C) | Drainage Area (ac) | Depth of Water over Grate (h) (in) | Gravity (g) (ft/s ²) | Q Allowable (cfs) | Q Calculated (cfs) | CASTING TYPE | PONDING DEPTH (WEIR) (d) (ft) | |
| D109 | 0.85 | 7.16 | 144 | 0.67 | 0.39 | 7 | 32.2 | 4.11 | > 2.37 | R-4342 | 0.49 | |
| D111 | 0.85 | 7.16 | 187.2 | 0.67 | 1.07 | 7 | 32.2 | 5.34 | > 6.51 | R-3455-C | 0.96 | Partial Perforated Underdrain |
| D112 | 0.85 | 7.16 | 144 | 0.67 | 5.09 | 7 | 32.2 | 4.11 | > 30.98 | R-4342 | 2.72 | Stub for Future Expansion |
| D113 | 0.85 | 7.16 | 79.2 | 0.67 | 0.12 | 7 | 32.2 | 2.26 | > 0.73 | R-3010 | 0.22 | |
| D114 | 0.85 | 7.16 | 93.6 | 0.67 | 0.20 | 7 | 32.2 | 2.67 | > 1.22 | R-3472 | 0.31 | |
| D116 | 0.85 | 7.16 | 187.2 | 0.67 | 0.72 | 7 | 32.2 | 5.34 | > 4.38 | R-3455-C | 0.74 | |
| D117 | 0.85 | 7.16 | 187.2 | 0.67 | 0.50 | 7 | 32.2 | 5.34 | > 3.04 | R-3455-C | 0.58 | |
| D118 | 0.85 | 7.16 | 187.2 | 0.67 | 0.22 | 7 | 32.2 | 5.34 | > 1.34 | R-3455-C | 0.34 | |
| D119 | 0.85 | 7.16 | 151.2 | 0.67 | 0.70 | 7 | 32.2 | 4.31 | > 4.26 | R-3287-10V | 0.73 | |
| D120 | 0.85 | 7.16 | 187.2 | 0.67 | 0.51 | 7 | 32.2 | 5.34 | > 3.10 | R-3455-C | 0.59 | |
| D121 | 0.85 | 7.16 | 187.2 | 0.67 | 0.60 | 7 | 32.2 | 5.34 | > 3.65 | R-3455-C | 0.65 | |
| D122 | 0.85 | 7.16 | 187.2 | 0.67 | 0.44 | 7 | 32.2 | 5.34 | > 2.68 | R-3455-C | 0.53 | |
| D123 | 0.85 | 7.16 | 93.6 | 0.67 | 0.15 | 7 | 32.2 | 2.67 | > 0.91 | R-3472 | 0.26 | |
| D124 | 0.85 | 7.16 | 93.6 | 0.67 | 0.34 | 7 | 32.2 | 2.67 | > 2.07 | R-3472 | 0.45 | |
| D125 | 0.85 | 7.16 | 151.2 | 0.67 | 0.60 | 7 | 32.2 | 4.31 | > 3.65 | R-3287-10V | 0.65 | |
| D127 | 0.67 | 7.16 | 93.6 | 0.67 | 0.34 | 7 | 32.2 | 2.67 | > 1.64 | R-3472 | 0.38 | |
| D128 | 0.85 | 7.16 | 79.2 | 0.67 | 0.35 | 7 | 32.2 | 2.26 | > 2.13 | R-3010 | 0.46 | |
| D129 | 0.79 | 7.16 | 187.2 | 0.67 | 0.59 | 7 | 32.2 | 5.34 | > 3.32 | R-3455-C | 0.61 | |
| D130 | 0.60 | 7.16 | 144 | 0.67 | 2.04 | 36 | 32.2 | 9.31 | > 8.77 | R-4342 | 1.17 | Depressed Yard |
| D201 | 0.85 | 7.16 | 93.6 | 0.67 | 0.56 | 7 | 32.2 | 2.67 | > 3.41 | R-3472 | 0.62 | Perforated |
| D202 | 0.67 | 7.16 | 108 | 0.67 | 0.30 | 7 | 32.2 | 3.08 | > 1.44 | R-3287-SB10 | 0.35 | |
| D300 | 0.85 | 7.16 | 187.2 | 0.67 | 1.46 | 7 | 32.2 | 5.34 | > 8.89 | R-3455-C | 1.18 | Stub for Future Expansion |
| D301 | 0.85 | 7.16 | 187.2 | 0.67 | 0.36 | 12 | 32.2 | 6.99 | > 2.19 | R-3455-C | 0.47 | |
| D302 | 0.85 | 7.16 | 187.2 | 0.67 | 0.75 | 12 | 32.2 | 6.99 | > 4.56 | R-3455-C | 0.76 | |
| D303 | 0.85 | 7.16 | 187.2 | 0.67 | 0.91 | 12 | 32.2 | 6.99 | > 5.54 | R-3455-C | 0.86 | |
| D304 | 0.85 | 7.16 | 187.2 | 0.67 | 0.30 | 12 | 32.2 | 6.99 | > 1.83 | R-3455-C | 0.41 | |
| D305 | 0.85 | 7.16 | 187.2 | 0.67 | 0.48 | 12 | 32.2 | 6.99 | > 2.92 | R-3455-C | 0.56 | |
| D306 | 0.85 | 7.16 | 187.2 | 0.67 | 0.48 | 12 | 32.2 | 6.99 | > 2.92 | R-3455-C | 0.56 | |
| D307 | 0.85 | 7.16 | 187.2 | 0.67 | 0.39 | 12 | 32.2 | 6.99 | > 2.37 | R-3455-C | 0.49 | |
| D308 | 0.85 | 7.16 | 187.2 | 0.67 | 1.14 | 12 | 32.2 | 6.99 | > 6.94 | R-3455-C | 1.00 | |
| D309 | 0.85 | 7.16 | 187.2 | 0.67 | 1.34 | 12 | 32.2 | 6.99 | > 8.16 | R-3455-C | 1.12 | Any Clogging Overflow over Curb will spill directly into Pond 2 |
| D312 | 0.70 | 7.16 | 187.2 | 0.67 | 1.03 | 12 | 32.2 | 6.99 | > 5.13 | R-3455-C | 0.82 | |

| | | | | | | | | | | | | | |
|------|------|------|-------|------|------|----|------|------|---|------|----------|------|-------------------|
| D313 | 0.85 | 7.16 | 187.2 | 0.67 | 0.49 | 12 | 32.2 | 6.99 | > | 2.98 | R-3455-C | 0.57 | |
| D314 | 0.85 | 7.16 | 187.2 | 0.67 | 0.85 | 12 | 32.2 | 6.99 | > | 5.17 | R-3455-C | 0.83 | |
| D315 | 0.85 | 7.16 | 187.2 | 0.67 | 0.88 | 12 | 32.2 | 6.99 | > | 5.36 | R-3455-C | 0.84 | |
| D316 | 0.85 | 7.16 | 187.2 | 0.67 | 0.29 | 12 | 32.2 | 6.99 | > | 1.76 | R-3455-C | 0.40 | |
| D317 | 0.85 | 7.16 | 187.2 | 0.67 | 0.47 | 12 | 32.2 | 6.99 | > | 2.86 | R-3455-C | 0.56 | |
| D318 | 0.85 | 7.16 | 187.2 | 0.67 | 0.46 | 12 | 32.2 | 6.99 | > | 2.80 | R-3455-C | 0.55 | |
| D319 | 0.85 | 7.16 | 187.2 | 0.67 | 0.37 | 12 | 32.2 | 6.99 | > | 2.25 | R-3455-C | 0.47 | |
| D320 | 0.85 | 7.16 | 187.2 | 0.67 | 1.06 | 12 | 32.2 | 6.99 | > | 6.45 | R-3455-C | 0.96 | |
| D321 | 0.78 | 7.16 | 187.2 | 0.67 | 0.83 | 12 | 32.2 | 6.99 | > | 4.64 | R-3455-C | 0.77 | |
| D324 | 0.82 | 7.16 | 187.2 | 0.67 | 1.00 | 12 | 32.2 | 6.99 | > | 5.85 | R-3455-C | 0.90 | |
| D325 | 0.85 | 7.16 | 187.2 | 0.67 | 0.79 | 12 | 32.2 | 6.99 | > | 4.81 | R-3455-C | 0.79 | |
| D326 | 0.85 | 7.16 | 187.2 | 0.67 | 0.97 | 12 | 32.2 | 6.99 | > | 5.90 | R-3455-C | 0.90 | |
| D327 | 0.85 | 7.16 | 187.2 | 0.67 | 1.15 | 12 | 32.2 | 6.99 | > | 7.00 | R-3455-C | 1.01 | Doubled with D326 |
| D328 | 0.85 | 7.16 | 187.2 | 0.67 | 0.38 | 12 | 32.2 | 6.99 | > | 2.31 | R-3455-C | 0.48 | |
| D329 | 0.85 | 7.16 | 187.2 | 0.67 | 0.61 | 12 | 32.2 | 6.99 | > | 3.71 | R-3455-C | 0.66 | |
| D330 | 0.85 | 7.16 | 187.2 | 0.67 | 0.60 | 12 | 32.2 | 6.99 | > | 3.65 | R-3455-C | 0.65 | |
| D331 | 0.85 | 7.16 | 187.2 | 0.67 | 0.49 | 12 | 32.2 | 6.99 | > | 2.98 | R-3455-C | 0.57 | |
| D332 | 0.85 | 7.16 | 187.2 | 0.67 | 1.38 | 12 | 32.2 | 6.99 | > | 8.40 | R-3455-C | 1.14 | Doubled with D331 |
| D333 | 0.78 | 7.16 | 187.2 | 0.67 | 1.09 | 12 | 32.2 | 6.99 | > | 6.10 | R-3455-C | 0.92 | |
| D336 | 0.85 | 7.16 | 187.2 | 0.67 | 1.01 | 12 | 32.2 | 6.99 | > | 6.15 | R-3455-C | 0.93 | |
| D337 | 0.85 | 7.16 | 187.2 | 0.67 | 0.98 | 12 | 32.2 | 6.99 | > | 5.96 | R-3455-C | 0.91 | |
| D338 | 0.85 | 7.16 | 187.2 | 0.67 | 0.66 | 12 | 32.2 | 6.99 | > | 4.02 | R-3455-C | 0.70 | |
| D339 | 0.85 | 7.16 | 187.2 | 0.67 | 0.69 | 12 | 32.2 | 6.99 | > | 4.20 | R-3455-C | 0.72 | |
| D340 | 0.85 | 7.16 | 187.2 | 0.67 | 0.47 | 12 | 32.2 | 6.99 | > | 2.86 | R-3455-C | 0.56 | |
| D341 | 0.85 | 7.16 | 187.2 | 0.67 | 0.44 | 12 | 32.2 | 6.99 | > | 2.68 | R-3455-C | 0.53 | |
| D342 | 0.85 | 7.16 | 187.2 | 0.67 | 0.52 | 12 | 32.2 | 6.99 | > | 3.16 | R-3455-C | 0.59 | |
| D343 | 0.85 | 7.16 | 187.2 | 0.67 | 0.61 | 12 | 32.2 | 6.99 | > | 3.71 | R-3455-C | 0.66 | |
| D345 | 0.71 | 7.16 | 79.2 | 0.67 | 0.46 | 12 | 32.2 | 2.96 | > | 2.33 | R-3010 | 0.48 | |
| D346 | 0.70 | 7.16 | 79.2 | 0.67 | 0.46 | 12 | 32.2 | 2.96 | > | 2.29 | R-3010 | 0.48 | |
| D347 | 0.78 | 7.16 | 79.2 | 0.67 | 0.49 | 12 | 32.2 | 2.96 | > | 2.75 | R-3010 | 0.54 | |
| D348 | 0.82 | 7.16 | 79.2 | 0.67 | 0.24 | 12 | 32.2 | 2.96 | > | 1.41 | R-3010 | 0.35 | |
| D349 | 0.80 | 7.16 | 144 | 0.67 | 0.28 | 12 | 32.2 | 5.38 | > | 1.60 | R-4342 | 0.38 | |
| D350 | 0.78 | 7.16 | 144 | 0.67 | 0.30 | 12 | 32.2 | 5.38 | > | 1.68 | R-4342 | 0.39 | |
| D356 | 0.85 | 7.16 | 144 | 0.67 | 0.32 | 12 | 32.2 | 5.38 | > | 1.95 | R-4342 | 0.43 | |

Project Description

File Name MalarkeyIND_StormSewerSizing_10-3-24.SPF

Project Options

| | |
|---|----------------|
| Flow Units | CFS |
| Elevation Type | Elevation |
| Hydrology Method | Rational |
| Time of Concentration (TOC) Method | User-Defined |
| Link Routing Method | Kinematic Wave |
| Enable Overflow Ponding at Nodes | YES |
| Skip Steady State Analysis Time Periods | NO |

Analysis Options

| | | |
|--------------------------------------|------------|---------------|
| Start Analysis On | 00:00:00 | 0:00:00 |
| End Analysis On | 00:00:00 | 0:00:00 |
| Start Reporting On | 00:00:00 | 0:00:00 |
| Antecedent Dry Days | 0 | days |
| Runoff (Dry Weather) Time Step | 0 01:00:00 | days hh:mm:ss |
| Runoff (Wet Weather) Time Step | 0 00:05:00 | days hh:mm:ss |
| Reporting Time Step | 0 00:05:00 | days hh:mm:ss |
| Routing Time Step | 30 | seconds |

Number of Elements

| | Qty |
|------------------------------|-----|
| Rain Gages | 0 |
| Subbasins..... | 92 |
| Nodes..... | 113 |
| <i>Junctions</i> | 93 |
| <i>Outfalls</i> | 20 |
| <i>Flow Diversions</i> | 0 |
| <i>Inlets</i> | 0 |
| <i>Storage Nodes</i> | 0 |
| Links..... | 93 |
| <i>Channels</i> | 0 |
| <i>Pipes</i> | 93 |
| <i>Pumps</i> | 0 |
| <i>Orifices</i> | 0 |
| <i>Weirs</i> | 0 |
| <i>Outlets</i> | 0 |
| Pollutants | 0 |
| Land Uses | 0 |

Rainfall Details

Return Period..... 10 year(s)

Subbasin Summary

| SN | Subbasin ID | Area (ac) | Weighted Runoff Coefficient | Total Rainfall | Total Runoff | Total Runoff | Peak (cfs) | Time of Concentration (days hh:mm:ss) |
|----|-------------|--------------|-----------------------------------|-------------------|-----------------|-----------------|---------------|---|
| | | | | | | Volume (in) | | |
| | | | | | | (in) | (ac-in) | |
| 1 | Sub-D10 | 0.83 | 0.4900 | 0.60 | 0.29 | 0.24 | 2.93 | 0 00:05:00 |
| 2 | Sub-D109 | 0.39 | 0.8500 | 0.60 | 0.51 | 0.20 | 2.41 | 0 00:05:00 |
| 3 | Sub-D11 | 0.63 | 0.5400 | 0.60 | 0.32 | 0.20 | 2.46 | 0 00:05:00 |
| 4 | Sub-D111 | 1.07 | 0.8500 | 0.60 | 0.51 | 0.55 | 6.56 | 0 00:05:00 |
| 5 | Sub-D111.1 | 1.61 | 0.8500 | 0.60 | 0.51 | 0.82 | 9.87 | 0 00:05:00 |
| 6 | Sub-D112 | 5.09 | 0.8500 | 0.60 | 0.51 | 2.60 | 31.21 | 0 00:05:00 |
| 7 | Sub-D113 | 0.12 | 0.8500 | 0.60 | 0.51 | 0.06 | 0.73 | 0 00:05:00 |
| 8 | Sub-D114 | 0.20 | 0.8500 | 0.60 | 0.51 | 0.10 | 1.23 | 0 00:05:00 |
| 9 | Sub-D115 | 7.46 | 0.7200 | 0.60 | 0.43 | 3.23 | 38.73 | 0 00:05:00 |
| 10 | Sub-D116 | 0.72 | 0.8500 | 0.60 | 0.51 | 0.37 | 4.42 | 0 00:05:00 |
| 11 | Sub-D117 | 0.50 | 0.8500 | 0.60 | 0.51 | 0.26 | 3.08 | 0 00:05:00 |
| 12 | Sub-D118 | 0.22 | 0.8500 | 0.60 | 0.51 | 0.11 | 1.34 | 0 00:05:00 |
| 13 | Sub-D119 | 0.70 | 0.8500 | 0.60 | 0.51 | 0.36 | 4.30 | 0 00:05:00 |
| 14 | Sub-D120 | 0.51 | 0.8500 | 0.60 | 0.51 | 0.26 | 3.10 | 0 00:05:00 |
| 15 | Sub-D121 | 0.60 | 0.8500 | 0.60 | 0.51 | 0.31 | 3.70 | 0 00:05:00 |
| 16 | Sub-D122 | 0.44 | 0.8500 | 0.60 | 0.51 | 0.23 | 2.72 | 0 00:05:00 |
| 17 | Sub-D123 | 0.15 | 0.8500 | 0.60 | 0.51 | 0.08 | 0.92 | 0 00:05:00 |
| 18 | Sub-D124 | 0.34 | 0.8500 | 0.60 | 0.51 | 0.17 | 2.09 | 0 00:05:00 |
| 19 | Sub-D125 | 0.60 | 0.8500 | 0.60 | 0.51 | 0.31 | 3.66 | 0 00:05:00 |
| 20 | Sub-D127 | 0.34 | 0.6700 | 0.60 | 0.40 | 0.14 | 1.64 | 0 00:05:00 |
| 21 | Sub-D128 | 0.35 | 0.8500 | 0.60 | 0.51 | 0.18 | 2.16 | 0 00:05:00 |
| 22 | Sub-D129 | 0.33 | 0.7900 | 0.60 | 0.48 | 0.16 | 1.87 | 0 00:05:00 |
| 23 | Sub-D13 | 0.15 | 0.6200 | 0.60 | 0.37 | 0.06 | 0.66 | 0 00:05:00 |
| 24 | Sub-D130 | 2.04 | 0.6000 | 0.60 | 0.36 | 0.73 | 8.83 | 0 00:05:00 |
| 25 | Sub-D14 | 0.11 | 0.5400 | 0.60 | 0.32 | 0.04 | 0.44 | 0 00:05:00 |
| 26 | Sub-D18 | 0.71 | 0.5300 | 0.60 | 0.32 | 0.23 | 2.72 | 0 00:05:00 |
| 27 | Sub-D19 | 0.54 | 0.5400 | 0.60 | 0.32 | 0.18 | 2.11 | 0 00:05:00 |
| 28 | Sub-D200 | 1.19 | 0.8300 | 0.60 | 0.50 | 0.59 | 7.12 | 0 00:05:00 |
| 29 | Sub-D201 | 0.56 | 0.8500 | 0.60 | 0.51 | 0.29 | 3.45 | 0 00:05:00 |
| 30 | Sub-D202 | 0.30 | 0.6700 | 0.60 | 0.40 | 0.12 | 1.45 | 0 00:05:00 |
| 31 | Sub-D202.1 | 1.10 | 0.8500 | 0.60 | 0.51 | 0.56 | 6.74 | 0 00:05:00 |
| 32 | Sub-D203 | 0.74 | 0.8500 | 0.60 | 0.51 | 0.38 | 4.52 | 0 00:05:00 |
| 33 | Sub-D203.1 | 0.74 | 0.8500 | 0.60 | 0.51 | 0.38 | 4.54 | 0 00:05:00 |
| 34 | Sub-D21 | 0.26 | 0.4900 | 0.60 | 0.29 | 0.08 | 0.91 | 0 00:05:00 |
| 35 | Sub-D22 | 0.20 | 0.5500 | 0.60 | 0.33 | 0.06 | 0.78 | 0 00:05:00 |
| 36 | Sub-D24 | 0.40 | 0.6300 | 0.60 | 0.38 | 0.15 | 1.80 | 0 00:05:00 |
| 37 | Sub-D25 | 0.30 | 0.5400 | 0.60 | 0.32 | 0.10 | 1.18 | 0 00:05:00 |
| 38 | Sub-D29 | 0.24 | 0.6800 | 0.60 | 0.41 | 0.10 | 1.16 | 0 00:05:00 |
| 39 | Sub-D30 | 0.39 | 0.5400 | 0.60 | 0.32 | 0.13 | 1.53 | 0 00:05:00 |
| 40 | Sub-D300 | 1.46 | 0.8500 | 0.60 | 0.51 | 0.75 | 8.96 | 0 00:05:00 |
| 41 | Sub-D301 | 0.36 | 0.8500 | 0.60 | 0.51 | 0.18 | 2.18 | 0 00:05:00 |
| 42 | Sub-D302 | 0.75 | 0.8500 | 0.60 | 0.51 | 0.38 | 4.58 | 0 00:05:00 |
| 43 | Sub-D303 | 0.91 | 0.8500 | 0.60 | 0.51 | 0.46 | 5.56 | 0 00:05:00 |
| 44 | Sub-D304 | 0.30 | 0.8500 | 0.60 | 0.51 | 0.15 | 1.83 | 0 00:05:00 |
| 45 | Sub-D305 | 0.48 | 0.8500 | 0.60 | 0.51 | 0.25 | 2.96 | 0 00:05:00 |
| 46 | Sub-D306 | 0.48 | 0.8500 | 0.60 | 0.51 | 0.24 | 2.92 | 0 00:05:00 |
| 47 | Sub-D307 | 0.39 | 0.8500 | 0.60 | 0.51 | 0.20 | 2.37 | 0 00:05:00 |
| 48 | Sub-D308 | 1.14 | 0.8500 | 0.60 | 0.51 | 0.58 | 7.00 | 0 00:05:00 |
| 49 | Sub-D309 | 1.34 | 0.8000 | 0.60 | 0.48 | 0.64 | 7.73 | 0 00:05:00 |
| 50 | Sub-D31 | 0.28 | 0.5400 | 0.60 | 0.32 | 0.09 | 1.09 | 0 00:05:00 |
| 51 | Sub-D312 | 1.03 | 0.7000 | 0.60 | 0.42 | 0.43 | 5.19 | 0 00:05:00 |
| 52 | Sub-D313 | 0.49 | 0.8500 | 0.60 | 0.51 | 0.25 | 3.00 | 0 00:05:00 |
| 53 | Sub-D314 | 0.85 | 0.8500 | 0.60 | 0.51 | 0.43 | 5.21 | 0 00:05:00 |
| 54 | Sub-D315 | 0.88 | 0.8500 | 0.60 | 0.51 | 0.45 | 5.38 | 0 00:05:00 |
| 55 | Sub-D316 | 0.29 | 0.8500 | 0.60 | 0.51 | 0.15 | 1.78 | 0 00:05:00 |
| 56 | Sub-D317 | 0.47 | 0.8500 | 0.60 | 0.51 | 0.24 | 2.87 | 0 00:05:00 |
| 57 | Sub-D318 | 0.46 | 0.8500 | 0.60 | 0.51 | 0.24 | 2.83 | 0 00:05:00 |
| 58 | Sub-D319 | 0.37 | 0.8500 | 0.60 | 0.51 | 0.19 | 2.30 | 0 00:05:00 |
| 59 | Sub-D320 | 1.06 | 0.8500 | 0.60 | 0.51 | 0.54 | 6.48 | 0 00:05:00 |
| 60 | Sub-D321 | 0.83 | 0.7800 | 0.60 | 0.47 | 0.39 | 4.67 | 0 00:05:00 |
| 61 | Sub-D324 | 1.00 | 0.8200 | 0.60 | 0.49 | 0.49 | 5.92 | 0 00:05:00 |
| 62 | Sub-D325 | 0.79 | 0.8500 | 0.60 | 0.51 | 0.40 | 4.82 | 0 00:05:00 |
| 63 | Sub-D326 | 0.97 | 0.8500 | 0.60 | 0.51 | 0.49 | 5.92 | 0 00:05:00 |
| 64 | Sub-D327 | 1.15 | 0.8500 | 0.60 | 0.51 | 0.59 | 7.04 | 0 00:05:00 |
| 65 | Sub-D328 | 0.38 | 0.8500 | 0.60 | 0.51 | 0.19 | 2.32 | 0 00:05:00 |

Subbasin Summary

| SN ID | Subbasin | Area (ac) | Weighted Runoff Coefficient | Total Rainfall | Total Runoff | Total Runoff | Peak (cfs) | Time of Concentration (days hh:mm:ss) |
|----------|------------|--------------|-----------------------------------|-------------------|-----------------|-----------------|---------------|---|
| | | | | | | Volume (in) | | |
| | | | | | | (ac-in) | | |
| 66 | Sub-D329 | 0.61 | 0.8500 | 0.60 | 0.51 | 0.31 | 3.75 | 0 00:05:00 |
| 67 | Sub-D330 | 0.60 | 0.8500 | 0.60 | 0.51 | 0.31 | 3.70 | 0 00:05:00 |
| 68 | Sub-D331 | 0.49 | 0.8500 | 0.60 | 0.51 | 0.25 | 3.00 | 0 00:05:00 |
| 69 | Sub-D332 | 1.38 | 0.8500 | 0.60 | 0.51 | 0.71 | 8.47 | 0 00:05:00 |
| 70 | Sub-D333 | 1.09 | 0.7800 | 0.60 | 0.47 | 0.51 | 6.11 | 0 00:05:00 |
| 71 | Sub-D336 | 1.01 | 0.8500 | 0.60 | 0.51 | 0.52 | 6.20 | 0 00:05:00 |
| 72 | Sub-D337 | 0.98 | 0.8500 | 0.60 | 0.51 | 0.50 | 6.02 | 0 00:05:00 |
| 73 | Sub-D338 | 0.73 | 0.8500 | 0.60 | 0.51 | 0.37 | 4.47 | 0 00:05:00 |
| 74 | Sub-D338.1 | 0.73 | 0.8500 | 0.60 | 0.51 | 0.37 | 4.47 | 0 00:05:00 |
| 75 | Sub-D339 | 0.69 | 0.8500 | 0.60 | 0.51 | 0.35 | 4.22 | 0 00:05:00 |
| 76 | Sub-D340 | 0.47 | 0.8500 | 0.60 | 0.51 | 0.24 | 2.86 | 0 00:05:00 |
| 77 | Sub-D341 | 0.44 | 0.8500 | 0.60 | 0.51 | 0.23 | 2.71 | 0 00:05:00 |
| 78 | Sub-D342 | 0.52 | 0.8500 | 0.60 | 0.51 | 0.26 | 3.18 | 0 00:05:00 |
| 79 | Sub-D343 | 0.61 | 0.7300 | 0.60 | 0.44 | 0.27 | 3.21 | 0 00:05:00 |
| 80 | Sub-D345 | 0.46 | 0.7100 | 0.60 | 0.43 | 0.20 | 2.36 | 0 00:05:00 |
| 81 | Sub-D345.1 | 1.91 | 0.8500 | 0.60 | 0.51 | 0.98 | 11.71 | 0 00:05:00 |
| 82 | Sub-D346 | 0.46 | 0.7000 | 0.60 | 0.42 | 0.19 | 2.31 | 0 00:05:00 |
| 83 | Sub-D347 | 0.49 | 0.7800 | 0.60 | 0.47 | 0.23 | 2.75 | 0 00:05:00 |
| 84 | Sub-D348 | 0.24 | 0.8200 | 0.60 | 0.49 | 0.12 | 1.42 | 0 00:05:00 |
| 85 | Sub-D349 | 0.28 | 0.8000 | 0.60 | 0.48 | 0.13 | 1.62 | 0 00:05:00 |
| 86 | Sub-D350 | 0.30 | 0.8000 | 0.60 | 0.48 | 0.14 | 1.73 | 0 00:05:00 |
| 87 | Sub-D350.1 | 0.63 | 0.8500 | 0.60 | 0.51 | 0.32 | 3.86 | 0 00:05:00 |
| 88 | Sub-D355 | 0.69 | 0.4700 | 0.60 | 0.28 | 0.19 | 2.34 | 0 00:05:00 |
| 89 | Sub-D356 | 0.32 | 0.8500 | 0.60 | 0.51 | 0.16 | 1.96 | 0 00:05:00 |
| 90 | Sub-D4 | 1.42 | 0.5000 | 0.60 | 0.30 | 0.43 | 5.12 | 0 00:05:00 |
| 91 | Sub-D6 | 1.28 | 0.5000 | 0.60 | 0.30 | 0.38 | 4.61 | 0 00:05:00 |
| 92 | Sub-D900 | 17.53 | 0.8500 | 0.90 | 0.77 | 13.43 | 80.60 | 0 00:10:00 |

Node Summary

| SN ID | Element Type | Invert | Ground/Rim | Initial | Surcharge | Ponded | Peak | Max HGL Attained | Max Surcharge Attained | Min Freeboard Attained | Time of | Total | Total Time |
|-----------------------|-----------------|-----------|------------|-----------------|--------------------|--------|--------|---------------------|------------------------------|------------------------------|--------------|---------|------------|
| | | Elevation | (Max) | Water Elevation | Elevation | Area | Inflow | | | | Peak | Flooded | Volume |
| | | (ft) | (ft) | (ft) | (ft ²) | (cfs) | (ft) | | | | (days hh:mm) | (ac-in) | (min) |
| 65 D330 | Junction | 775.45 | 781.96 | 775.45 | 781.96 | 0.00 | 28.74 | 777.46 | 0.00 | 4.51 | 0 00:00 | 0.00 | 0.00 |
| 66 D331 | Junction | 775.26 | 781.96 | 775.26 | 781.96 | 0.00 | 30.90 | 777.37 | 0.00 | 4.59 | 0 00:00 | 0.00 | 0.00 |
| 67 D332 | Junction | 774.93 | 781.43 | 774.93 | 781.43 | 0.00 | 36.90 | 777.05 | 0.00 | 4.38 | 0 00:00 | 0.00 | 0.00 |
| 68 D333 | Junction | 773.99 | 781.05 | 773.99 | 781.05 | 0.00 | 40.47 | 776.22 | 0.00 | 4.83 | 0 00:00 | 0.00 | 0.00 |
| 69 D336 | Junction | 777.88 | 782.65 | 777.88 | 782.65 | 0.00 | 6.20 | 778.93 | 0.00 | 3.72 | 0 00:00 | 0.00 | 0.00 |
| 70 D337 | Junction | 776.97 | 784.46 | 776.97 | 784.46 | 0.00 | 11.67 | 778.51 | 0.00 | 5.95 | 0 00:00 | 0.00 | 0.00 |
| 71 D338 | Junction | 776.55 | 784.81 | 776.55 | 784.81 | 0.00 | 19.63 | 778.36 | 0.00 | 6.46 | 0 00:00 | 0.00 | 0.00 |
| 72 D339 | Junction | 775.71 | 784.10 | 775.71 | 784.10 | 0.00 | 22.65 | 777.49 | 0.00 | 6.61 | 0 00:00 | 0.00 | 0.00 |
| 73 D340 | Junction | 775.29 | 783.75 | 775.29 | 783.75 | 0.00 | 24.73 | 777.10 | 0.00 | 6.65 | 0 00:00 | 0.00 | 0.00 |
| 74 D341 | Junction | 774.87 | 783.40 | 774.87 | 783.40 | 0.00 | 26.55 | 776.77 | 0.00 | 6.64 | 0 00:00 | 0.00 | 0.00 |
| 75 D342 | Junction | 774.47 | 782.75 | 774.47 | 782.75 | 0.00 | 28.51 | 776.46 | 0.00 | 6.29 | 0 00:00 | 0.00 | 0.00 |
| 76 D343 | Junction | 773.90 | 782.05 | 773.90 | 782.05 | 0.00 | 30.27 | 775.98 | 0.00 | 6.07 | 0 00:00 | 0.00 | 0.00 |
| 77 D345 | Junction | 779.73 | 785.41 | 779.73 | 785.41 | 0.00 | 16.22 | 780.89 | 0.00 | 4.52 | 0 00:00 | 0.00 | 0.00 |
| 78 D346 | Junction | 781.32 | 784.99 | 781.32 | 784.99 | 0.00 | 2.31 | 781.91 | 0.00 | 3.07 | 0 00:00 | 0.00 | 0.00 |
| 79 D347 | Junction | 780.29 | 784.75 | 780.29 | 784.75 | 0.00 | 2.75 | 780.95 | 0.00 | 3.80 | 0 00:00 | 0.00 | 0.00 |
| 80 D348 | Junction | 777.69 | 784.87 | 777.69 | 784.87 | 0.00 | 19.80 | 779.84 | 0.00 | 5.03 | 0 00:00 | 0.00 | 0.00 |
| 81 D349 | Junction | 777.23 | 785.46 | 777.23 | 785.46 | 0.00 | 21.27 | 778.60 | 0.00 | 6.86 | 0 00:00 | 0.00 | 0.00 |
| 82 D350 | Junction | 775.85 | 784.95 | 775.85 | 784.95 | 0.00 | 26.16 | 777.72 | 0.00 | 7.23 | 0 00:00 | 0.00 | 0.00 |
| 83 D355 | Junction | 773.78 | 782.92 | 773.78 | 782.92 | 0.00 | 37.04 | 775.58 | 0.00 | 7.34 | 0 00:00 | 0.00 | 0.00 |
| 84 D356 | Junction | 774.46 | 784.16 | 774.46 | 784.16 | 0.00 | 35.13 | 776.41 | 0.00 | 7.76 | 0 00:00 | 0.00 | 0.00 |
| 85 D4 | Junction | 771.38 | 772.90 | 771.38 | 772.90 | 0.00 | 9.64 | 772.50 | 0.00 | 0.88 | 0 00:00 | 0.00 | 0.00 |
| 86 D6 | Junction | 772.21 | 773.46 | 772.21 | 773.46 | 0.00 | 4.61 | 772.90 | 0.00 | 0.56 | 0 00:00 | 0.00 | 0.00 |
| 87 D900 | Junction | 774.94 | 782.05 | 774.94 | 782.05 | 0.00 | 80.60 | 777.88 | 0.00 | 4.17 | 0 00:00 | 0.00 | 0.00 |
| 88 D904 | Junction | 774.24 | 786.22 | 774.24 | 786.22 | 0.00 | 79.78 | 777.15 | 0.00 | 9.07 | 0 00:00 | 0.00 | 0.00 |
| 89 D905 | Junction | 775.94 | 779.36 | 775.94 | 779.36 | 0.00 | 0.00 | 775.94 | 0.00 | 3.42 | 0 00:00 | 0.00 | 0.00 |
| 90 D906 | Junction | 773.50 | 776.92 | 773.50 | 776.92 | 0.00 | 0.00 | 773.50 | 0.00 | 3.42 | 0 00:00 | 0.00 | 0.00 |
| 91 D907 | Junction | 773.50 | 776.92 | 773.50 | 776.92 | 0.00 | 0.00 | 773.50 | 0.00 | 3.42 | 0 00:00 | 0.00 | 0.00 |
| 92 D910 | Junction | 772.52 | 776.48 | 772.52 | 776.48 | 0.00 | 0.00 | 772.52 | 0.00 | 3.96 | 0 00:00 | 0.00 | 0.00 |
| 93 D911 | Junction | 772.50 | 776.46 | 772.50 | 776.46 | 0.00 | 0.00 | 772.50 | 0.00 | 3.96 | 0 00:00 | 0.00 | 0.00 |
| 94 Out-1D109 TO D110 | Outfall | 771.00 | | | | | 88.84 | 774.11 | | | | | |
| 95 Out-1D125 TO D126 | Outfall | 771.00 | | | | | 43.70 | 773.28 | | | | | |
| 96 Out-1D309 TO D310 | Outfall | 773.50 | | | | | 35.47 | 775.89 | | | | | |
| 97 Out-1D321 TO D322 | Outfall | 773.50 | | | | | 30.74 | 775.61 | | | | | |
| 98 Out-1D333 TO D334 | Outfall | 773.50 | | | | | 40.38 | 775.73 | | | | | |
| 99 Out-1D343 TO D344 | Outfall | 773.50 | | | | | 30.22 | 775.58 | | | | | |
| 100 Out-1D355 TO D354 | Outfall | 773.50 | | | | | 37.01 | 775.29 | | | | | |
| 101 Out-1D904 TO D903 | Outfall | 773.50 | | | | | 79.32 | 776.40 | | | | | |
| 102 Out-1D906 TO D908 | Outfall | 772.83 | | | | | 0.00 | 772.83 | | | | | |
| 103 Out-1D907 TO D909 | Outfall | 772.83 | | | | | 0.00 | 772.83 | | | | | |
| 104 Out-1D910 TO D912 | Outfall | 771.00 | | | | | 0.00 | 771.00 | | | | | |
| 105 Out-1D911 TO D913 | Outfall | 771.00 | | | | | 0.00 | 771.00 | | | | | |
| 106 Out-1PIPE D10 | Outfall | 774.00 | | | | | 4.74 | 774.70 | | | | | |
| 107 Out-1PIPE D12 | Outfall | 774.00 | | | | | 1.65 | 774.39 | | | | | |
| 108 Out-1PIPE D14 | Outfall | 774.50 | | | | | 2.89 | 775.04 | | | | | |
| 109 Out-1PIPE D16 | Outfall | 776.90 | | | | | 3.67 | 777.57 | | | | | |
| 110 Out-1PIPE D2 | Outfall | 771.00 | | | | | 9.54 | 772.11 | | | | | |
| 111 Out-1PIPE D5 | Outfall | 773.00 | | | | | 5.24 | 773.93 | | | | | |
| 112 Out-1PIPE D7 | Outfall | 773.00 | | | | | 1.07 | 773.29 | | | | | |
| 113 Out-1PIPE-D2 | Outfall | 770.39 | | | | | 0.00 | 770.39 | | | | | |

Link Summary

| SN Element ID | Element Type | From (Inlet) Node | To (Outlet) Node | Length Elevation | Inlet Invert | Outlet Invert | Average Slope | Diameter or Height | Manning's Roughness | Peak Flow | Design Flow Capacity | Peak Flow/ Design Flow | Peak Velocity | Peak Depth | Peak Depth/ Total Depth | Total Time Ratio | Reported Condition |
|------------------|-----------------|----------------------|---------------------|---------------------|-----------------|------------------|------------------|-----------------------|------------------------|--------------|-------------------------|---------------------------|---------------|------------|----------------------------|---------------------|-----------------------|
| | | | | | | | | | | | | | | | | | |
| | | | | | (ft) | (ft) | (ft) | (%) | (in) | (cfs) | (cfs) | | (ft/sec) | (ft) | | (min) | |
| 93 PIPE-D2 | Pipe | D1 | Out-1PIPE-D2 | 116.38 | 770.95 | 770.39 | 0.4800 | 36.000 | 0.0130 | 0.00 | 46.34 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 Calculated | |

Junction Input

| SN Element ID | Invert Elevation (ft) | Ground/Rim (Max) Elevation (ft) | Ground/Rim (Max) Offset (ft) | Initial Water Elevation (ft) | Initial Water Depth (ft) | Surcharge Elevation (ft) | Surcharge Depth (ft) | Ponded Area (ft ²) | Minimum Pipe Cover (in) |
|------------------|-----------------------------|--|---------------------------------------|---------------------------------------|-----------------------------------|--------------------------------|----------------------------|--------------------------------------|----------------------------------|
| 1 D1 | 770.95 | 774.78 | 3.83 | 770.95 | 0.00 | 774.78 | 0.00 | 0.00 | 10.00 |
| 2 D10 | 773.41 | 776.76 | 3.36 | 773.41 | 0.00 | 776.76 | 0.00 | 0.00 | 22.28 |
| 3 D109 | 771.46 | 779.12 | 7.66 | 771.46 | 0.00 | 779.12 | 0.00 | 0.00 | 37.94 |
| 4 D11 | 773.69 | 776.39 | 2.69 | 773.69 | 0.00 | 776.39 | 0.00 | 0.00 | 20.34 |
| 5 D111 | 777.10 | 786.60 | 9.50 | 777.10 | 0.00 | 786.60 | 0.00 | 0.00 | 85.42 |
| 6 D112 | 772.70 | 777.00 | 4.30 | 772.70 | 0.00 | 777.00 | 0.00 | 0.00 | 15.59 |
| 7 D113 | 772.38 | 778.29 | 5.92 | 772.38 | 0.00 | 778.29 | 0.00 | 0.00 | 33.80 |
| 8 D114 | 779.59 | 786.43 | 6.84 | 779.59 | 0.00 | 786.43 | 0.00 | 0.00 | 70.10 |
| 9 D115 | 774.75 | 778.17 | 3.42 | 774.75 | 0.00 | 778.17 | 0.00 | 0.00 | 0.00 |
| 10 D116 | 778.80 | 783.61 | 4.81 | 778.80 | 0.00 | 783.61 | 0.00 | 0.00 | 42.69 |
| 11 D117 | 777.54 | 783.61 | 6.07 | 777.54 | 0.00 | 783.61 | 0.00 | 0.00 | 54.83 |
| 12 D118 | 776.10 | 783.03 | 6.93 | 776.10 | 0.00 | 783.03 | 0.00 | 0.00 | 65.20 |
| 13 D119 | 774.03 | 778.45 | 4.42 | 774.03 | 0.00 | 778.45 | 0.00 | 0.00 | 35.05 |
| 14 D120 | 775.18 | 784.31 | 9.13 | 775.18 | 0.00 | 784.31 | 0.00 | 0.00 | 85.58 |
| 15 D121 | 775.48 | 783.69 | 8.21 | 775.48 | 0.00 | 783.69 | 0.00 | 0.00 | 68.55 |
| 16 D122 | 774.64 | 783.58 | 8.94 | 774.64 | 0.00 | 783.58 | 0.00 | 0.00 | 76.04 |
| 17 D123 | 773.46 | 782.80 | 9.34 | 773.46 | 0.00 | 782.80 | 0.00 | 0.00 | 80.85 |
| 18 D124 | 772.68 | 780.83 | 8.15 | 772.68 | 0.00 | 780.83 | 0.00 | 0.00 | 66.57 |
| 19 D125 | 771.63 | 778.45 | 6.82 | 771.63 | 0.00 | 778.45 | 0.00 | 0.00 | 45.82 |
| 20 D127 | 771.99 | 781.48 | 9.48 | 771.99 | 0.00 | 781.48 | 0.00 | 0.00 | 65.81 |
| 21 D128 | 774.27 | 778.24 | 3.97 | 774.27 | 0.00 | 778.24 | 0.00 | 0.00 | 35.70 |
| 22 D129 | 773.77 | 786.06 | 12.29 | 773.77 | 0.00 | 786.06 | 0.00 | 0.00 | 105.51 |
| 23 D13 | 774.66 | 780.46 | 5.80 | 774.66 | 0.00 | 780.46 | 0.00 | 0.00 | 41.46 |
| 24 D130 | 772.88 | 780.33 | 7.45 | 772.88 | 0.00 | 780.33 | 0.00 | 0.00 | 41.42 |
| 25 D14 | 776.29 | 779.98 | 3.69 | 776.29 | 0.00 | 779.98 | 0.00 | 0.00 | 32.30 |
| 26 D18 | 775.55 | 781.61 | 6.07 | 775.55 | 0.00 | 781.61 | 0.00 | 0.00 | 55.95 |
| 27 D19 | 776.51 | 780.29 | 3.78 | 776.51 | 0.00 | 780.29 | 0.00 | 0.00 | 33.34 |
| 28 D200 | 777.00 | 786.35 | 9.35 | 777.00 | 0.00 | 786.35 | 0.00 | 0.00 | 88.23 |
| 29 D201 | 776.57 | 786.77 | 10.20 | 776.57 | 0.00 | 786.77 | 0.00 | 0.00 | 97.19 |
| 30 D202 | 777.30 | 786.22 | 8.92 | 777.30 | 0.00 | 786.22 | 0.00 | 0.00 | 89.08 |
| 31 D203 | 778.04 | 783.88 | 5.84 | 778.04 | 0.00 | 783.88 | 0.00 | 0.00 | 52.04 |
| 32 D21 | 775.55 | 783.72 | 8.17 | 775.55 | 0.00 | 783.72 | 0.00 | 0.00 | 36.93 |
| 33 D22 | 780.20 | 783.72 | 3.52 | 780.20 | 0.00 | 783.72 | 0.00 | 0.00 | 30.22 |
| 34 D24 | 776.28 | 784.17 | 7.89 | 776.28 | 0.00 | 784.17 | 0.00 | 0.00 | 29.47 |
| 35 D25 | 781.06 | 784.47 | 3.40 | 781.06 | 0.00 | 784.47 | 0.00 | 0.00 | 28.85 |
| 36 D29 | 777.47 | 786.63 | 9.15 | 777.47 | 0.00 | 786.63 | 0.00 | 0.00 | 49.51 |
| 37 D30 | 781.74 | 784.81 | 3.07 | 781.74 | 0.00 | 784.81 | 0.00 | 0.00 | 24.83 |
| 38 D300 | 778.58 | 784.16 | 5.58 | 778.58 | 0.00 | 784.16 | 0.00 | 0.00 | 48.96 |
| 39 D301 | 777.60 | 782.42 | 4.82 | 777.60 | 0.00 | 782.42 | 0.00 | 0.00 | 33.85 |
| 40 D302 | 777.06 | 782.16 | 5.10 | 777.06 | 0.00 | 782.16 | 0.00 | 0.00 | 31.24 |
| 41 D303 | 776.64 | 782.16 | 5.53 | 776.64 | 0.00 | 782.16 | 0.00 | 0.00 | 36.32 |
| 42 D304 | 776.22 | 783.56 | 7.34 | 776.22 | 0.00 | 783.56 | 0.00 | 0.00 | 58.07 |
| 43 D305 | 775.80 | 782.16 | 6.37 | 775.80 | 0.00 | 782.16 | 0.00 | 0.00 | 40.38 |
| 44 D306 | 775.45 | 781.71 | 6.26 | 775.45 | 0.00 | 781.71 | 0.00 | 0.00 | 39.10 |
| 45 D307 | 775.26 | 781.71 | 6.45 | 775.26 | 0.00 | 781.71 | 0.00 | 0.00 | 41.39 |
| 46 D308 | 774.93 | 781.17 | 6.23 | 774.93 | 0.00 | 781.17 | 0.00 | 0.00 | 38.80 |
| 47 D309 | 773.99 | 780.25 | 6.26 | 773.99 | 0.00 | 780.25 | 0.00 | 0.00 | 39.16 |
| 48 D31 | 782.21 | 783.88 | 1.67 | 782.21 | 0.00 | 783.88 | 0.00 | 0.00 | 8.00 |
| 49 D312 | 777.89 | 783.92 | 6.02 | 777.89 | 0.00 | 783.92 | 0.00 | 0.00 | 54.28 |
| 50 D313 | 777.67 | 782.83 | 5.16 | 777.67 | 0.00 | 782.83 | 0.00 | 0.00 | 37.92 |
| 51 D314 | 777.06 | 781.63 | 4.57 | 777.06 | 0.00 | 781.63 | 0.00 | 0.00 | 30.82 |
| 52 D315 | 776.64 | 781.64 | 5.01 | 776.64 | 0.00 | 781.64 | 0.00 | 0.00 | 30.07 |
| 53 D316 | 776.22 | 784.29 | 8.08 | 776.22 | 0.00 | 784.29 | 0.00 | 0.00 | 66.91 |
| 54 D317 | 775.80 | 782.89 | 7.10 | 775.80 | 0.00 | 782.89 | 0.00 | 0.00 | 55.15 |
| 55 D318 | 775.45 | 781.74 | 6.29 | 775.45 | 0.00 | 781.74 | 0.00 | 0.00 | 45.48 |
| 56 D319 | 775.26 | 781.60 | 6.35 | 775.26 | 0.00 | 781.60 | 0.00 | 0.00 | 40.15 |
| 57 D320 | 774.93 | 780.62 | 5.68 | 774.93 | 0.00 | 780.62 | 0.00 | 0.00 | 32.18 |
| 58 D321 | 773.99 | 780.50 | 6.51 | 773.99 | 0.00 | 780.50 | 0.00 | 0.00 | 42.16 |
| 59 D324 | 778.58 | 783.17 | 4.59 | 778.58 | 0.00 | 783.17 | 0.00 | 0.00 | 37.05 |
| 60 D325 | 777.60 | 782.70 | 5.09 | 777.60 | 0.00 | 782.70 | 0.00 | 0.00 | 37.09 |
| 61 D326 | 777.06 | 782.42 | 5.36 | 777.06 | 0.00 | 782.42 | 0.00 | 0.00 | 34.36 |
| 62 D327 | 776.64 | 782.41 | 5.78 | 776.64 | 0.00 | 782.41 | 0.00 | 0.00 | 39.33 |
| 63 D328 | 776.11 | 784.01 | 7.90 | 776.11 | 0.00 | 784.01 | 0.00 | 0.00 | 58.83 |
| 64 D329 | 775.80 | 782.41 | 6.62 | 775.80 | 0.00 | 782.41 | 0.00 | 0.00 | 43.41 |
| 65 D330 | 775.45 | 781.96 | 6.51 | 775.45 | 0.00 | 781.96 | 0.00 | 0.00 | 42.15 |

Junction Input

| SN Element ID | Invert Elevation (ft) | Ground/Rim (Max) Elevation (ft) | Ground/Rim (Max) Offset | Initial Water (ft) | Initial Water (ft) | Surcharge Elevation (ft) | Surcharge Depth (ft) | Ponded Area (ft ²) | Minimum Pipe Cover (in) |
|------------------|-----------------------------|--|-------------------------------|--------------------------|--------------------------|--------------------------------|----------------------------|--------------------------------------|----------------------------------|
| 66 D331 | 775.26 | 781.96 | 6.71 | 775.26 | 0.00 | 781.96 | 0.00 | 0.00 | 44.49 |
| 67 D332 | 774.93 | 781.43 | 6.49 | 774.93 | 0.00 | 781.43 | 0.00 | 0.00 | 35.91 |
| 68 D333 | 773.99 | 781.05 | 7.06 | 773.99 | 0.00 | 781.05 | 0.00 | 0.00 | 42.76 |
| 69 D336 | 777.88 | 782.65 | 4.77 | 777.88 | 0.00 | 782.65 | 0.00 | 0.00 | 39.20 |
| 70 D337 | 776.97 | 784.46 | 7.50 | 776.97 | 0.00 | 784.46 | 0.00 | 0.00 | 65.96 |
| 71 D338 | 776.55 | 784.81 | 8.27 | 776.55 | 0.00 | 784.81 | 0.00 | 0.00 | 69.20 |
| 72 D339 | 775.71 | 784.10 | 8.39 | 775.71 | 0.00 | 784.10 | 0.00 | 0.00 | 64.74 |
| 73 D340 | 775.29 | 783.75 | 8.46 | 775.29 | 0.00 | 783.75 | 0.00 | 0.00 | 65.56 |
| 74 D341 | 774.87 | 783.40 | 8.53 | 774.87 | 0.00 | 783.40 | 0.00 | 0.00 | 66.40 |
| 75 D342 | 774.47 | 782.75 | 8.28 | 774.47 | 0.00 | 782.75 | 0.00 | 0.00 | 63.35 |
| 76 D343 | 773.90 | 782.05 | 8.15 | 773.90 | 0.00 | 782.05 | 0.00 | 0.00 | 61.83 |
| 77 D345 | 779.73 | 785.41 | 5.68 | 779.73 | 0.00 | 785.41 | 0.00 | 0.00 | 38.22 |
| 78 D346 | 781.32 | 784.99 | 3.66 | 781.32 | 0.00 | 784.99 | 0.00 | 0.00 | 31.93 |
| 79 D347 | 780.29 | 784.75 | 4.46 | 780.29 | 0.00 | 784.75 | 0.00 | 0.00 | 41.48 |
| 80 D348 | 777.69 | 784.87 | 7.18 | 777.69 | 0.00 | 784.87 | 0.00 | 0.00 | 50.13 |
| 81 D349 | 777.23 | 785.46 | 8.22 | 777.23 | 0.00 | 785.46 | 0.00 | 0.00 | 68.69 |
| 82 D350 | 775.85 | 784.95 | 9.10 | 775.85 | 0.00 | 784.95 | 0.00 | 0.00 | 73.15 |
| 83 D355 | 773.78 | 782.92 | 9.14 | 773.78 | 0.00 | 782.92 | 0.00 | 0.00 | 67.63 |
| 84 D356 | 774.46 | 784.16 | 9.71 | 774.46 | 0.00 | 784.16 | 0.00 | 0.00 | 74.48 |
| 85 D4 | 771.38 | 772.90 | 1.52 | 771.38 | 0.00 | 772.90 | 0.00 | 0.00 | 0.00 |
| 86 D6 | 772.21 | 773.46 | 1.25 | 772.21 | 0.00 | 773.46 | 0.00 | 0.00 | 0.00 |
| 87 D900 | 774.94 | 782.05 | 7.10 | 774.94 | 0.00 | 782.05 | 0.00 | 0.00 | 37.23 |
| 88 D904 | 774.24 | 786.22 | 11.98 | 774.24 | 0.00 | 786.22 | 0.00 | 0.00 | 95.75 |
| 89 D905 | 775.94 | 779.36 | 3.42 | 775.94 | 0.00 | 779.36 | 0.00 | 0.00 | 5.00 |
| 90 D906 | 773.50 | 776.92 | 3.42 | 773.50 | 0.00 | 776.92 | 0.00 | 0.00 | 5.00 |
| 91 D907 | 773.50 | 776.92 | 3.42 | 773.50 | 0.00 | 776.92 | 0.00 | 0.00 | 5.00 |
| 92 D910 | 772.52 | 776.48 | 3.96 | 772.52 | 0.00 | 776.48 | 0.00 | 0.00 | 5.50 |
| 93 D911 | 772.50 | 776.46 | 3.96 | 772.50 | 0.00 | 776.46 | 0.00 | 0.00 | 5.50 |

Junction Results

| SN Element ID | Peak Inflow | Peak Lateral Inflow | Max HGL Attained | Max HGL Attained | Max Surcharge Depth | Min Freeboard Attained | Average HGL Elevation Attained | Average HGL Depth Attained | Time of Max HGL Occurrence | Time of Peak Flooding | Total Flooded | Total Time Volume (ac-in) |
|------------------|----------------|---------------------------|---------------------|---------------------|---------------------------|------------------------------|--------------------------------------|----------------------------------|----------------------------------|-----------------------------|------------------|---------------------------------|
| | Attained | | | | | | | | | | | |
| | (cfs) | (cfs) | (ft) | (ft) | (ft) | (ft) | (ft) | (ft) | (days hh:mm) | (days hh:mm) | (min) | |
| 65 D330 | 28.74 | 3.70 | 777.46 | 2.01 | 0.00 | 4.51 | 775.46 | 0.01 | 0 00:06 | 0 00:00 | 0.00 | 0.00 |
| 66 D331 | 30.90 | 3.00 | 777.37 | 2.11 | 0.00 | 4.59 | 775.27 | 0.01 | 0 00:06 | 0 00:00 | 0.00 | 0.00 |
| 67 D332 | 36.90 | 8.47 | 777.05 | 2.12 | 0.00 | 4.38 | 774.95 | 0.02 | 0 00:06 | 0 00:00 | 0.00 | 0.00 |
| 68 D333 | 40.47 | 6.11 | 776.22 | 2.23 | 0.00 | 4.83 | 774.00 | 0.01 | 0 00:06 | 0 00:00 | 0.00 | 0.00 |
| 69 D336 | 6.20 | 6.20 | 778.93 | 1.05 | 0.00 | 3.72 | 777.89 | 0.01 | 0 00:05 | 0 00:00 | 0.00 | 0.00 |
| 70 D337 | 11.67 | 6.02 | 778.51 | 1.54 | 0.00 | 5.95 | 776.98 | 0.01 | 0 00:05 | 0 00:00 | 0.00 | 0.00 |
| 71 D338 | 19.63 | 8.94 | 778.36 | 1.81 | 0.00 | 6.46 | 776.56 | 0.01 | 0 00:05 | 0 00:00 | 0.00 | 0.00 |
| 72 D339 | 22.65 | 4.22 | 777.49 | 1.78 | 0.00 | 6.61 | 775.72 | 0.01 | 0 00:06 | 0 00:00 | 0.00 | 0.00 |
| 73 D340 | 24.73 | 2.86 | 777.10 | 1.81 | 0.00 | 6.65 | 775.30 | 0.01 | 0 00:06 | 0 00:00 | 0.00 | 0.00 |
| 74 D341 | 26.55 | 2.71 | 776.77 | 1.90 | 0.00 | 6.64 | 774.88 | 0.01 | 0 00:06 | 0 00:00 | 0.00 | 0.00 |
| 75 D342 | 28.51 | 3.18 | 776.46 | 1.99 | 0.00 | 6.29 | 774.48 | 0.01 | 0 00:06 | 0 00:00 | 0.00 | 0.00 |
| 76 D343 | 30.27 | 3.21 | 775.98 | 2.08 | 0.00 | 6.07 | 773.91 | 0.01 | 0 00:07 | 0 00:00 | 0.00 | 0.00 |
| 77 D345 | 16.22 | 14.06 | 780.89 | 1.16 | 0.00 | 4.52 | 780.23 | 0.50 | 0 00:05 | 0 00:00 | 0.00 | 0.00 |
| 78 D346 | 2.31 | 2.31 | 781.91 | 0.59 | 0.00 | 3.07 | 781.33 | 0.01 | 0 00:05 | 0 00:00 | 0.00 | 0.00 |
| 79 D347 | 2.75 | 2.75 | 780.95 | 0.66 | 0.00 | 3.80 | 780.29 | 0.00 | 0 00:05 | 0 00:00 | 0.00 | 0.00 |
| 80 D348 | 19.80 | 1.42 | 779.84 | 2.15 | 0.00 | 5.03 | 779.19 | 1.50 | 0 00:05 | 0 00:00 | 0.00 | 0.00 |
| 81 D349 | 21.27 | 1.62 | 778.60 | 1.37 | 0.00 | 6.86 | 777.24 | 0.01 | 0 00:05 | 0 00:00 | 0.00 | 0.00 |
| 82 D350 | 26.16 | 5.59 | 777.72 | 1.87 | 0.00 | 7.23 | 776.36 | 0.51 | 0 00:05 | 0 00:00 | 0.00 | 0.00 |
| 83 D355 | 37.04 | 2.34 | 775.58 | 1.80 | 0.00 | 7.34 | 773.79 | 0.01 | 0 00:05 | 0 00:00 | 0.00 | 0.00 |
| 84 D356 | 35.13 | 1.96 | 776.41 | 1.95 | 0.00 | 7.76 | 775.62 | 1.16 | 0 00:05 | 0 00:00 | 0.00 | 0.00 |
| 85 D4 | 9.64 | 5.12 | 772.50 | 1.12 | 0.00 | 0.88 | 771.39 | 0.01 | 0 00:05 | 0 00:00 | 0.00 | 0.00 |
| 86 D6 | 4.61 | 4.61 | 772.90 | 0.69 | 0.00 | 0.56 | 772.21 | 0.00 | 0 00:05 | 0 00:00 | 0.00 | 0.00 |
| 87 D900 | 80.60 | 80.60 | 777.88 | 2.94 | 0.00 | 4.17 | 774.97 | 0.03 | 0 00:10 | 0 00:00 | 0.00 | 0.00 |
| 88 D904 | 79.78 | 0.00 | 777.15 | 2.91 | 0.00 | 9.07 | 775.03 | 0.79 | 0 00:10 | 0 00:00 | 0.00 | 0.00 |
| 89 D905 | 0.00 | 0.00 | 775.94 | 0.00 | 0.00 | 3.42 | 775.94 | 0.00 | 0 00:00 | 0 00:00 | 0.00 | 0.00 |
| 90 D906 | 0.00 | 0.00 | 773.50 | 0.00 | 0.00 | 3.42 | 773.50 | 0.00 | 0 00:00 | 0 00:00 | 0.00 | 0.00 |
| 91 D907 | 0.00 | 0.00 | 773.50 | 0.00 | 0.00 | 3.42 | 773.50 | 0.00 | 0 00:00 | 0 00:00 | 0.00 | 0.00 |
| 92 D910 | 0.00 | 0.00 | 772.52 | 0.00 | 0.00 | 3.96 | 772.52 | 0.00 | 0 00:00 | 0 00:00 | 0.00 | 0.00 |
| 93 D911 | 0.00 | 0.00 | 772.50 | 0.00 | 0.00 | 3.96 | 772.50 | 0.00 | 0 00:00 | 0 00:00 | 0.00 | 0.00 |

Pipe Input

| SN Element ID | Length | Inlet Invert Elevation | Inlet Invert Offset | Outlet Invert Elevation | Outlet Invert Offset | Total Drop | Average Slope (%) | Pipe Shape | Pipe Diameter or Height (in) | Pipe Width (in) | Manning's Roughness | Entrance Losses | Exit/Bend Losses | Additional Losses | Initial Flow (cfs) | Flap Gate | No. of Barrels |
|------------------|--------|------------------------------|---------------------------|-------------------------------|----------------------------|---------------|----------------------|---------------|------------------------------------|--------------------|------------------------|--------------------|---------------------|----------------------|-----------------------|-----------|-------------------|
| | (ft) | (ft) | (ft) | (ft) | (ft) | (ft) | (%) | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | |
| 66 D348 TO D349 | 57.06 | 777.69 | 0.00 | 777.23 | 0.00 | 0.46 | 0.8000 | CIRCULAR | 30.000 | 30.000 | 0.0130 | 0.5000 | 0.5000 | 0.0000 | 0.00 | No | 1 |
| 67 D349 TO D350 | 110.00 | 777.23 | 0.00 | 776.35 | 0.50 | 0.88 | 0.8000 | CIRCULAR | 30.000 | 30.000 | 0.0130 | 0.5000 | 0.5000 | 0.0000 | 0.00 | No | 1 |
| 68 D350 TO D356 | 120.00 | 775.85 | 0.00 | 774.89 | 0.44 | 0.96 | 0.8000 | CIRCULAR | 36.000 | 36.000 | 0.0130 | 0.5000 | 0.5000 | 0.0000 | 0.00 | No | 1 |
| 69 D355 TO D354 | 56.70 | 773.78 | 0.00 | 773.50 | 0.00 | 0.28 | 0.5000 | CIRCULAR | 42.000 | 42.000 | 0.0130 | 0.5000 | 0.5000 | 0.0000 | 0.00 | No | 1 |
| 70 D356 TO D355 | 134.48 | 774.46 | 0.00 | 773.78 | 0.00 | 0.67 | 0.5000 | CIRCULAR | 42.000 | 42.000 | 0.0130 | 0.5000 | 0.5000 | 0.0000 | 0.00 | No | 1 |
| 71 D900 TO D904 | 175.29 | 774.94 | 0.00 | 774.24 | 0.00 | 0.70 | 0.4000 | CIRCULAR | 48.000 | 48.000 | 0.0130 | 0.5000 | 0.5000 | 0.0000 | 0.00 | No | 1 |
| 72 D904 TO D903 | 185.55 | 774.24 | 0.00 | 773.50 | 0.00 | 0.74 | 0.4000 | CIRCULAR | 48.000 | 48.000 | 0.0130 | 0.5000 | 0.5000 | 0.0000 | 0.00 | No | 1 |
| 73 D905 TO D904 | 92.59 | 775.94 | 0.00 | 775.02 | 0.78 | 0.93 | 1.0000 | CIRCULAR | 36.000 | 36.000 | 0.0130 | 0.5000 | 0.5000 | 0.0000 | 0.00 | No | 1 |
| 74 D906 TO D908 | 195.02 | 773.50 | 0.00 | 772.83 | 0.00 | 0.67 | 0.3400 | CIRCULAR | 36.000 | 36.000 | 0.0130 | 0.5000 | 0.5000 | 0.0000 | 0.00 | No | 1 |
| 75 D907 TO D909 | 194.94 | 773.50 | 0.00 | 772.83 | 0.00 | 0.67 | 0.3400 | CIRCULAR | 36.000 | 36.000 | 0.0130 | 0.5000 | 0.5000 | 0.0000 | 0.00 | No | 1 |
| 76 D910 TO D912 | 258.62 | 772.52 | 0.00 | 771.00 | 0.00 | 1.52 | 0.5900 | CIRCULAR | 42.000 | 42.000 | 0.0130 | 0.5000 | 0.5000 | 0.0000 | 0.00 | No | 1 |
| 77 D911 TO D913 | 258.78 | 772.50 | 0.00 | 771.00 | 0.00 | 1.50 | 0.5800 | CIRCULAR | 42.000 | 42.000 | 0.0130 | 0.5000 | 0.5000 | 0.0000 | 0.00 | No | 1 |
| 78 PIPE D10 | 103.09 | 775.55 | 0.00 | 774.00 | 0.00 | 1.55 | 1.5000 | CIRCULAR | 15.000 | 15.000 | 0.0130 | 0.5000 | 0.5000 | 0.0000 | 0.00 | No | 1 |
| 79 PIPE D11 | 55.92 | 776.51 | 0.00 | 775.95 | 0.41 | 0.56 | 1.0000 | CIRCULAR | 12.000 | 12.000 | 0.0130 | 0.5000 | 0.5000 | 0.0000 | 0.00 | No | 1 |
| 80 PIPE D12 | 103.17 | 775.55 | 0.00 | 774.00 | 0.00 | 1.55 | 1.5000 | CIRCULAR | 15.000 | 15.000 | 0.0130 | 0.5000 | 0.5000 | 0.0000 | 0.00 | No | 1 |
| 81 PIPE D13 | 55.93 | 780.20 | 0.00 | 779.64 | 4.10 | 0.56 | 1.0000 | CIRCULAR | 12.000 | 12.000 | 0.0130 | 0.5000 | 0.5000 | 0.0000 | 0.00 | No | 1 |
| 82 PIPE D14 | 88.78 | 776.28 | 0.00 | 774.50 | 0.00 | 1.78 | 2.0000 | CIRCULAR | 12.000 | 12.000 | 0.0130 | 0.5000 | 0.5000 | 0.0000 | 0.00 | No | 1 |
| 83 PIPE D15 | 70.43 | 781.06 | 0.00 | 780.71 | 4.44 | 0.35 | 0.5000 | CIRCULAR | 12.000 | 12.000 | 0.0130 | 0.5000 | 0.5000 | 0.0000 | 0.00 | No | 1 |
| 84 PIPE D16 | 55.01 | 777.47 | 0.00 | 776.90 | 0.00 | 0.57 | 1.0400 | CIRCULAR | 15.000 | 15.000 | 0.0130 | 0.5000 | 0.5000 | 0.0000 | 0.00 | No | 1 |
| 85 PIPE D17 | 58.24 | 781.74 | 0.00 | 781.46 | 3.98 | 0.28 | 0.4800 | CIRCULAR | 12.000 | 12.000 | 0.0130 | 0.5000 | 0.5000 | 0.0000 | 0.00 | No | 1 |
| 86 PIPE D2 | 76.01 | 771.38 | 0.00 | 771.00 | 0.00 | 0.38 | 0.5000 | CIRCULAR | 24.000 | 24.000 | 0.0130 | 0.5000 | 0.5000 | 0.0000 | 0.00 | No | 1 |
| 87 PIPE D3 | 55.52 | 772.21 | 0.00 | 771.38 | 0.00 | 0.83 | 1.4900 | CIRCULAR | 15.000 | 15.000 | 0.0130 | 0.5000 | 0.5000 | 0.0000 | 0.00 | No | 1 |
| 88 PIPE D5 | 81.00 | 773.41 | 0.00 | 773.00 | 0.00 | 0.41 | 0.5000 | CIRCULAR | 18.000 | 18.000 | 0.0130 | 0.5000 | 0.5000 | 0.0000 | 0.00 | No | 1 |
| 89 PIPE D6 | 57.80 | 773.69 | 0.00 | 773.41 | 0.00 | 0.29 | 0.5000 | CIRCULAR | 12.000 | 12.000 | 0.0130 | 0.5000 | 0.5000 | 0.0000 | 0.00 | No | 1 |
| 90 PIPE D7 | 83.06 | 774.66 | 0.00 | 773.00 | 0.00 | 1.66 | 2.0000 | CIRCULAR | 15.000 | 15.000 | 0.0130 | 0.5000 | 0.5000 | 0.0000 | 0.00 | No | 1 |
| 91 PIPE D8 | 55.87 | 776.29 | 0.00 | 776.01 | 1.35 | 0.28 | 0.5000 | CIRCULAR | 12.000 | 12.000 | 0.0130 | 0.5000 | 0.5000 | 0.0000 | 0.00 | No | 1 |
| 92 PIPE-33 | 71.16 | 782.21 | 0.00 | 781.50 | 4.03 | 0.71 | 1.0000 | CIRCULAR | 12.000 | 12.000 | 0.0130 | 0.5000 | 0.5000 | 0.0000 | 0.00 | No | 1 |
| 93 PIPE-D2 | 116.38 | 770.95 | 0.00 | 770.39 | 0.00 | 0.56 | 0.4800 | CIRCULAR | 36.000 | 36.000 | 0.0130 | 0.5000 | 0.5000 | 0.0000 | 0.00 | No | 1 |

Pipe Results

| SN Element ID | Peak Flow | Time of Occurrence | Design Flow Capacity | Peak Flow/ Design Flow | Peak Velocity | Travel Time | Peak Depth | Peak Depth/ Total Depth | Total Time | Froude Number | Reported Condition |
|------------------|--------------|-----------------------|-------------------------|---------------------------|---------------|----------------|------------|----------------------------|------------|------------------|-----------------------|
| | | | | Ratio | | | Ratio | | | | |
| | (cfs) | (days hh:mm) | (cfs) | | (ft/sec) | (min) | (ft) | | (min) | | |
| 65 D347 TO D348 | 2.69 | 0 00:05 | 3.56 | 0.75 | 7.53 | 0.24 | 0.65 | 0.65 | 0.00 | Calculated | |
| 66 D348 TO D349 | 19.78 | 0 00:05 | 36.69 | 0.54 | 7.63 | 0.12 | 1.31 | 0.52 | 0.00 | Calculated | |
| 67 D349 TO D350 | 21.17 | 0 00:05 | 36.69 | 0.58 | 7.80 | 0.24 | 1.36 | 0.54 | 0.00 | Calculated | |
| 68 D350 TO D356 | 26.08 | 0 00:05 | 59.66 | 0.44 | 8.22 | 0.24 | 1.39 | 0.46 | 0.00 | Calculated | |
| 69 D355 TO D354 | 37.01 | 0 00:06 | 71.14 | 0.52 | 7.48 | 0.13 | 1.79 | 0.51 | 0.00 | Calculated | |
| 70 D356 TO D355 | 35.06 | 0 00:05 | 71.14 | 0.49 | 7.44 | 0.30 | 1.73 | 0.50 | 0.00 | Calculated | |
| 71 D900 TO D904 | 79.78 | 0 00:10 | 90.85 | 0.88 | 10.64 | 0.27 | 2.90 | 0.73 | 0.00 | Calculated | |
| 72 D904 TO D903 | 79.32 | 0 00:10 | 90.85 | 0.87 | 8.22 | 0.38 | 2.89 | 0.72 | 0.00 | Calculated | |
| 73 D905 TO D904 | 0.00 | 0 00:00 | 66.70 | 0.00 | 0.00 | | 0.00 | 0.00 | 0.00 | Calculated | |
| 74 D906 TO D908 | 0.00 | 0 00:00 | 39.09 | 0.00 | 0.00 | | 0.00 | 0.00 | 0.00 | Calculated | |
| 75 D907 TO D909 | 0.00 | 0 00:00 | 39.10 | 0.00 | 0.00 | | 0.00 | 0.00 | 0.00 | Calculated | |
| 76 D910 TO D912 | 0.00 | 0 00:00 | 77.13 | 0.00 | 0.00 | | 0.00 | 0.00 | 0.00 | Calculated | |
| 77 D911 TO D913 | 0.00 | 0 00:00 | 76.60 | 0.00 | 0.00 | | 0.00 | 0.00 | 0.00 | Calculated | |
| 78 PIPE D10 | 4.74 | 0 00:05 | 7.91 | 0.60 | 6.80 | 0.25 | 0.70 | 0.56 | 0.00 | Calculated | |
| 79 PIPE D11 | 2.09 | 0 00:05 | 3.56 | 0.59 | 6.09 | 0.15 | 0.55 | 0.55 | 0.00 | Calculated | |
| 80 PIPE D12 | 1.65 | 0 00:05 | 7.91 | 0.21 | 5.14 | 0.33 | 0.39 | 0.31 | 0.00 | Calculated | |
| 81 PIPE D13 | 0.77 | 0 00:05 | 3.56 | 0.22 | 4.96 | 0.19 | 0.31 | 0.31 | 0.00 | Calculated | |
| 82 PIPE D14 | 2.89 | 0 00:05 | 5.04 | 0.57 | 6.68 | 0.22 | 0.54 | 0.54 | 0.00 | Calculated | |
| 83 PIPE D15 | 1.15 | 0 00:05 | 2.52 | 0.46 | 4.66 | 0.25 | 0.47 | 0.47 | 0.00 | Calculated | |
| 84 PIPE D16 | 3.67 | 0 00:05 | 6.59 | 0.56 | 5.54 | 0.17 | 0.67 | 0.53 | 0.00 | Calculated | |
| 85 PIPE D17 | 1.50 | 0 00:05 | 2.47 | 0.61 | 4.71 | 0.21 | 0.56 | 0.56 | 0.00 | Calculated | |
| 86 PIPE D2 | 9.54 | 0 00:05 | 16.00 | 0.60 | 5.36 | 0.24 | 1.11 | 0.56 | 0.00 | Calculated | |
| 87 PIPE D3 | 4.57 | 0 00:05 | 7.90 | 0.58 | 7.98 | 0.12 | 0.68 | 0.55 | 0.00 | Calculated | |
| 88 PIPE D5 | 5.24 | 0 00:05 | 7.43 | 0.70 | 4.60 | 0.29 | 0.93 | 0.62 | 0.00 | Calculated | |
| 89 PIPE D6 | 2.42 | 0 00:05 | 2.52 | 0.96 | 5.26 | 0.18 | 0.78 | 0.78 | 0.00 | Calculated | |
| 90 PIPE D7 | 1.07 | 0 00:05 | 9.14 | 0.12 | 5.01 | 0.28 | 0.29 | 0.23 | 0.00 | Calculated | |
| 91 PIPE D8 | 0.43 | 0 00:05 | 2.52 | 0.17 | 3.61 | 0.26 | 0.28 | 0.28 | 0.00 | Calculated | |
| 92 PIPE-33 | 1.06 | 0 00:05 | 3.56 | 0.30 | 5.60 | 0.21 | 0.37 | 0.37 | 0.00 | Calculated | |
| 93 PIPE-D2 | 0.00 | 0 00:00 | 46.34 | 0.00 | 0.00 | | 0.00 | 0.00 | 0.00 | Calculated | |

Appendix G: Complete Master Plan Drainage Report

Malarkey IND
Stormwater Management
3540 Essex Drive
Franklin, Indiana

Drainage Report

Prepared For:
Cooper & Associates
2200 Ellis Drive
New Lenox, IL 60451

Prepared By:
Kimley-Horn and Associates, Inc.
500 East 96th Street, Suite 300
Indianapolis, IN 46240
Phone: (317) 218-9560

Original: July 11th, 2024
Revised: August 9th, 2024

Kimley»Horn

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1.0. Project Summary

| | |
|--------------------------|--|
| Project Name: | Malarkey IND |
| Location: | 3540 Essex Drive, Franklin, Johnson County, Indiana |
| Type: | Drainage Report |
| Reviewing Agency: | City of Franklin & Johnson County |
| Detention Policy: | City of Franklin & Johnson County |
| Water Quality: | City of Franklin & Johnson County |
| Water Quantity Modeling: | HydroCAD with SCS Type II & Indianapolis Huff Distribution |
| Storm Sewer Modeling: | N/A (Future) |

Design:

| | |
|-----------------|---------------------|
| Water Quantity: | Wet Detention Basin |
| Water Quality: | Wet Detention Basin |
| Receiving Body: | Graham Arm |

2.0. Introduction

Kimley-Horn and Associates, Inc. has been retained by Cooper & Associates LLC to prepare construction documents and provide civil engineering services for the proposed industrial development for Malarkey Roofing Product as the Owner and end user (Project). The Project includes the development of approximately 138 acres of agricultural land to the north and west of Essex Drive in Franklin, Indiana. The project includes the planned construction of an approximately 353,300 SF industrial building with associated drives, parking, rail spur and substantial outdoor product storing spaces. The project also includes a 4,110 LF roadway extension of Essex Drive, connecting to Paul Hand Blvd. The extension will become the east frontage of the Malarkey site and will include sanitary sewer and water main extensions along with three entrances. It is anticipated that this private road will ultimately be shared as the lot(s) to the east develop on its own. 90' right of way will be dedicated to the City for Essex Drive. Utility services will be brought from extended infrastructure off Essex Drive and Paul Hand Blvd where applicable. Stormwater detention and quality measures will be provided in the form of a wet detention pond at the south of the site. The project will be broken down into two phases. The first being the mass grading and pond excavation. The second being the final buildout and Essex Drive extension.

This Drainage Report focuses on the mass grading phase while master planning for the fully developed condition. The design will incorporate the existing and planned proposed conditions onsite and offsite and provide supporting calculations for storm sewer, detention basin, and stormwater quality best management practice (BMP) sizing based on the *City of Franklin Stormwater Management Ordinance* and *Johnson County Stormwater Technical Standards Manual (Version 1.0 - 2023)* whichever is more stringent.

3.0. Existing Conditions

The existing site is currently undeveloped and is used for agricultural purposes. The adjacent property to the north, east and west are similar in nature. The property to the south is an existing industrial complex. The 138-acre tract of property is generally divided into three different drainage directions although all ultimately end into the same receiving body of water, Graham Arm. The main portion (114.95 acres) drains toward an on-site ephemeral drainage feature up the middle going N-S toward the existing patch of trees that have been partially classified as isolated wetlands. The second basin is a small portion (5.64 acres) at the northwest corner of the parcel that drains directly into Graham Arm regulated drain via an existing 24" culvert under the railroad tracks. The remaining portion (13.66 acres) along the east of the site drain east into Canary Ditch. In addition, there is a substantial offsite area (67.65 acres) entering the site from the north via a 12" CMP culvert under Paul Hand Blvd. Refer to **Appendix D** for the Existing Drainage Map.

Aerial Photograph

An aerial photograph of the Project Site has been included in **Appendix A** for reference.

FEMA

The Project Site is located on the Flood Insurance Rate Map number 18081C0139E (dated 1/29/2021) and 18081C0137D (date 8/2/2007) concluded that the site lies in Zone X which is the area of minimal flood hazard and outside the 100-Yr Flood Hazard zones. See **Appendix B** for the FEMA FIRMette.

Soil Characteristics

The Natural Resources Conservation Service (NRCS) Web Soil Survey of Johnson County, Indiana, indicates Brookston silty clay loam and Crosby silt loam on site. A soil map can be found in **Appendix C**.

4.0. Proposed Conditions

General Storm Routing & Provided Detention

During final buildout, it is anticipated that the proposed building, associated pavement areas, rail spurs, and Essex Drive extension will be constructed on the 138 AC+/- site. A part of the paved area will be deferred for future construction/expansion. However, the entire site in fully developed condition will be assumed for the stormwater management design. A set of interconnected wet and extended dry detention ponds will be designed to provide adequate detention for the developed site including Essex Drive to its full buildout condition while also adequately conveying off-site drainage from the north. For the mass grading phase, the proposed ponds will be located to the east of the proposed site, excavated in their entirety. An exception to this is the ponds will be connected via interim swales to eventually be filled in and replaced with culverts during final buildout. The outfall point for the pond will be located to the southwest of the south wet pond. The outfall will route detained discharge from the pond to the existing Graham Arm along the west property line, east of the rail right of way. In the interim condition, the site will overland drain via sheet flow to the closest available pond. During final buildout, proposed storm sewers will be designed to collect surface and roof runoff and route it to the said pond. Said design

will be presented with the drainage memorandum to be developed along with final calculations of the basins to confirm master planned assumptions. Refer to **Appendix E** for the Proposed Drainage Map.

Proposed Hydrology

HydroCAD was utilized to size the detention ponds. HydroCAD utilizes areas, runoff curve numbers, times of concentration and rainfall data to calculate runoff hydrographs utilizing the NRCS TR-20 methodology. There are two applicable stormwater ordinances to design to, therefore presented respectively.

Per the *City of Franklin Stormwater Management Ordinance*, utilizing the Huff distribution, the storm water detention design shall outlet storm water at a 2-year pre-development rainfall event rate for a 10-year post-development storm and shall outlet at a 10-year pre-development rainfall event rate for a 100-year post-development storm. Utilizing the 114.95 acres onsite contributing basin, curve number CN of 74 (Pasture/Grassland/Range, Good condition) and calculated time concentration (Tc) of 141.1 minutes. The allowable release rates are 12.28 cfs and 25.42 cfs for the 10-year and 100-year storms respectively.

Per Johnson County's *Stormwater Technical Standards Manual*, utilizing the SCS Type II rainfall distribution, the storm water detention designs shall outlet storm water at 0.1 and 0.3 cfs per acre of development area for 10-year and 100-year post-development rainfall respectively. At 114.95 acres, the allowable release rates set by the County are 11.49 cfs and 34.48 cfs as the allowable release rates.

As presented above in addition to the use of SCS Type II vs Huff rainfall distribution, this concludes that both set of ordinances are more stringent than each other in certain ways therefore the need to present both results. Since the south pond will outfall directly into the existing ditch at or less than the current condition, there will be no downstream restrictions to consider, therefore the allowable release rates will not be reduced.

The interconnected proposed detention ponds for this project have been sized to provide rate control for the entire 138-acre developments of the project site including Essex Drive. In addition, the ponds have been oversized to accommodate 67.65 AC of offsite runoff in current condition from the north to bypass through the pond until that area is developed and assumingly their own detention pond is provided. A composite curve number of 95 was assumed for all of the on-site basins, 92 for the ROW area and 74 for the undeveloped off-site drainage area.

The normal pools of each pond were set to ensure positive drainage to their respective outfall. The south pond was set to ensure positive drainage to be at or above Graham Arm's active channel by having the outgoing pipe's crown at or above the existing shelf. The ultimate release rate from the south pond will be controlled by two orifices. The invert of the first, 17" diameter, orifice will be set at the normal pool elevation of 771.50. The invert of the second orifice, one 40"Wx24H" rectangular, will be set the elevation of 774.25. The table below summarizes the water surface elevations and release rates for the pond. Refer to **Appendix F** for detailed HydroCAD calculations.

Summary of Wet Pond 1 (South) Performance without Off-site Bypass

| Wet Pond 1 (South) | Peak 10-YR Release Rate (cfs) | Peak 10-YR Water Surface Elevation | Peak 100-YR Release Rate (cfs) | Peak 100-YR Water Surface Elevation | T/Berm |
|--|-------------------------------------|---|--------------------------------------|---|--------------|
| Allowable (City) | 12.28 | N/A | 25.42 | N/A | 2' Freeboard |
| Allowable (County) | 11.49 | N/A | 34.48 | N/A | 1' Freeboard |
| <i>SCS Type 2 Distribution</i> | 10.98 | 774.28 | 25.10 | 775.31 | 778.51 |
| <i>Huff Distribution (Highest of 24Hr, 1Q, 2Q, 3Q)</i> | 10.99 | 774.28 | 24.05 | 775.26 | 778.51 |

Summary of Wet Pond 1 (South) Performance with Off-site Bypass

| Wet Pond 1 (South) | Peak 10-YR Release Rate (cfs) | Peak 10-YR Water Surface Elevation | Peak 100-YR Release Rate (cfs) | Peak 100-YR Water Surface Elevation | T/Berm |
|--|-------------------------------------|---|--------------------------------------|---|--------|
| <i>SCS Type 2 Distribution</i> | 16.14 | 774.77 | 39.70 | 776.01 | 778.51 |
| <i>Huff Distribution (Highest of 24Hr, 1Q, 2Q, 3Q)</i> | 16.66 | 774.81 | 37.62 | 775.92 | 778.51 |

The emergency overflow weir was designed using 1.25 times the maximum flow into the pond. As seen in **Appendix F** of this report, the highest peak 100-Yr flow with offsite into the pond is 418 CFS resulting in the design flow rate for the overflow weir to be 522.5 cfs. A 335-ft wide trapezoidal weir and 6" height was modeled with a 3:1 side slope on both sides to the west, toward Graham Arm. The spillway is designed to be set at 776.01. The resulting maximum overflow elevation is 776.51. The top of bank is set at 778.51 in order to provide the minimum required two feet of freeboard above the top of spillway elevation. The top casting of the outlet control structure will also be set at 776.01 in order to act in clogging situations. All building foundations are set to a minimum 2.0-ft above the overflow elevation. Weir calculations can be found shown in **Appendix F**.

Proposed Hydraulics

The drainage report of the final buildout will present the hydraulic calculations for all on-site storm sewer. It will be required that all the HGL of the 10-yr storm be kept below the proposed rim elevations of each structure. Rainfall intensities and 'c' values to be taken from the *City of Franklin Stormwater Management Ordinance*. The storm sewers are to be designed to maintain a minimum full flow velocity of 2.5 ft/s. The outfall pipe was sized to the highest resulting peak release rate out of the south pond which is 39.70 with offsite. See **Appendix G** for calculations.

Stormwater Quality

Stormwater quality treatment for the project site will be accomplished by routing onsite flow through the proposed detention pond. According to the City of Franklin Subdivisions Standards, "The developer shall be required to provide a water quality detention system that is designed to detain, for over 24 hours after peak run-off from a 24-hour storm, at least 20% of the run-off from either a 1-1/4 inch storm or ½ inch of direct runoff, whichever is greater." With this condition, it is required that the pond have a water quality design volume of 57,896 cubic-feet. It was determined that the available stormwater quality volume is 2,583,071 cubic-feet. See below for detailed calculations and **Appendix H** for HydroCAD outputs.

Scenario 1: South Pond area = 492,794 SF x ½" / 12"/Ft = 20,533 CF

Scenario 2: Highest WQV event per HydroCAD = 289,482 CF (0.17 Hr) x 0.20 = **57,896 CF**

Total Detention Volume = 2,872,553 CF

2,872,553 CF – 289,482 CF = 2,583,071 CF available.

5.0 Appendices

Appendix A: Aerial Photograph



Appendix B: FEMA Flood Insurance Rate Map

NOTES TO USERS

This map is for use in administering the National Flood Insurance Program. It does not necessarily identify all areas subject to flooding, particularly from local drainage sources of small size. The **community map repository** should be consulted for possible updated or additional flood hazard information.

To obtain more detailed information in areas where **Base Flood Elevations** (BFEs) and/or **floodways** have been determined, users are encouraged to consult the Flood Profiles and Floodway Data and/or Summary of Stillwater Elevations tables contained within the Flood Insurance Study (FIS) Report that accompanies this FIRM. Users should be aware that BFEs shown on this FIRM represent rounded whole-foot elevations. These BFEs are intended for flood insurance rating purposes only and should not be used as the sole source of flood elevation information. Accordingly, flood elevation data presented in the FIS Report should be utilized in conjunction with the FIRM for purposes of construction and/or floodplain management.

Boundaries of the **floodways** were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway widths and other pertinent floodway data are provided in the Flood Insurance Study Report for this jurisdiction.

Certain areas not in Special Flood Hazard Areas may be protected by **flood control structures**. Refer to Section 2.4 "Flood Protection Measures" of the Flood Insurance Study Report for information on flood control structures for this jurisdiction.

The projection used in the preparation of this map was Indiana State Plane East Zone FIPS zone 1301. The horizontal datum was NAD 83, GRS 1980 ellipsoid. Differences in datum, spheroid, projection or UTM zones used in the production of FIRMs for adjacent jurisdictions may result in slight positional differences in map features across jurisdiction boundaries. These differences do not affect the accuracy of this FIRM.

Flood elevations on this map are referenced to the North American Vertical Datum of 1988. These flood elevations must be compared to structure and ground elevations referenced to the same **vertical datum**. For information regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1988, visit the National Geodetic Survey website at <http://www.ngs.noaa.gov> or contact the National Geodetic Survey at the following address:

NGS Information Services
NOAA/NGS12
National Geodetic Survey
SSMC-3, #9202
1315 East-West Highway
Silver Spring, Maryland 20910-3262
(301) 713-3242

To obtain current elevation, description, and/or location information for **bench marks** shown on this map, please contact the Information Services Branch of the National Geodetic Survey at (301) 713-3242, or visit its website at <http://www.ngs.noaa.gov>.

Base map information shown on this FIRM was derived from the 2005 Indiana Orthophotography (IndianaMap Framework Data www.indianamap.org). This information was photogrammetrically compiled at a scale of 1:2400 from aerial photography dated spring 2005. Aerial Photography shown on the FIRM is from 2018 provided by Johnson County.

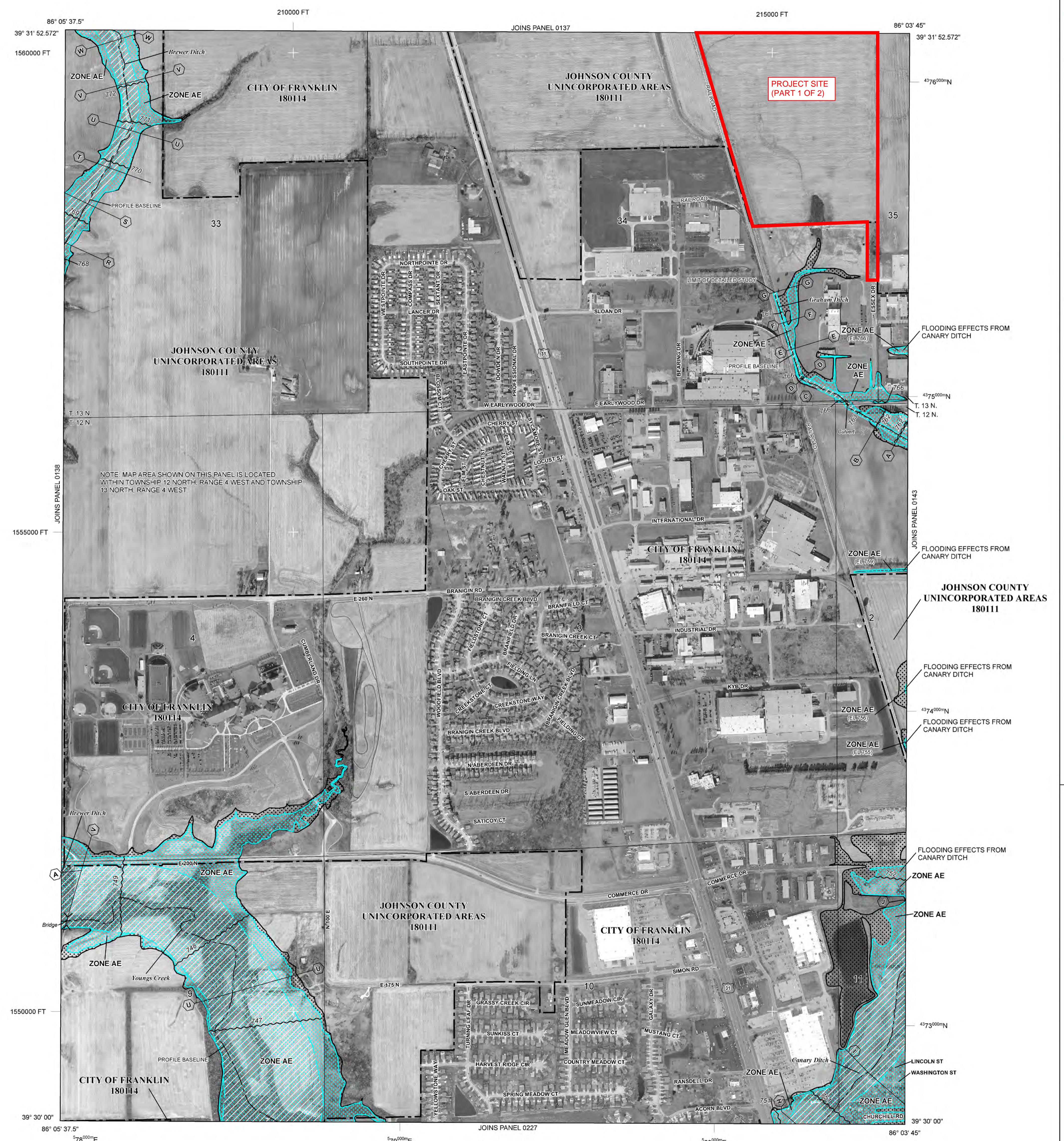
The **profile baselines** depicted on this map represent the hydraulic modeling baselines that match the flood profiles in the FIS report. As a result of improved topographic data, the **profile baseline**, in some cases, may deviate significantly from the channel centerline or appear outside the SFHA.

Corporate limits shown on this map are based on the best data available at the time of publication. Because changes due to annexations or de-annexations may have occurred after this map was published, map users should contact appropriate community officials to verify current corporate limit locations.

Please refer to the separately printed **Map Index** for an overview map of the county showing the layout of map panels; community map repository addresses; and a Listing of Communities table containing National Flood Insurance Program dates for each community as well as a listing of the panels on which each community is located.

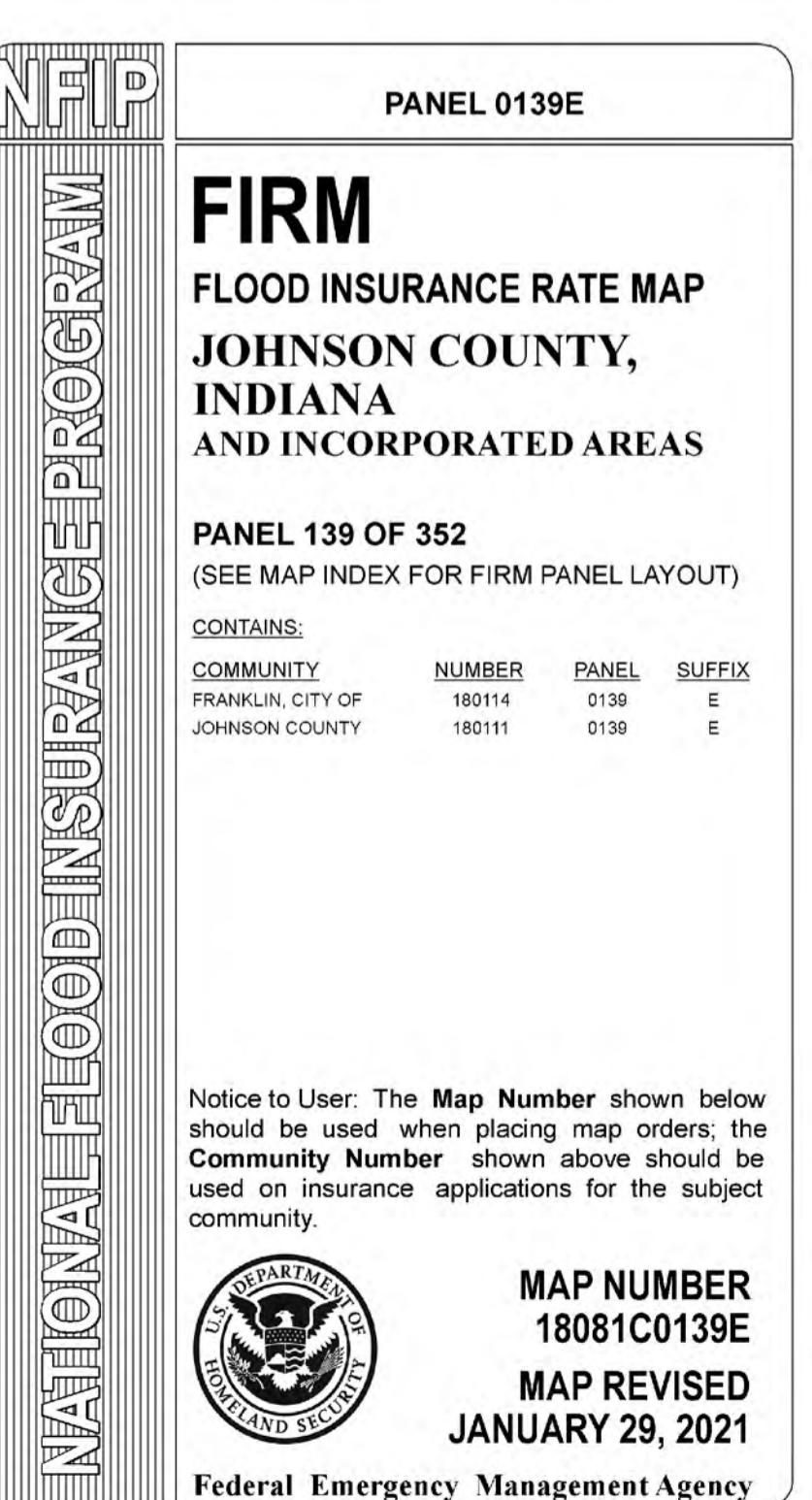
For information on available products associated with this FIRM visit the **Map Service Center (MSC)** website at <http://msc.fema.gov>. Available products may include previously issued Letters of Map Change, a Flood Insurance Study Report, and/or digital versions of this map. Many of these products can be ordered or obtained directly from the MSC website.

If you have questions about this map, how to order products, or the National Flood Insurance Program in general, please call the **FEMA Map Information eXchange (FMIX)** at 1-877-FEMA-MAP (1-877-336-2627) or visit the FEMA website at <http://www.fema.gov/business/nfip>.



LEGEND

| | |
|---|---|
| | SPECIAL FLOOD HAZARD AREAS (SFHAs) SUBJECT TO INUNDATION BY THE 1% ANNUAL CHANCE FLOOD |
| The 1% annual chance flood (100-year flood), also known as the base flood, is the flood that has a 1% chance of being equaled or exceeded in any given year. The Special Flood Hazard Area is the area subject to flooding by the 1% annual chance flood. Areas of Special Flood Hazard include Zones A, AE, AH, AO, AR, A99, V, and VE. The Base Flood Elevation is the water-surface elevation of the 1% annual chance flood. | |
| ZONE A | No Base Flood Elevations determined. |
| ZONE AE | Base Flood Elevations determined. |
| ZONE AH | Flood depths of 1 to 3 feet (usually areas of ponding); Base Flood Elevations determined. |
| ZONE AO | Flood depths of 1 to 3 feet (usually sheet flow on sloping terrain); average depths determined. For areas of alluvial fan flooding, velocities also determined. |
| ZONE AR | Special Flood Hazard Areas formerly protected from the 1% annual chance flood by a flood control system that was subsequently decertified. Zone AR indicates that the former flood control system is being restored to provide protection from the 1% annual chance or greater flood. |
| ZONE A99 | Area to be protected from 1% annual chance flood by a Federal flood protection system under construction, no Base Flood Elevations determined. |
| ZONE V | Coastal flood zone with velocity hazard (wave action); no Base Flood Elevations determined. |
| ZONE VE | Coastal flood zone with velocity hazard (wave action); Base Flood Elevations determined. |
| | FLOODWAY AREAS IN ZONE AE |
| The floodway is the channel of a stream plus any adjacent floodplain areas that must be kept free of encroachment so that the 1% annual chance flood can be carried without substantial increases in flood heights. | |
| | OTHER FLOOD AREAS |
| Area of 0.2% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 foot, or drainage areas less than 1 square mile; and areas protected by levees from 1% annual chance flood. | |
| | OTHER AREAS |
| Areas determined to be outside the 0.2% annual chance floodplain. | |
| | COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS |
| | OTHERWISE PROTECTED AREAS (OPAs) |
| CBRS areas and OPAs are normally located within or adjacent to Special Flood Hazard Areas. | |
| 1% Annual Chance Floodplain Boundary | |
| Floodway boundary | |
| Zone D boundary | |
| CBRS and OPA boundary | |
| Boundary dividing Special Flood Hazard Area Zones and boundary dividing Special Flood Hazard Areas of different Base Flood Elevations, flood depths, or flood velocities. | |
| Base Flood Elevation line and value; elevation in feet* | |
| Base Flood Elevation value where uniform within zone; elevation in feet* | |
| *Referenced to the North American Vertical Datum of 1988 | |
| Geographic coordinates referenced to the North American Datum of 1983 (NAD 83) Western Hemisphere. | |
| 500-foot ticks: Indiana State Plane East Zone | |
| FIPS Zone 1301, Transverse Mercator projection | |
| 100-meter Universal Transverse Mercator grid values, zone 16 | |
| Bench mark (see explanation in Notes to Users section of this FIRM panel) | |
| River Mile | |
| MAP REPOSITORIES | |
| Refer to Map Repositories list on Map Index. | |
| EFFECTIVE DATE OF COUNTYWIDE FLOOD INSURANCE RATE MAP | |
| August 2, 2007 | |
| EFFECTIVE DATE(S) OF REVISION(S) TO THIS PANEL | |
| January 29, 2021 - to increase Base Flood Elevations and to change Special Flood Hazard Areas. | |



Federal Emergency Management Agency

NOTES TO USERS

This map is for use in administering the National Flood Insurance Program. It does not necessarily identify all areas subject to flooding, particularly from local drainage sources of small size. The community map repository should be consulted for possible updated or additional flood hazard information.

To obtain more detailed information in areas where Base Flood Elevations (BFEs) and/or floodways have been determined, users are encouraged to consult the Flood Profiles and Floodway Data and/or Summary of Stillwater Elevation tables contained within the Flood Insurance Study (FIS) report that accompanies this FIRM. Users should be aware that BFEs shown on the FIRM represent rounded whole-foot elevations. These BFEs are intended for flood insurance purposes and should not be used as the sole source of flood elevation information. Accordingly, flood elevation data presented in the FIS report should be utilized in conjunction with the FIRM for purposes of construction and/or floodplain management.

Coastal Base Flood Elevations shown on this map apply only landward of 0' North American Vertical Datum of 1988 (NAVD 88). Users of this FIRM should be aware that coastal flood elevations are also provided in the Summary of Stillwater Elevations table in the Flood Insurance Study report for this jurisdiction. Elevation shown in the Summary of Stillwater Elevations table should be used for construction and/or floodplain management purposes when they are higher than the elevations shown on this FIRM.

Boundaries of the floodways were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway widths and other pertinent floodway data are provided in the Flood Insurance Study report for this jurisdiction.

Certain areas not in Special Flood Hazard Areas may be protected by flood control structures. Refer to Section 2.4 "Flood Protection Measures" of the Flood Insurance Study report for information on flood control structures for this jurisdiction.

The projection used in the preparation of this map was Indiana State Plane East zone 3826 (FIPSZONE 1301). The horizontal datum was NAD83. Differences in datum, spheroid, projection or state plane zones used in the production of FIRMs for adjacent jurisdictions may result in slight positional differences in map features across jurisdiction boundaries. These differences do not affect the accuracy of this FIRM.

Flood elevations on this map are referenced to the North American Vertical Datum of 1988. These flood elevations must be compared to structure and ground elevations referenced to the same vertical datum. For information regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1988, visit the National Geodetic Survey website at <http://www.ngs.noaa.gov/> or contact the National Geodetic Survey at the following address:

NGS Information Services
NOAA, NNGS12
National Geodetic Survey
SSMC-3, #9202
1315 East-West Highway
Silver Spring, Maryland 20910-3282
(301) 713-3242

To obtain current elevation, description, and/or location information for bench marks shown on this map, please contact the Information Services Branch of the National Geodetic Survey at (301) 713-3242, or visit its website at <http://www.ngs.noaa.gov/>.

Base Map information shown on this FIRM was derived from the Johnson County Computer Services from photography dated 2001 and from USGS digital orthophoto quadrangles dated 1998 or later.

This map reflects more detailed and up-to-date stream channel configurations than those shown on the previous FIRM for this jurisdiction. The floodplains and floodways that were transferred from the previous FIRM may have been adjusted to conform to these new stream channel configurations. As a result, the Flood Profiles and Floodway Data tables in the Flood Insurance Study report (which contains authoritative hydraulic data) may reflect stream channel distances that differ from what is shown on this map.

Corporate limits shown on this map are based on the best data available at the time of publication. Because changes due to annexations or de-annexations may have occurred after this map was published, map users should contact appropriate community officials to verify current corporate limit locations.

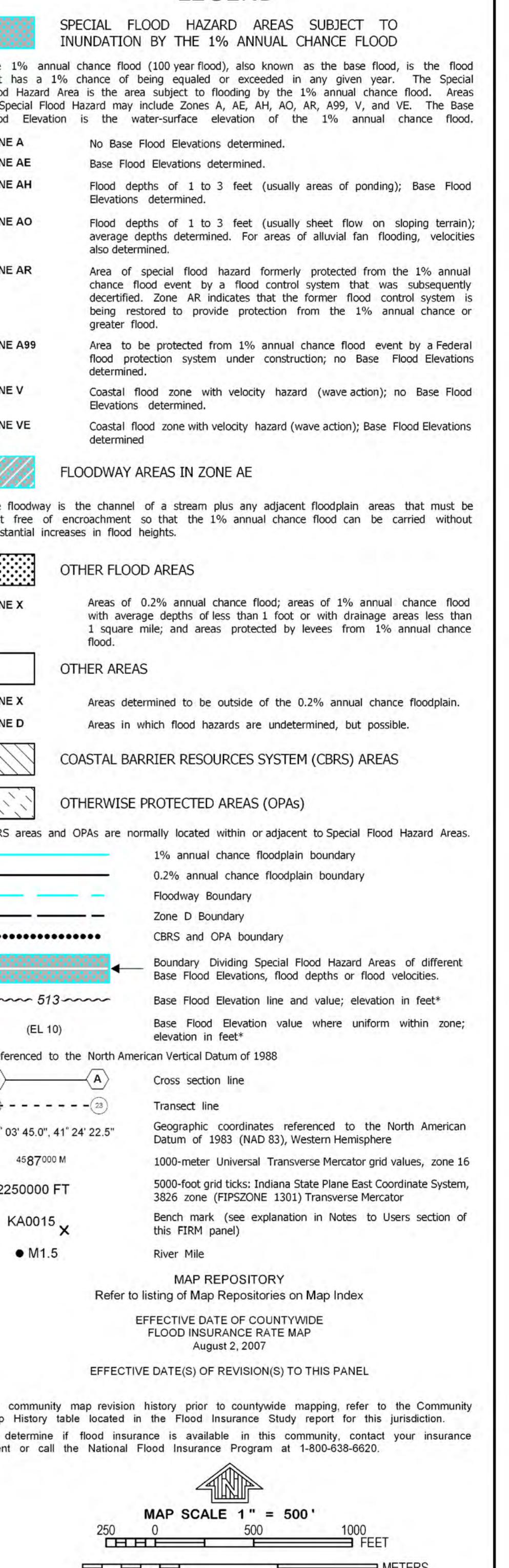
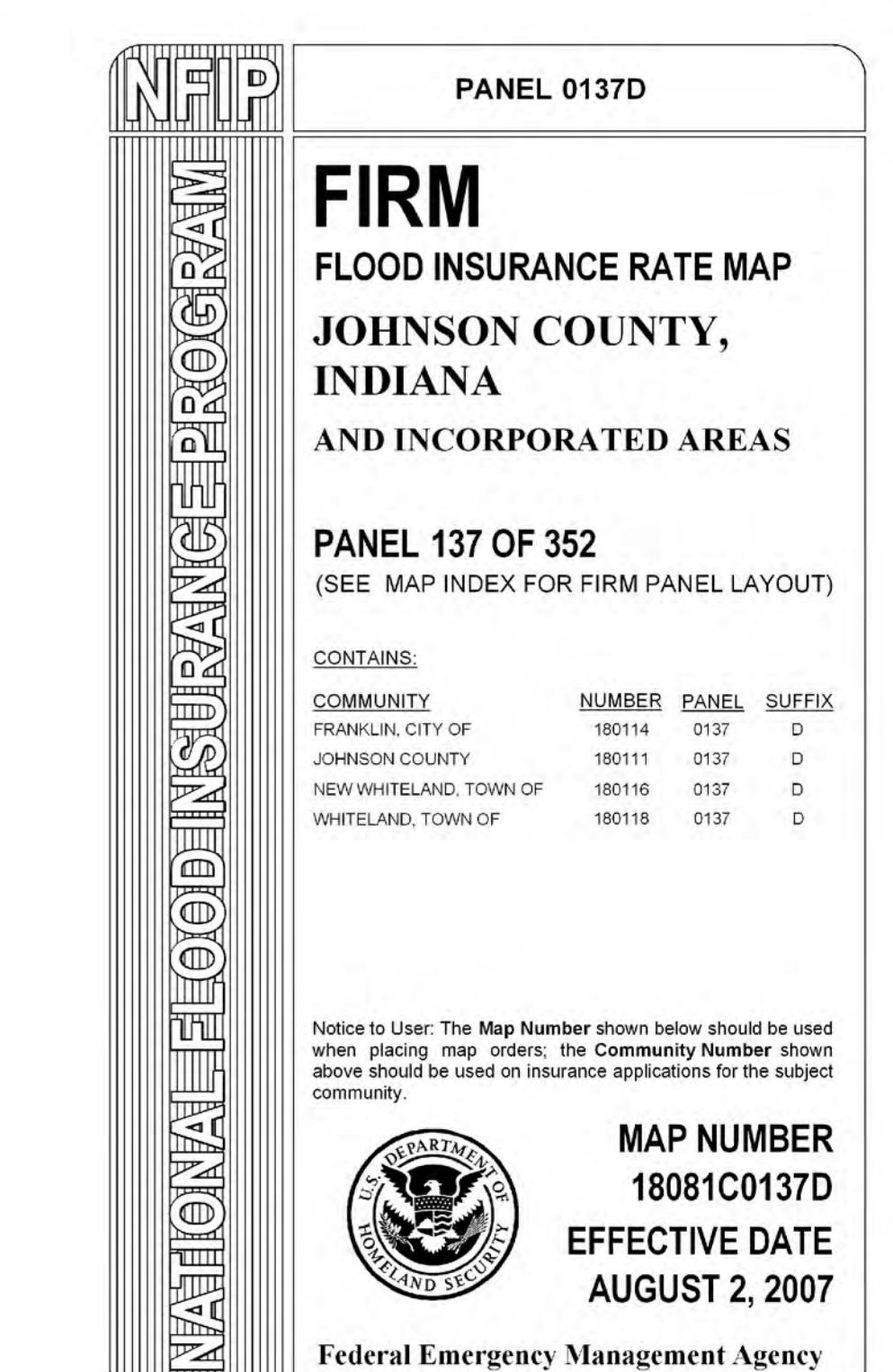
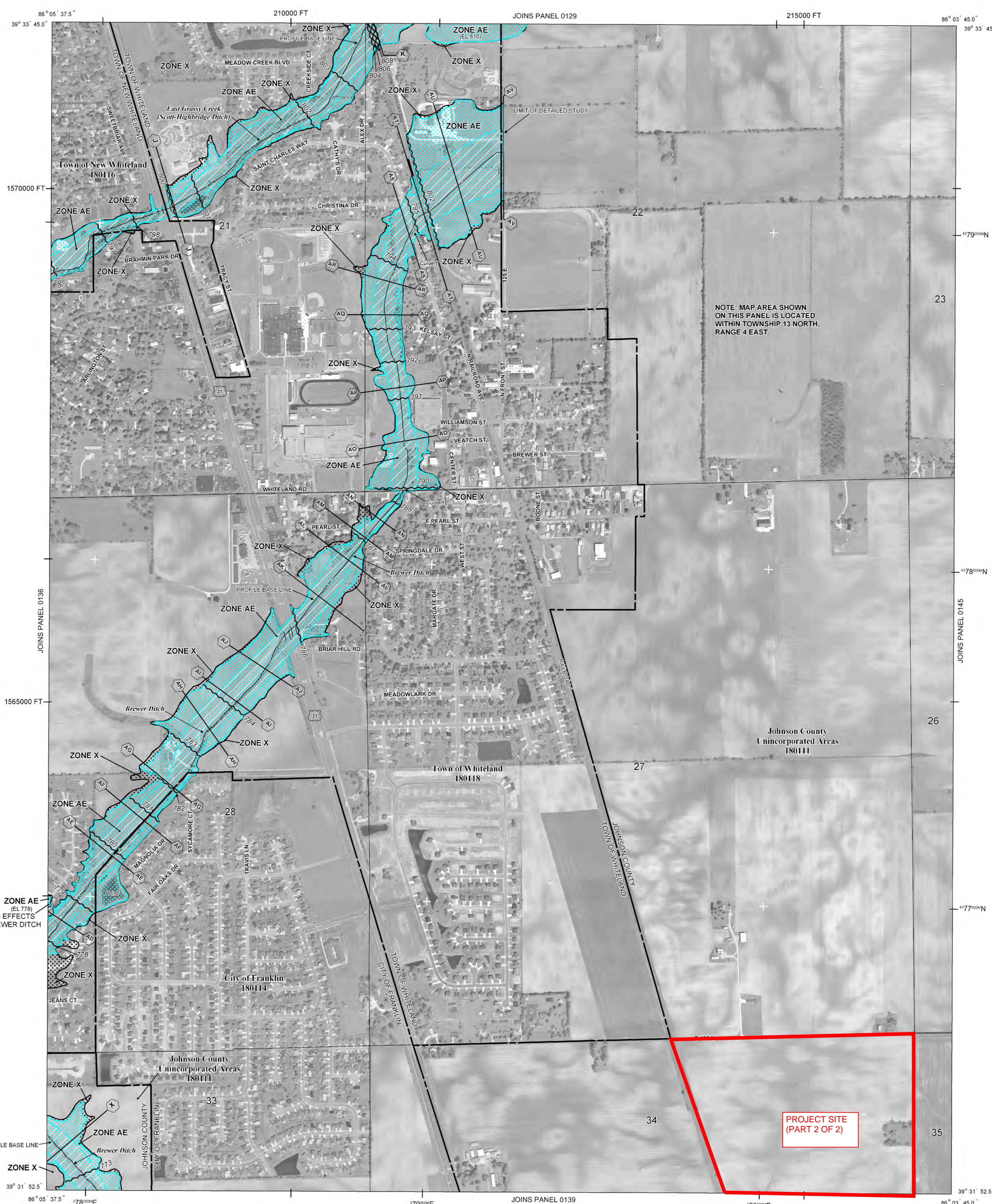
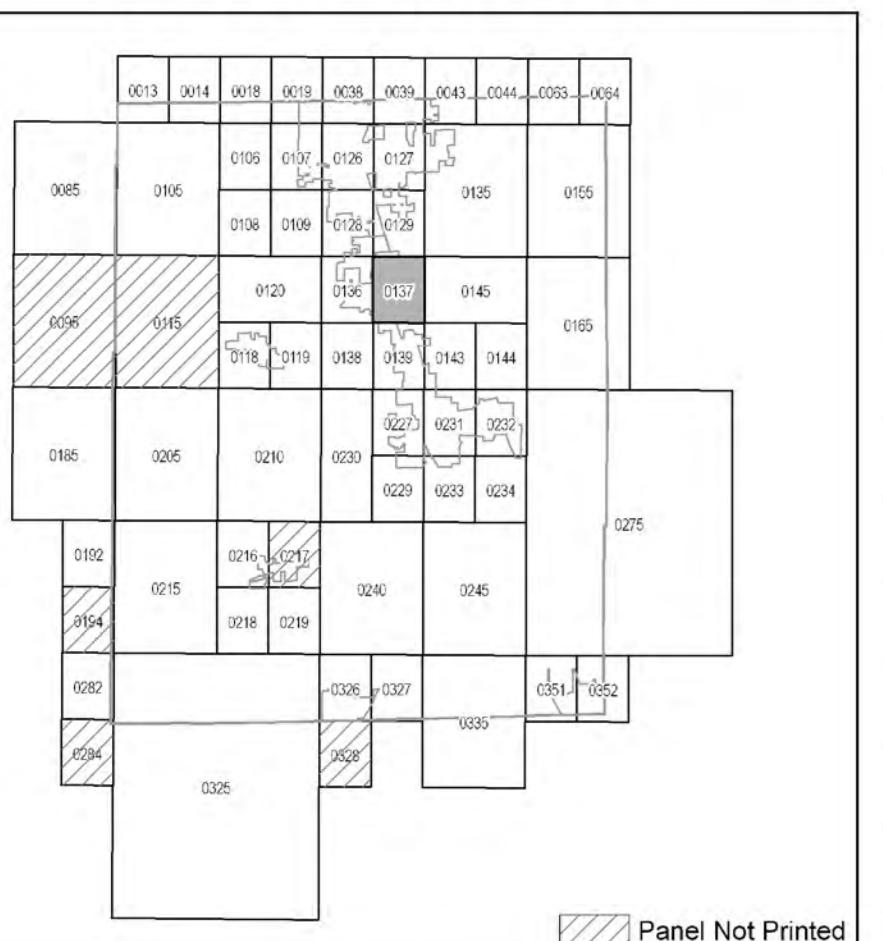
Please refer to the separately printed **Map Index** for an overview map of the county showing the layout of map panels, community map repository addresses, and a listing of communities table containing National Flood Insurance Program dates for each community as well as a listing of the panels on which each community is located.

Contact the **FEMA Map Service Center** at 1-800-358-9616 for information on available products associated with this FIRM. Available products may include previously issued Letters of Map Change, a Flood Insurance Study report, and/or digital versions of this map. The FEMA Map Service Center may also be reached by Fax at 1-800-358-9620 and its website at <http://msc.fema.gov/>.

If you have questions about this map or questions concerning the National Flood Insurance Program in general, please call 1-877-FEMA MAP (1-877-336-2627) or visit the FEMA website at <http://www.fema.gov/business/nfip/>.

The profile base lines depicted on this map represent the hydraulic modeling baselines that match the flood profiles in the FIS report. As a result of improved topographic data, the profile base line, in some cases, may deviate significantly from the channel centerline or appear outside the SFHA.

PANEL INDEX

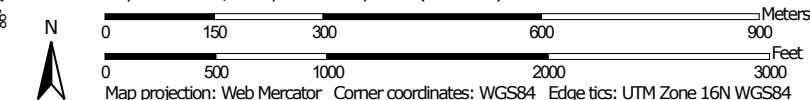


Appendix C: Soil Map

Hydrologic Soil Group—Johnson County, Indiana



Map Scale: 1:10,400 if printed on A portrait (8.5" x 11") sheet.



Map projection: Web Mercator Corner coordinates: WGS84 Edge tics: UTM Zone 16N WGS84



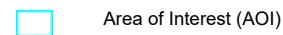
Natural Resources
Conservation Service

Web Soil Survey
National Cooperative Soil Survey

7/30/2024
Page 1 of 4

MAP LEGEND

Area of Interest (AOI)



Soils

Soil Rating Polygons

| | |
|--|----------------------------|
| | A |
| | A/D |
| | B |
| | B/D |
| | C |
| | C/D |
| | D |
| | Not rated or not available |

Soil Rating Lines

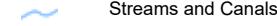
| | |
|--|----------------------------|
| | A |
| | A/D |
| | B |
| | B/D |
| | C |
| | C/D |
| | D |
| | Not rated or not available |

Soil Rating Points

| | |
|--|-----|
| | A |
| | A/D |
| | B |
| | B/D |

| | |
|--|----------------------------|
| | C |
| | C/D |
| | D |
| | Not rated or not available |

Water Features



| | |
|--|---------------------|
| | Rails |
| | Interstate Highways |
| | US Routes |
| | Major Roads |
| | Local Roads |

Background



MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:15,800.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service

Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Johnson County, Indiana

Survey Area Data: Version 31, Sep 1, 2023

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Jun 15, 2022—Jun 21, 2022

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.



Hydrologic Soil Group

| Map unit symbol | Map unit name | Rating | Acres in AOI | Percent of AOI |
|------------------------------------|--|--------|--------------|----------------|
| Br | Brookston silty clay loam, 0 to 2 percent slopes | B/D | 99.8 | 38.5% |
| CrA | Crosby silt loam, fine-loamy subsoil, 0 to 2 percent slopes | C/D | 110.0 | 42.5% |
| CsB2 | Crosby-Miami silt loams, 2 to 4 percent slopes, eroded | C/D | 11.7 | 4.5% |
| FxC2 | Fox complex, 6 to 12 percent slopes, eroded | B | 7.3 | 2.8% |
| MnB2 | Miami silt loam, 2 to 6 percent slopes, eroded | C | 22.3 | 8.6% |
| YclA | Crosby silt loam, fine-loamy subsoil-Urban land complex, 0 to 2 percent slopes | C/D | 7.9 | 3.0% |
| Totals for Area of Interest | | | 259.0 | 100.0% |

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition

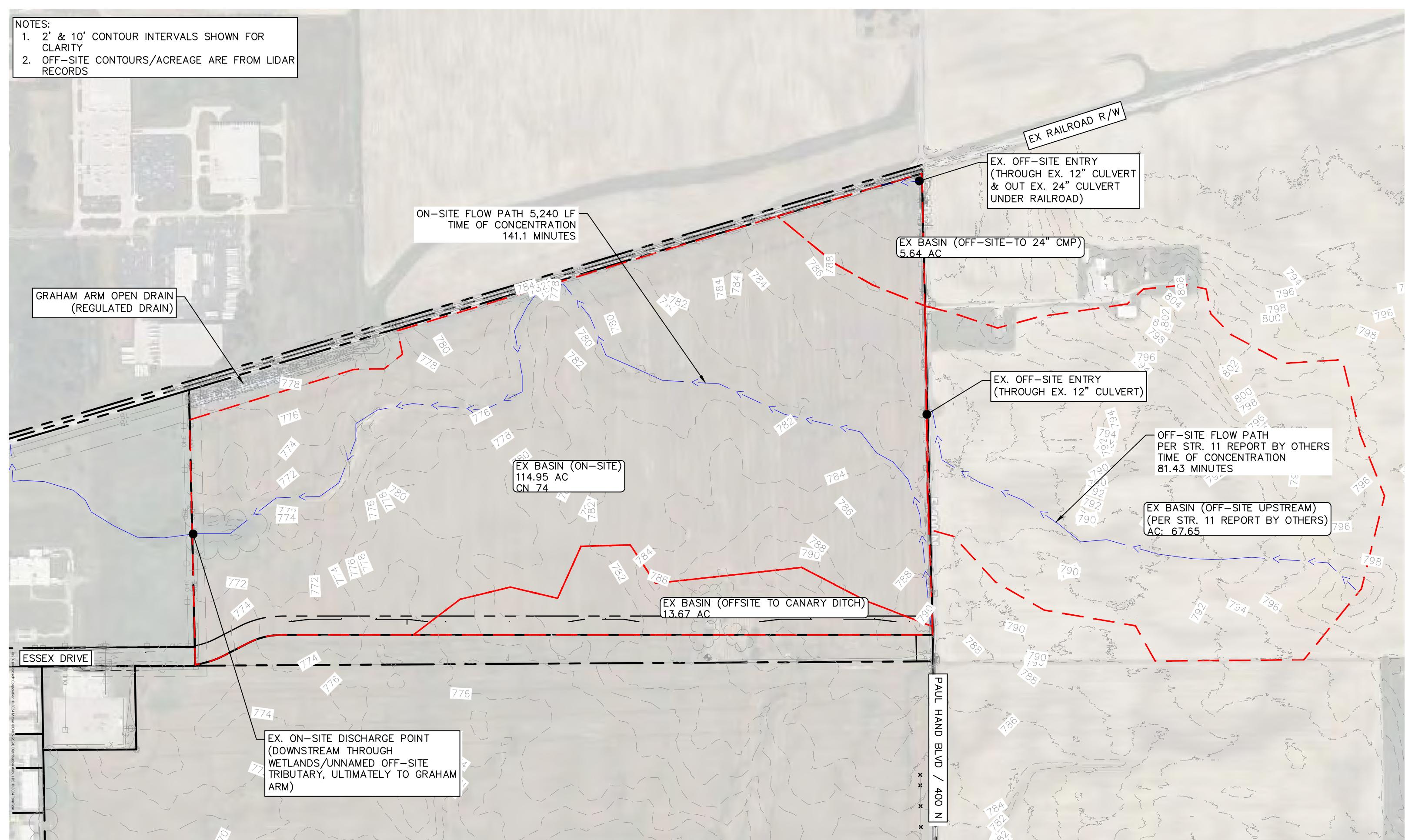
Component Percent Cutoff: None Specified

Tie-break Rule: Higher

Appendix D: Existing Conditions Map

NOTES:

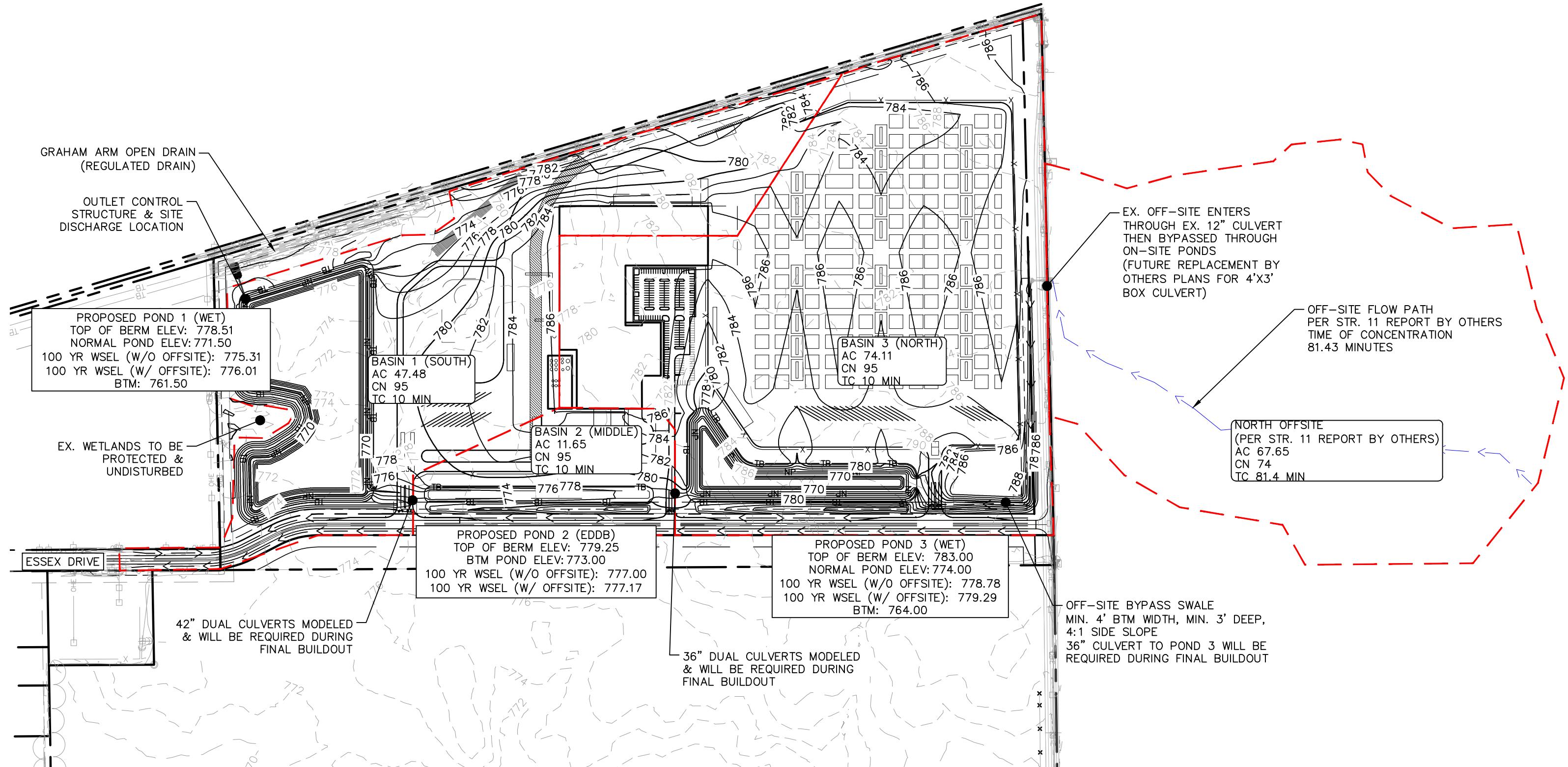
1. 2' & 10' CONTOUR INTERVALS SHOWN FOR CLARITY
2. OFF-SITE CONTOURS/ACREAGE ARE FROM LIDAR RECORDS



Appendix E: Proposed Drainage Map

NOTES:

1. SCHEMATIC SITE LAYOUT IS SHOWN FOR DRAINAGE MASTER PLANNING PURPOSES ONLY. FINAL LAYOUT IS SUBJECT TO CHANGE.
2. PROPOSED GRADING CONTOURS SHOWN ARE FOR MASS GRADING PURPOSES. IT IS THE INTENTION TO REPLACE INTERIM SWALES CONNECTING PONDS WITH EQUALIZING CULVERTS PROPERLY SIZED TO CONVEY DRAINAGE AS PRESENT IN THIS DRAINAGE REPORT.
3. 2' & 10' CONTOUR INTERVALS SHOWN FOR CLARITY
4. OFF-SITE CONTOURS/ACREAGE ARE FROM LIDAR RECORDS



Appendix F: Detention Basin Calculations

Table 2-2a Runoff curve numbers for urban areas ^{1/}

| Cover type and hydrologic condition | Cover description | Curve numbers for hydrologic soil group | | | | |
|--|-------------------|---|----|----|----|--|
| | | A | B | C | D | |
| Fully developed urban areas (vegetation established) | | | | | | |
| Open space (lawns, parks, golf courses, cemeteries, etc.) ^{3/} : | | | | | | |
| Poor condition (grass cover < 50%) | | 68 | 79 | 86 | 89 | |
| Fair condition (grass cover 50% to 75%) | | 49 | 69 | 79 | 84 | |
| Good condition (grass cover > 75%) | | 39 | 61 | 74 | 80 | |
| Impervious areas: | | | | | | |
| Paved parking lots, roofs, driveways, etc. (excluding right-of-way) | | 98 | 98 | 98 | 98 | |
| Streets and roads: | | | | | | |
| Paved; curbs and storm sewers (excluding right-of-way) | | 98 | 98 | 98 | 98 | |
| Paved; open ditches (including right-of-way) | | 83 | 89 | 92 | 93 | |
| Gravel (including right-of-way) | | 76 | 85 | 89 | 91 | |
| Dirt (including right-of-way) | | 72 | 82 | 87 | 89 | |
| Western desert urban areas: | | | | | | |
| Natural desert landscaping (pervious areas only) ^{4/} | | 63 | 77 | 85 | 88 | |
| Artificial desert landscaping (impervious weed barrier, desert shrub with 1- to 2-inch sand or gravel mulch and basin borders) | | 96 | 96 | 96 | 96 | |
| Urban districts: | | | | | | |
| Commercial and business | | 85 | 89 | 92 | 95 | |
| Industrial | | 72 | 81 | 88 | 91 | |
| Residential districts by average lot size: | | | | | | |
| 1/8 acre or less (town houses) | | 65 | 77 | 85 | 90 | |
| 1/4 acre | | 38 | 61 | 75 | 83 | |
| 1/3 acre | | 30 | 57 | 72 | 81 | |
| 1/2 acre | | 25 | 54 | 70 | 87 | |
| 1 acre | | 20 | 51 | 68 | 82 | |
| 2 acres | | 12 | 46 | 65 | 75 | |
| Developing urban areas | | | | | | |
| Newly graded areas (pervious areas only, no vegetation) ^{5/} | | 77 | 86 | 91 | 94 | |
| Idle lands (CN's are determined using cover types similar to those in table 2-2c). | | | | | | |

¹ Average runoff condition, and $I_a = 0.2S$.² The average percent impervious area shown was used to develop the composite CN's. Other assumptions are as follows: impervious areas are directly connected to the drainage system, impervious areas have a CN of 98, and pervious areas are considered equivalent to open space in good hydrologic condition. CN's for other combinations of conditions may be computed using figure 2-3 or 2-4.³ CN's shown are equivalent to those of pasture. Composite CN's may be computed for other combinations of open space cover type.⁴ Composite CN's for natural desert landscaping should be computed using figures 2-3 or 2-4 based on the impervious area percentage ($CN = 98$) and the pervious area CN. The pervious area CN's are assumed equivalent to desert shrub in poor hydrologic condition.⁵ Composite CN's to use for the design of temporary measures during grading and construction should be computed using figure 2-3 or 2-4 based on the degree of development (impervious area percentage) and the CN's for the newly graded pervious areas.

Use 95 for master planning purpose



Table 2-2b Runoff curve numbers for cultivated agricultural lands^{1/}

| Cover type | Treatment ^{2/} | Cover description | Hydrologic condition ^{3/} | Curve numbers for hydrologic soil group | | | |
|--|----------------------------|-------------------|------------------------------------|---|----|----|----|
| | | | | A | B | C | D |
| Fallow | Bare soil | | — | 77 | 86 | 91 | 94 |
| | Crop residue cover (CR) | | Poor | 76 | 85 | 90 | 93 |
| | | | Good | 74 | 83 | 88 | 90 |
| Row crops | Straight row (SR) | | Poor | 72 | 81 | 88 | 91 |
| | | | Good | 67 | 78 | 85 | 89 |
| | SR + CR | | Poor | 71 | 80 | 87 | 90 |
| | | | Good | 64 | 75 | 82 | 85 |
| | Contoured (C) | | Poor | 70 | 79 | 84 | 88 |
| | | | Good | 65 | 75 | 82 | 86 |
| | C + CR | | Poor | 69 | 78 | 83 | 87 |
| | | | Good | 64 | 74 | 81 | 85 |
| | Contoured & terraced (C&T) | | Poor | 66 | 74 | 80 | 82 |
| | | | Good | 62 | 71 | 78 | 81 |
| | C&T+ CR | | Poor | 65 | 73 | 79 | 81 |
| | | | Good | 61 | 70 | 77 | 80 |
| Small grain | SR | | Poor | 65 | 76 | 84 | 88 |
| | | | Good | 63 | 75 | 83 | 87 |
| | SR + CR | | Poor | 64 | 75 | 83 | 86 |
| | | | Good | 60 | 72 | 80 | 84 |
| | C | | Poor | 63 | 74 | 82 | 85 |
| | | | Good | 61 | 73 | 81 | 84 |
| | C + CR | | Poor | 62 | 73 | 81 | 84 |
| | | | Good | 60 | 72 | 80 | 83 |
| | C&T | | Poor | 61 | 72 | 79 | 82 |
| | | | Good | 59 | 70 | 78 | 81 |
| Close-seeded or broadcast legumes or rotation meadow | C&T+ CR | | Poor | 60 | 71 | 78 | 81 |
| | | | Good | 58 | 69 | 77 | 80 |
| | SR | | Poor | 66 | 77 | 85 | 89 |
| | | | Good | 58 | 72 | 81 | 85 |
| | C | | Poor | 64 | 75 | 83 | 85 |
| | | | Good | 55 | 69 | 78 | 83 |
| | C&T | | Poor | 63 | 73 | 80 | 83 |
| | | | Good | 51 | 67 | 76 | 80 |

^{1/} Average runoff condition, and $I_a=0.2S$ ^{2/} Crop residue cover applies only if residue is on at least 5% of the surface throughout the year.^{3/} Hydraulic condition is based on combination factors that affect infiltration and runoff, including (a) density and canopy of vegetative areas, (b) amount of year-round cover, (c) amount of grass or close-seeded legumes, (d) percent of residue cover on the land surface (good $\geq 20\%$), and (e) degree of surface roughness.

Poor: Factors impair infiltration and tend to increase runoff.

Good: Factors encourage average and better than average infiltration and tend to decrease runoff.

**STORMWATER TECHNICAL STANDARDS
MANUAL
JOHNSON COUNTY, INDIANA**

Version 1.0 (2023)

**MODEL/CALCULATIONS
WITHOUT OFFSITE**

Development Site Area
- 114.95 AC

City allowable: 10 to 2,
100 to 10 = 12.28/
25.42



Ex Site



North Offsite

Off-Site Swale

County allowable:
0.1/0.3 = 11.49/ 34.48



Basin 3 (North)

Wet Pond 3 (North)



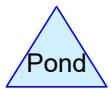
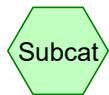
Basin 2 (Middle)

EDDB Pond 2 (Middle)



Basin 1 (South)

Wet Pond 1 (South)



Routing Diagram for Malarkey IND_Huff_R1
Prepared by Kimley-Horn & Associates, Printed 8/7/2024
HydroCAD® 10.20-3c s/n 02344 © 2023 HydroCAD Software Solutions LLC

Malarkey IND_Huff_R1

Prepared by Kimley-Horn & Associates

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Printed 8/7/2024

Page 3

Rainfall Events Listing

| Event# | Event Name | Storm Type | Curve | Mode | Duration (hours) | B/B | Depth (inches) | AMC |
|--------|-----------------|---------------|--------------|---------|------------------|-----|----------------|-----|
| 1 | 002yr-0.17hr | Indy Huff | 1st Quartile | Scale | 0.17 | 1 | 0.69 | 2 |
| 2 | 002yr-0.25hr | Indy Huff | 1st Quartile | Scale | 0.25 | 1 | 0.85 | 2 |
| 3 | 002yr-0.50hr | Indy Huff | 1st Quartile | Scale | 0.50 | 1 | 1.13 | 2 |
| 4 | 002yr-01hr | Indy Huff | 1st Quartile | Scale | 1.00 | 1 | 1.39 | 2 |
| 5 | 002yr-02hr | Indy Huff | 1st Quartile | Scale | 2.00 | 1 | 1.62 | 2 |
| 6 | 002yr-03hr | Indy Huff | 1st Quartile | Scale | 3.00 | 1 | 1.72 | 2 |
| 7 | 002yr-06hr | Indy Huff | 1st Quartile | Scale | 6.00 | 1 | 2.05 | 2 |
| 8 | 002yr-12hr | Indy Huff | 2nd Quartile | Scale | 12.00 | 1 | 2.45 | 2 |
| 9 | 002yr-24hr | Indy Huff | 3rd Quartile | Scale | 24.00 | 1 | 2.92 | 2 |
| 10 | 10 Yr-SCS 24Hr | Type II 24-Hr | | Default | 24.00 | 1 | 4.10 | 2 |
| 11 | 010yr-0.17hr | Indy Huff | 1st Quartile | Scale | 0.17 | 1 | 0.93 | 2 |
| 12 | 010yr-0.25hr | Indy Huff | 1st Quartile | Scale | 0.25 | 1 | 1.14 | 2 |
| 13 | 010yr-0.50hr | Indy Huff | 1st Quartile | Scale | 0.50 | 1 | 1.59 | 2 |
| 14 | 010yr-01hr | Indy Huff | 1st Quartile | Scale | 1.00 | 1 | 2.02 | 2 |
| 15 | 010yr-02hr | Indy Huff | 1st Quartile | Scale | 2.00 | 1 | 2.37 | 2 |
| 16 | 010yr-03hr | Indy Huff | 1st Quartile | Scale | 3.00 | 1 | 2.53 | 2 |
| 17 | 010yr-06hr | Indy Huff | 1st Quartile | Scale | 6.00 | 1 | 3.03 | 2 |
| 18 | 010yr-12hr | Indy Huff | 2nd Quartile | Scale | 12.00 | 1 | 3.52 | 2 |
| 19 | 010yr-24hr | Indy Huff | 3rd Quartile | Scale | 24.00 | 1 | 4.08 | 2 |
| 20 | 100 Yr-SCS 24Hr | Type II 24-Hr | | Default | 24.00 | 1 | 5.91 | 2 |
| 21 | 100yr-0.17hr | Indy Huff | 1st Quartile | Scale | 0.17 | 1 | 1.25 | 2 |
| 22 | 100yr-0.25hr | Indy Huff | 1st Quartile | Scale | 0.25 | 1 | 1.56 | 2 |
| 23 | 100yr-0.50hr | Indy Huff | 1st Quartile | Scale | 0.50 | 1 | 2.25 | 2 |
| 24 | 100yr-01hr | Indy Huff | 1st Quartile | Scale | 1.00 | 1 | 3.01 | 2 |
| 25 | 100yr-02hr | Indy Huff | 1st Quartile | Scale | 2.00 | 1 | 2.65 | 2 |
| 26 | 100yr-03hr | Indy Huff | 1st Quartile | Scale | 3.00 | 1 | 3.94 | 2 |
| 27 | 100yr-06hr | Indy Huff | 1st Quartile | Scale | 6.00 | 1 | 4.78 | 2 |
| 28 | 100yr-12hr | Indy Huff | 2nd Quartile | Scale | 12.00 | 1 | 5.37 | 2 |
| 29 | 100yr-24hr | Indy Huff | 3rd Quartile | Scale | 24.00 | 1 | 5.91 | 2 |
| 30 | WQV-0.17hr | Indy Huff | 1st Quartile | Scale | 0.17 | 1 | 1.25 | 2 |
| 31 | WQV-0.25hr | Indy Huff | 1st Quartile | Scale | 0.25 | 1 | 1.25 | 2 |
| 32 | WQV-0.50hr | Indy Huff | 1st Quartile | Scale | 0.50 | 1 | 1.25 | 2 |
| 33 | WQV-01hr | Indy Huff | 1st Quartile | Scale | 1.00 | 1 | 1.25 | 2 |
| 34 | WQV-02hr | Indy Huff | 1st Quartile | Scale | 2.00 | 1 | 1.25 | 2 |
| 35 | WQV-03hr | Indy Huff | 1st Quartile | Scale | 3.00 | 1 | 1.25 | 2 |
| 36 | WQV-06hr | Indy Huff | 1st Quartile | Scale | 6.00 | 1 | 1.25 | 2 |
| 37 | WQV-12hr | Indy Huff | 2nd Quartile | Scale | 12.00 | 1 | 1.25 | 2 |
| 38 | WQV-24hr | Indy Huff | 3rd Quartile | Scale | 24.00 | 1 | 1.25 | 2 |

Use for existing condition to establish pre-development existing condition per City of Franklin code

Table 2-2c Runoff curve numbers for other agricultural lands ^{1/}

| Cover type | Cover description | Hydrologic condition | Curve numbers for hydrologic soil group | | | |
|--|-------------------|----------------------|---|----|----|----|
| | | | A | B | C | D |
| Pasture, grassland, or range—continuous forage for grazing. ^{2/} | | Poor | 68 | 79 | 86 | 89 |
| | | Fair | 49 | 69 | 79 | 84 |
| | | Good | 39 | 61 | 74 | 80 |
| Meadow—continuous grass, protected from grazing and generally mowed for hay. | | — | 30 | 58 | 71 | 78 |
| Brush—brush-weed-grass mixture with brush the major element. ^{3/} | | Poor | 48 | 67 | 77 | 83 |
| | | Fair | 35 | 56 | 70 | 77 |
| | | Good | 30 ^{4/} | 48 | 65 | 73 |
| Woods—grass combination (orchard or tree farm). ^{5/} | | Poor | 57 | 73 | 82 | 86 |
| | | Fair | 43 | 65 | 76 | 82 |
| | | Good | 32 | 58 | 72 | 79 |
| Woods. ^{6/} | | Poor | 45 | 66 | 77 | 83 |
| | | Fair | 36 | 60 | 73 | 79 |
| | | Good | 30 ^{4/} | 55 | 70 | 77 |
| Farmsteads—buildings, lanes, driveways, and surrounding lots. | | — | 59 | 74 | 82 | 86 |

¹ Average runoff condition, and $I_a = 0.2S$.² Poor: <50% ground cover or heavily grazed with no mulch.

Fair: 50 to 75% ground cover and not heavily grazed.

Good: > 75% ground cover and lightly or only occasionally grazed.

³ Poor: <50% ground cover.

Fair: 50 to 75% ground cover.

Good: >75% ground cover.

⁴ Actual curve number is less than 30; use CN = 30 for runoff computations.⁵ CN's shown were computed for areas with 50% woods and 50% grass (pasture) cover. Other combinations of conditions may be computed from the CN's for woods and pasture.⁶ Poor: Forest litter, small trees, and brush are destroyed by heavy grazing or regular burning.

Fair: Woods are grazed but not burned, and some forest litter covers the soil.

Good: Woods are protected from grazing, and litter and brush adequately cover the soil.

Table 2-2d Runoff curve numbers for arid and semiarid rangelands ^{1/}

| Cover type | Cover description | Hydrologic condition ^{2/} | Curve numbers for hydrologic soil group | | |
|--|-------------------|------------------------------------|---|----|----|
| | | | A ^{3/} | B | C |
| Herbaceous—mixture of grass, weeds, and low-growing brush, with brush the minor element. | Poor | | 80 | 87 | 93 |
| | Fair | | 71 | 81 | 89 |
| | Good | | 62 | 74 | 85 |
| Oak-aspen—mountain brush mixture of oak brush, aspen, mountain mahogany, bitter brush, maple, and other brush. | Poor | | 66 | 74 | 79 |
| | Fair | | 48 | 57 | 63 |
| | Good | | 30 | 41 | 48 |
| Pinyon-juniper—pinyon, juniper, or both; grass understory. | Poor | | 75 | 85 | 89 |
| | Fair | | 58 | 73 | 80 |
| | Good | | 41 | 61 | 71 |
| Sagebrush with grass understory. | Poor | | 67 | 80 | 85 |
| | Fair | | 51 | 63 | 70 |
| | Good | | 35 | 47 | 55 |
| Desert shrub—major plants include saltbush, greasewood, creosotebush, blackbrush, bursage, palo verde, mesquite, and cactus. | Poor | | 63 | 77 | 85 |
| | Fair | | 55 | 72 | 81 |
| | Good | | 49 | 68 | 79 |

¹ Average runoff condition, and $I_a = 0.2S$. For range in humid regions, use table 2-2c.

² Poor: <30% ground cover (litter, grass, and brush overstory).

Fair: 30 to 70% ground cover.

Good: > 70% ground cover.

³ Curve numbers for group A have been developed only for desert shrub.

TABLE 2-3

Use 10 min due to
anticipation of
substantial length of
storm sewer system

| Runoff Coefficients by Land Use, Typical Inlet Times, and Storm Recurrence Interval | | | | | | | | | | | | | | |
|---|---|------------|------------|-------------|----------------|------------|------------|-------------|--------------|------------|------------|-------------|--------------------------------|--|
| Land Use | Runoff Coefficients "C" (by Storm Recurrence Interval) | | | | | | | | | | | | Inlet Time (Minutes) (4) | |
| | Flat (1) | | | | Rolling (2) | | | | Steep (3) | | | | | |
| | < 25 year | 25 year | 50 year | 100 year | < 25 year | 25 year | 50 year | 100 year | < 25 year | 25 year | 50 year | 100 year | | |
| Commercial (CBD) | 0.75 | 0.83 | 0.99 | 1.00 | 0.83 | 0.91 | 1.00 | 1.00 | 0.91 | 1.00 | 1.00 | 1.00 | 5 | |
| Commercial (Neighborhood) | 0.54 | 0.59 | 0.71 | 0.89 | 0.60 | 0.66 | 0.79 | 0.99 | 0.66 | 0.73 | 0.87 | 1.00 | 5 - 10 | |
| Industrial | 0.63 | 0.69 | 0.83 | 1.00 | 0.70 | 0.77 | 0.92 | 1.00 | 0.77 | 0.85 | 1.00 | 1.00 | | |
| Garden Apartments | 0.54 | 0.59 | 0.71 | 0.89 | 0.60 | 0.66 | 0.79 | 0.99 | 0.66 | 0.73 | 0.87 | 1.00 | | |
| Churches | 0.54 | 0.59 | 0.71 | 0.89 | 0.60 | 0.66 | 0.79 | 0.99 | 0.66 | 0.73 | 0.87 | 1.00 | | |
| Schools | 0.31 | 0.34 | 0.41 | 0.51 | 0.35 | 0.39 | 0.46 | 0.58 | 0.39 | 0.43 | 0.51 | 0.64 | 10 - 15 | |
| Semi Detached Residential | 0.45 | 0.50 | 0.59 | 0.74 | 0.50 | 0.55 | 0.66 | 0.83 | 0.55 | 0.61 | 0.73 | 0.91 | | |
| Detached Residential | 0.40 | 0.44 | 0.53 | 0.66 | 0.45 | 0.50 | 0.59 | 0.74 | 0.50 | 0.55 | 0.66 | 0.83 | | |
| Quarter Acre Lots | 0.36 | 0.40 | 0.48 | 0.59 | 0.40 | 0.44 | 0.53 | 0.66 | 0.44 | 0.48 | 0.58 | 0.73 | | |
| Half Acre Lots | 0.31 | 0.34 | 0.41 | 0.51 | 0.35 | 0.39 | 0.46 | 0.58 | 0.39 | 0.43 | 0.51 | 0.64 | | |
| Parkland | 0.18 | 0.20 | 0.24 | 0.30 | 0.20 | 0.22 | 0.26 | 0.33 | 0.22 | 0.24 | 0.29 | 0.36 | To be Computed | |

Source: HERPICC Stormwater Drainage Manual, July 1995, and other sources.

(1) Flat terrain involves slopes of 0-2%.

(2) Rolling terrain involves slopes of 2-7%.

(3) Steep terrain involves slopes greater than 7%.

(4) Interpolation, extrapolation and adjustment for local conditions shall be based on engineering experience and judgment.

Time span=0.00-48.00 hrs, dt=0.05 hrs, 961 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 11S: Ex Site

Runoff Area=114.950 ac 0.00% Impervious Runoff Depth=3.11"
Flow Length=5,240' Tc=141.1 min CN=74 Runoff=98.87 cfs 29.785 af

Subcatchment 13S: Basin 3 (North)

Runoff Area=74.111 ac 0.00% Impervious Runoff Depth=5.32"
Tc=10.0 min CN=95 Runoff=532.34 cfs 32.869 af

Subcatchment 15S: Basin 2 (Middle)

Runoff Area=11.651 ac 0.00% Impervious Runoff Depth=5.32"
Tc=10.0 min CN=95 Runoff=83.69 cfs 5.167 af

Subcatchment 16S: Basin 1 (South)

Runoff Area=47.476 ac 0.00% Impervious Runoff Depth=5.32"
Tc=10.0 min CN=95 Runoff=341.02 cfs 21.056 af

Subcatchment 18S: North Offsite

Runoff Area=67.650 ac 1.06% Impervious Runoff Depth=3.11"
Tc=81.4 min CN=74 Runoff=88.88 cfs 17.529 af

Reach 14R: Off-Site Swale

Avg. Flow Depth=1.67' Max Vel=4.96 fps Inflow=88.88 cfs 17.529 af
n=0.022 L=1,260.0' S=0.0054 '/' Capacity=334.55 cfs Outflow=88.47 cfs 17.529 af

Pond 7P: Wet Pond 1 (South)

Peak Elev=775.31' Storage=1,645,819 cf Inflow=415.48 cfs 58.610 af
Outflow=25.10 cfs 42.456 af

Pond 17P: EDDB Pond 2 (Middle)

Peak Elev=777.00' Storage=141,561 cf Inflow=178.30 cfs 37.591 af
42.0" Round Culvert x 2.00 n=0.013 L=810.0' S=0.0019 '/' Outflow=100.55 cfs 37.554 af

Pond 18P: Wet Pond 3 (North)

Peak Elev=778.78' Storage=14.760 af Inflow=532.34 cfs 32.869 af
36.0" Round Culvert x 2.00 n=0.013 L=211.0' S=0.0047 '/' Outflow=97.03 cfs 32.424 af

Total Runoff Area = 315.838 ac Runoff Volume = 106.407 af Average Runoff Depth = 4.04"
99.77% Pervious = 315.118 ac 0.23% Impervious = 0.720 ac

Malarkey IND_Huff_R1

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Area Listing (all nodes)

| Area (acres) | CN | Description (subcatchment-numbers) |
|-----------------|-----------|---|
| 133.238 | 95 | (13S, 15S, 16S) |
| 66.930 | 74 | From Paul Hand Drainage Report (Structure 11) (18S) |
| 0.720 | 98 | From Paul Hand Drainage Report (Structure 11) (18S) |
| 114.950 | 74 | Pasture/grassland/range, Good, HSG C (11S) |
| 315.838 | 83 | TOTAL AREA |

Malarkey IND_Huff_R1

Prepared by Kimley-Horn & Associates

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Soil Listing (all nodes)

| Area (acres) | Soil Group | Subcatchment Numbers |
|-----------------|---------------|-------------------------|
| 0.000 | HSG A | |
| 0.000 | HSG B | |
| 114.950 | HSG C | 11S |
| 0.000 | HSG D | |
| 200.888 | Other | 13S, 15S, 16S, 18S |
| 315.838 | | TOTAL AREA |

Malarkey IND_Huff_R1

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Ground Covers (all nodes)

| HSG-A (acres) | HSG-B (acres) | HSG-C (acres) | HSG-D (acres) | Other (acres) | Total (acres) | Ground Cover |
|------------------|------------------|------------------|------------------|------------------|------------------|--|
| 0.000 | 0.000 | 0.000 | 0.000 | 133.238 | 133.238 | |
| 0.000 | 0.000 | 0.000 | 0.000 | 67.650 | 67.650 | From Paul Hand Drainage Report (Structure 11) |
| 0.000 | 0.000 | 114.950 | 0.000 | 0.000 | 114.950 | Pasture/grassland/range, Good |
| 0.000 | 0.000 | 114.950 | 0.000 | 200.888 | 315.838 | TOTAL AREA |

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Pipe Listing (all nodes)

| Line# | Node Number | In-Invert (feet) | Out-Invert (feet) | Length (feet) | Slope (ft/ft) | n | Width (inches) | Diam/Height (inches) | Inside-Fill (inches) | Node Name |
|-------|-------------|---------------------|----------------------|------------------|------------------|-------|-------------------|-------------------------|-------------------------|-----------|
| 1 | 17P | 773.00 | 771.50 | 810.0 | 0.0019 | 0.013 | 0.0 | 42.0 | 0.0 | |
| 2 | 18P | 774.00 | 773.00 | 211.0 | 0.0047 | 0.013 | 0.0 | 36.0 | 0.0 | |

Events for Subcatchment 13S: Basin 3 (North)

| Event | Rainfall (inches) | Runoff (cfs) | Volume (acre-feet) | Depth (inches) |
|-----------------|----------------------|-----------------|-----------------------|-------------------|
| 002yr-0.17hr | 0.69 | 115.53 | 1.901 | 0.31 |
| 002yr-0.25hr | 0.85 | 129.97 | 2.695 | 0.44 |
| 002yr-0.50hr | 1.13 | 125.94 | 4.181 | 0.68 |
| 002yr-01hr | 1.39 | 113.79 | 5.629 | 0.91 |
| 002yr-02hr | 1.62 | 81.37 | 6.943 | 1.12 |
| 002yr-03hr | 1.72 | 61.32 | 7.521 | 1.22 |
| 002yr-06hr | 2.05 | 40.32 | 9.452 | 1.53 |
| 002yr-12hr | 2.45 | 23.43 | 11.826 | 1.91 |
| 002yr-24hr | 2.92 | 17.64 | 14.645 | 2.37 |
| 10 Yr-SCS 24Hr | 4.10 | 361.52 | 21.799 | 3.53 |
| 010yr-0.17hr | 0.93 | 187.73 | 3.109 | 0.50 |
| 010yr-0.25hr | 1.14 | 201.69 | 4.236 | 0.69 |
| 010yr-0.50hr | 1.59 | 217.72 | 6.770 | 1.10 |
| 010yr-01hr | 2.02 | 195.02 | 9.276 | 1.50 |
| 010yr-02hr | 2.37 | 138.21 | 11.349 | 1.84 |
| 010yr-03hr | 2.53 | 104.05 | 12.304 | 1.99 |
| 010yr-06hr | 3.03 | 67.23 | 15.308 | 2.48 |
| 010yr-12hr | 3.52 | 35.61 | 18.273 | 2.96 |
| 010yr-24hr | 4.08 | 25.46 | 21.677 | 3.51 |
| 100 Yr-SCS 24Hr | 5.91 | 532.34 | 32.869 | 5.32 |
| 100yr-0.17hr | 1.25 | 290.94 | 4.843 | 0.78 |
| 100yr-0.25hr | 1.56 | 312.23 | 6.597 | 1.07 |
| 100yr-0.50hr | 2.25 | 353.19 | 10.636 | 1.72 |
| 100yr-01hr | 3.01 | 330.96 | 15.188 | 2.46 |
| 100yr-02hr | 2.65 | 159.89 | 13.023 | 2.11 |
| 100yr-03hr | 3.94 | 180.17 | 20.825 | 3.37 |
| 100yr-06hr | 4.78 | 115.46 | 25.949 | 4.20 |
| 100yr-12hr | 5.37 | 56.54 | 29.560 | 4.79 |
| 100yr-24hr | 5.91 | 37.69 | 32.869 | 5.32 |
| WQV-0.17hr | 1.25 | 290.94 | 4.843 | 0.78 |
| WQV-0.25hr | 1.25 | 230.02 | 4.843 | 0.78 |
| WQV-0.50hr | 1.25 | 147.68 | 4.843 | 0.78 |
| WQV-01hr | 1.25 | 96.58 | 4.843 | 0.78 |
| WQV-02hr | 1.25 | 54.92 | 4.843 | 0.78 |
| WQV-03hr | 1.25 | 37.85 | 4.843 | 0.78 |
| WQV-06hr | 1.25 | 19.37 | 4.843 | 0.78 |
| WQV-12hr | 1.25 | 9.79 | 4.843 | 0.78 |
| WQV-24hr | 1.25 | 6.54 | 4.843 | 0.78 |

Summary for Subcatchment 13S: Basin 3 (North)

Runoff = 532.34 cfs @ 12.01 hrs, Volume= 32.869 af, Depth= 5.32"
Routed to Pond 18P : Wet Pond 3 (North)

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs
Type II 24-Hr 100 Yr-SCS 24Hr Rainfall=5.91"

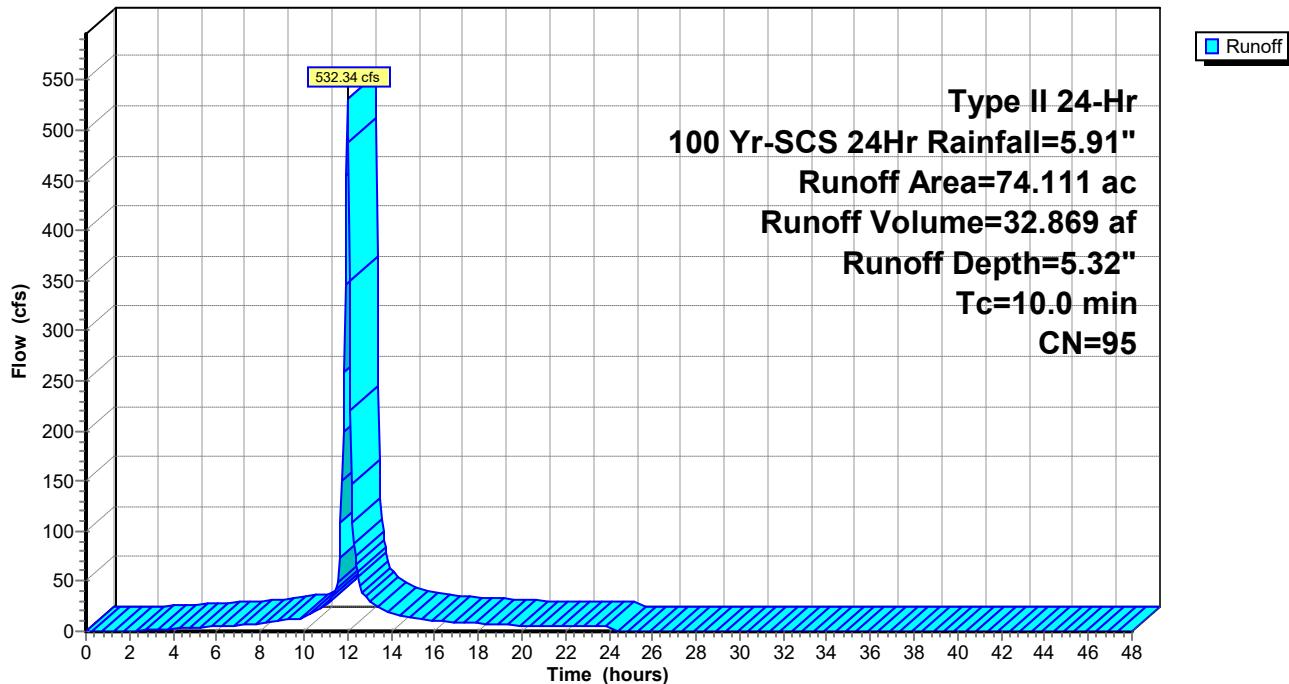
| Area (ac) | CN | Description |
|-----------|----|-------------|
|-----------|----|-------------|

| | | |
|---|--------|----|
| * | 74.111 | 95 |
|---|--------|----|

| | |
|--------|-----------------------|
| 74.111 | 100.00% Pervious Area |
|--------|-----------------------|

| Tc | Length | Slope | Velocity | Capacity | Description |
|-------|--------|---------|----------|----------|-------------|
| (min) | (feet) | (ft/ft) | (ft/sec) | (cfs) | |

| | |
|------|---------------|
| 10.0 | Direct Entry, |
|------|---------------|

Subcatchment 13S: Basin 3 (North)**Hydrograph**

Events for Subcatchment 15S: Basin 2 (Middle)

| Event | Rainfall (inches) | Runoff (cfs) | Volume (acre-feet) | Depth (inches) |
|-----------------|----------------------|-----------------|-----------------------|-------------------|
| 002yr-0.17hr | 0.69 | 18.16 | 0.299 | 0.31 |
| 002yr-0.25hr | 0.85 | 20.43 | 0.424 | 0.44 |
| 002yr-0.50hr | 1.13 | 19.80 | 0.657 | 0.68 |
| 002yr-01hr | 1.39 | 17.89 | 0.885 | 0.91 |
| 002yr-02hr | 1.62 | 12.79 | 1.091 | 1.12 |
| 002yr-03hr | 1.72 | 9.64 | 1.182 | 1.22 |
| 002yr-06hr | 2.05 | 6.34 | 1.486 | 1.53 |
| 002yr-12hr | 2.45 | 3.68 | 1.859 | 1.91 |
| 002yr-24hr | 2.92 | 2.77 | 2.302 | 2.37 |
| 10 Yr-SCS 24Hr | 4.10 | 56.83 | 3.427 | 3.53 |
| 010yr-0.17hr | 0.93 | 29.51 | 0.489 | 0.50 |
| 010yr-0.25hr | 1.14 | 31.71 | 0.666 | 0.69 |
| 010yr-0.50hr | 1.59 | 34.23 | 1.064 | 1.10 |
| 010yr-01hr | 2.02 | 30.66 | 1.458 | 1.50 |
| 010yr-02hr | 2.37 | 21.73 | 1.784 | 1.84 |
| 010yr-03hr | 2.53 | 16.36 | 1.934 | 1.99 |
| 010yr-06hr | 3.03 | 10.57 | 2.407 | 2.48 |
| 010yr-12hr | 3.52 | 5.60 | 2.873 | 2.96 |
| 010yr-24hr | 4.08 | 4.00 | 3.408 | 3.51 |
| 100 Yr-SCS 24Hr | 5.91 | 83.69 | 5.167 | 5.32 |
| 100yr-0.17hr | 1.25 | 45.74 | 0.761 | 0.78 |
| 100yr-0.25hr | 1.56 | 49.09 | 1.037 | 1.07 |
| 100yr-0.50hr | 2.25 | 55.52 | 1.672 | 1.72 |
| 100yr-01hr | 3.01 | 52.03 | 2.388 | 2.46 |
| 100yr-02hr | 2.65 | 25.14 | 2.047 | 2.11 |
| 100yr-03hr | 3.94 | 28.32 | 3.274 | 3.37 |
| 100yr-06hr | 4.78 | 18.15 | 4.079 | 4.20 |
| 100yr-12hr | 5.37 | 8.89 | 4.647 | 4.79 |
| 100yr-24hr | 5.91 | 5.93 | 5.167 | 5.32 |
| WQV-0.17hr | 1.25 | 45.74 | 0.761 | 0.78 |
| WQV-0.25hr | 1.25 | 36.16 | 0.761 | 0.78 |
| WQV-0.50hr | 1.25 | 23.22 | 0.761 | 0.78 |
| WQV-01hr | 1.25 | 15.18 | 0.761 | 0.78 |
| WQV-02hr | 1.25 | 8.63 | 0.761 | 0.78 |
| WQV-03hr | 1.25 | 5.95 | 0.761 | 0.78 |
| WQV-06hr | 1.25 | 3.05 | 0.761 | 0.78 |
| WQV-12hr | 1.25 | 1.54 | 0.761 | 0.78 |
| WQV-24hr | 1.25 | 1.03 | 0.761 | 0.78 |

Summary for Subcatchment 15S: Basin 2 (Middle)

Runoff = 83.69 cfs @ 12.01 hrs, Volume= 5.167 af, Depth= 5.32"
Routed to Pond 17P : EDDB Pond 2 (Middle)

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs
Type II 24-Hr 100 Yr-SCS 24Hr Rainfall=5.91"

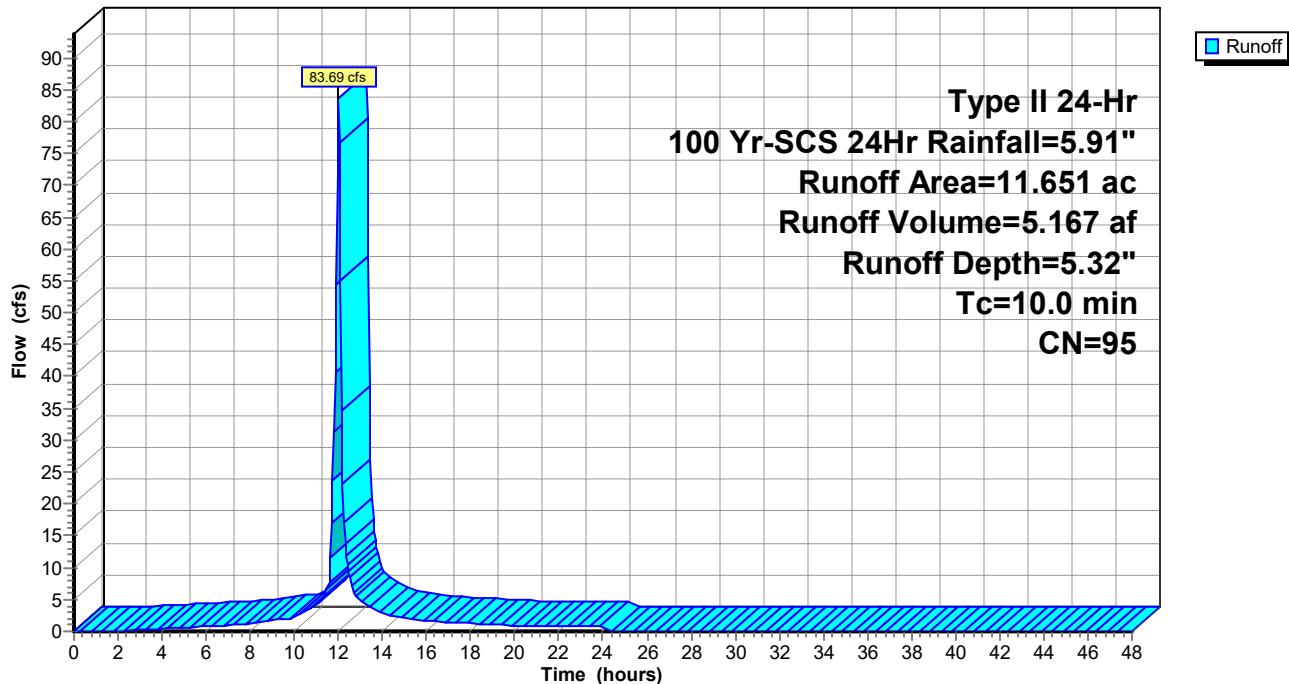
| Area (ac) | CN | Description |
|-----------|----|-------------|
|-----------|----|-------------|

| | | |
|---|--------|----|
| * | 11.651 | 95 |
|---|--------|----|

| | |
|--------|-----------------------|
| 11.651 | 100.00% Pervious Area |
|--------|-----------------------|

| Tc | Length | Slope | Velocity | Capacity | Description |
|-------|--------|---------|----------|----------|-------------|
| (min) | (feet) | (ft/ft) | (ft/sec) | (cfs) | |

| | |
|------|---------------|
| 10.0 | Direct Entry, |
|------|---------------|

Subcatchment 15S: Basin 2 (Middle)**Hydrograph**

Events for Subcatchment 16S: Basin 1 (South)

| Event | Rainfall (inches) | Runoff (cfs) | Volume (acre-feet) | Depth (inches) |
|-----------------|----------------------|-----------------|-----------------------|-------------------|
| 002yr-0.17hr | 0.69 | 74.01 | 1.218 | 0.31 |
| 002yr-0.25hr | 0.85 | 83.26 | 1.726 | 0.44 |
| 002yr-0.50hr | 1.13 | 80.68 | 2.678 | 0.68 |
| 002yr-01hr | 1.39 | 72.89 | 3.606 | 0.91 |
| 002yr-02hr | 1.62 | 52.13 | 4.447 | 1.12 |
| 002yr-03hr | 1.72 | 39.28 | 4.818 | 1.22 |
| 002yr-06hr | 2.05 | 25.83 | 6.055 | 1.53 |
| 002yr-12hr | 2.45 | 15.01 | 7.576 | 1.91 |
| 002yr-24hr | 2.92 | 11.30 | 9.382 | 2.37 |
| 10 Yr-SCS 24Hr | 4.10 | 231.59 | 13.965 | 3.53 |
| 010yr-0.17hr | 0.93 | 120.26 | 1.992 | 0.50 |
| 010yr-0.25hr | 1.14 | 129.20 | 2.714 | 0.69 |
| 010yr-0.50hr | 1.59 | 139.47 | 4.337 | 1.10 |
| 010yr-01hr | 2.02 | 124.93 | 5.942 | 1.50 |
| 010yr-02hr | 2.37 | 88.54 | 7.270 | 1.84 |
| 010yr-03hr | 2.53 | 66.65 | 7.882 | 1.99 |
| 010yr-06hr | 3.03 | 43.07 | 9.807 | 2.48 |
| 010yr-12hr | 3.52 | 22.81 | 11.706 | 2.96 |
| 010yr-24hr | 4.08 | 16.31 | 13.887 | 3.51 |
| 100 Yr-SCS 24Hr | 5.91 | 341.02 | 21.056 | 5.32 |
| 100yr-0.17hr | 1.25 | 186.38 | 3.103 | 0.78 |
| 100yr-0.25hr | 1.56 | 200.02 | 4.226 | 1.07 |
| 100yr-0.50hr | 2.25 | 226.25 | 6.813 | 1.72 |
| 100yr-01hr | 3.01 | 212.02 | 9.729 | 2.46 |
| 100yr-02hr | 2.65 | 102.43 | 8.342 | 2.11 |
| 100yr-03hr | 3.94 | 115.42 | 13.341 | 3.37 |
| 100yr-06hr | 4.78 | 73.96 | 16.623 | 4.20 |
| 100yr-12hr | 5.37 | 36.22 | 18.936 | 4.79 |
| 100yr-24hr | 5.91 | 24.15 | 21.056 | 5.32 |
| WQV-0.17hr | 1.25 | 186.38 | 3.103 | 0.78 |
| WQV-0.25hr | 1.25 | 147.35 | 3.103 | 0.78 |
| WQV-0.50hr | 1.25 | 94.60 | 3.103 | 0.78 |
| WQV-01hr | 1.25 | 61.87 | 3.103 | 0.78 |
| WQV-02hr | 1.25 | 35.18 | 3.103 | 0.78 |
| WQV-03hr | 1.25 | 24.24 | 3.103 | 0.78 |
| WQV-06hr | 1.25 | 12.41 | 3.103 | 0.78 |
| WQV-12hr | 1.25 | 6.27 | 3.103 | 0.78 |
| WQV-24hr | 1.25 | 4.19 | 3.103 | 0.78 |

Summary for Subcatchment 16S: Basin 1 (South)

Runoff = 341.02 cfs @ 12.01 hrs, Volume= 21.056 af, Depth= 5.32"
Routed to Pond 7P : Wet Pond 1 (South)

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs
Type II 24-Hr 100 Yr-SCS 24Hr Rainfall=5.91"

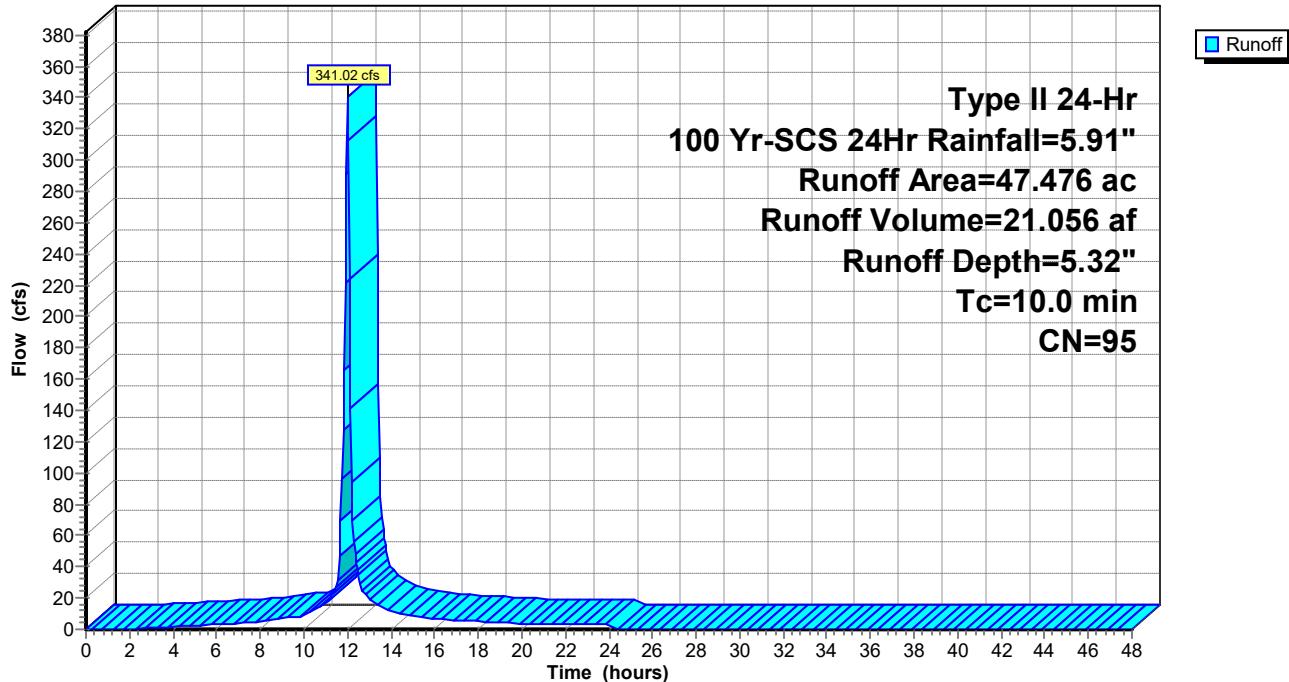
| Area (ac) | CN | Description |
|-----------|----|-------------|
|-----------|----|-------------|

| | | |
|---|--------|----|
| * | 47.476 | 95 |
|---|--------|----|

| | |
|--------|-----------------------|
| 47.476 | 100.00% Pervious Area |
|--------|-----------------------|

| Tc | Length | Slope | Velocity | Capacity | Description |
|-------|--------|---------|----------|----------|-------------|
| (min) | (feet) | (ft/ft) | (ft/sec) | (cfs) | |

| | |
|------|---------------|
| 10.0 | Direct Entry, |
|------|---------------|

Subcatchment 16S: Basin 1 (South)**Hydrograph**

Events for Subcatchment 11S: Ex Site

| Event | Rainfall (inches) | Runoff (cfs) | Volume (acre-feet) | Depth (inches) |
|-----------------|----------------------|-----------------|-----------------------|-------------------|
| 002yr-0.17hr | 0.69 | 0.00 | 0.000 | 0.00 |
| 002yr-0.25hr | 0.85 | 0.33 | 0.057 | 0.01 |
| 002yr-0.50hr | 1.13 | 2.54 | 0.444 | 0.05 |
| 002yr-01hr | 1.39 | 6.05 | 1.077 | 0.11 |
| 002yr-02hr | 1.62 | 9.37 | 1.819 | 0.19 |
| 002yr-03hr | 1.72 | 9.85 | 2.188 | 0.23 |
| 002yr-06hr | 2.05 | 9.98 | 3.577 | 0.37 |
| 002yr-12hr | 2.45 | 9.91 | 5.559 | 0.58 |
| 002yr-24hr | 2.92 | 12.28 | 8.218 | 0.86 |
| 10 Yr-SCS 24Hr | 4.10 | 50.99 | 15.998 | 1.67 |
| 010yr-0.17hr | 0.93 | 0.76 | 0.132 | 0.01 |
| 010yr-0.25hr | 1.14 | 2.68 | 0.464 | 0.05 |
| 010yr-0.50hr | 1.59 | 9.79 | 1.714 | 0.18 |
| 010yr-01hr | 2.02 | 19.19 | 3.441 | 0.36 |
| 010yr-02hr | 2.37 | 25.42 | 5.140 | 0.54 |
| 010yr-03hr | 2.53 | 24.96 | 5.989 | 0.63 |
| 010yr-06hr | 3.03 | 21.74 | 8.883 | 0.93 |
| 010yr-12hr | 3.52 | 21.84 | 12.010 | 1.25 |
| 010yr-24hr | 4.08 | 22.56 | 15.856 | 1.66 |
| 100 Yr-SCS 24Hr | 5.91 | 98.87 | 29.785 | 3.11 |
| 100yr-0.17hr | 1.25 | 4.08 | 0.707 | 0.07 |
| 100yr-0.25hr | 1.56 | 9.30 | 1.611 | 0.17 |
| 100yr-0.50hr | 2.25 | 25.88 | 4.532 | 0.47 |
| 100yr-01hr | 3.01 | 48.36 | 8.761 | 0.91 |
| 100yr-02hr | 2.65 | 32.68 | 6.652 | 0.69 |
| 100yr-03hr | 3.94 | 58.75 | 14.871 | 1.55 |
| 100yr-06hr | 4.78 | 47.15 | 20.979 | 2.19 |
| 100yr-12hr | 5.37 | 46.75 | 25.507 | 2.66 |
| 100yr-24hr | 5.91 | 40.28 | 29.785 | 3.11 |
| WQV-0.17hr | 1.25 | 4.08 | 0.707 | 0.07 |
| WQV-0.25hr | 1.25 | 4.08 | 0.707 | 0.07 |
| WQV-0.50hr | 1.25 | 4.04 | 0.707 | 0.07 |
| WQV-01hr | 1.25 | 3.98 | 0.707 | 0.07 |
| WQV-02hr | 1.25 | 3.79 | 0.707 | 0.07 |
| WQV-03hr | 1.25 | 3.48 | 0.707 | 0.07 |
| WQV-06hr | 1.25 | 2.57 | 0.707 | 0.07 |
| WQV-12hr | 1.25 | 1.54 | 0.707 | 0.07 |
| WQV-24hr | 1.25 | 1.20 | 0.707 | 0.07 |

10 YR POST ALLOWABLE
RELEASE, PER CITY OF
FRANKLIN STORMWATER
MANAGEMENT ORDINANCE

100 YR POST ALLOWABLE
RELEASE, PER CITY OF
FRANKLIN STORMWATER
MANAGEMENT ORDINANCE

Summary for Subcatchment 11S: Ex Site

Runoff = **12.28 cfs** @ 18.70 hrs, Volume= 8.218 af, Depth= 0.86"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs. dt= 0.05 hrs
 Indy Huff 3rd Quartile scaled to 24.00 hrs 002yr-24hr Rainfall=2.92"

| Area (ac) | CN | Description |
|-----------|----|--------------------------------------|
| 114.950 | 74 | Pasture/grassland/range, Good, HSG C |
| 114.950 | | 100.00% Pervious Area |

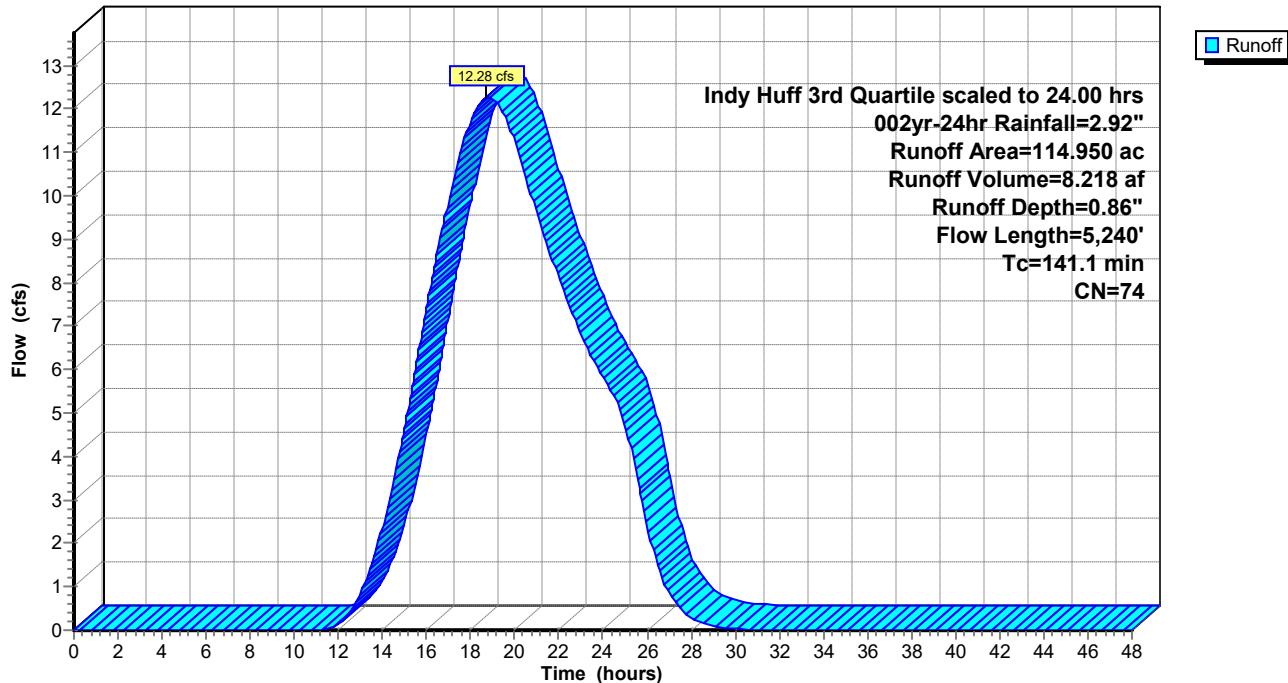
10 YR POST ALLOWABLE RELEASE, PER CITY OF FRANKLIN STORMWATER MANAGEMENT ORDINANCE

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|-------------|------------------|------------------|----------------------|-------------------|---|
| 6.5 | 100 | 0.0100 | 0.26 | | Sheet Flow, Cultivated: Residue<=20% n= 0.060 P2= 2.91" |
| 134.6 | 5,140 | 0.0050 | 0.64 | | Shallow Concentrated Flow, Cultivated Straight Rows Kv= 9.0 fps |
| 141.1 | 5,240 | Total | | | |

+—————
 Subcatchment 11S: Ex Site

Subcatchment 11S: Ex Site

Hydrograph



Summary for Subcatchment 11S: Ex Site

Runoff = **25.42 cfs** @ 3.02 hrs, Volume= 5.140 af, Depth= 0.54"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs
 Indy Huff 1st Quartile scaled to 2.00 hrs 010yr-02hr Rainfall=2.37"

| Area (ac) | CN | Description |
|-----------|----|--------------------------------------|
| 114.950 | 74 | Pasture/grassland/range, Good, HSG C |
| 114.950 | | 100.00% Pervious Area |

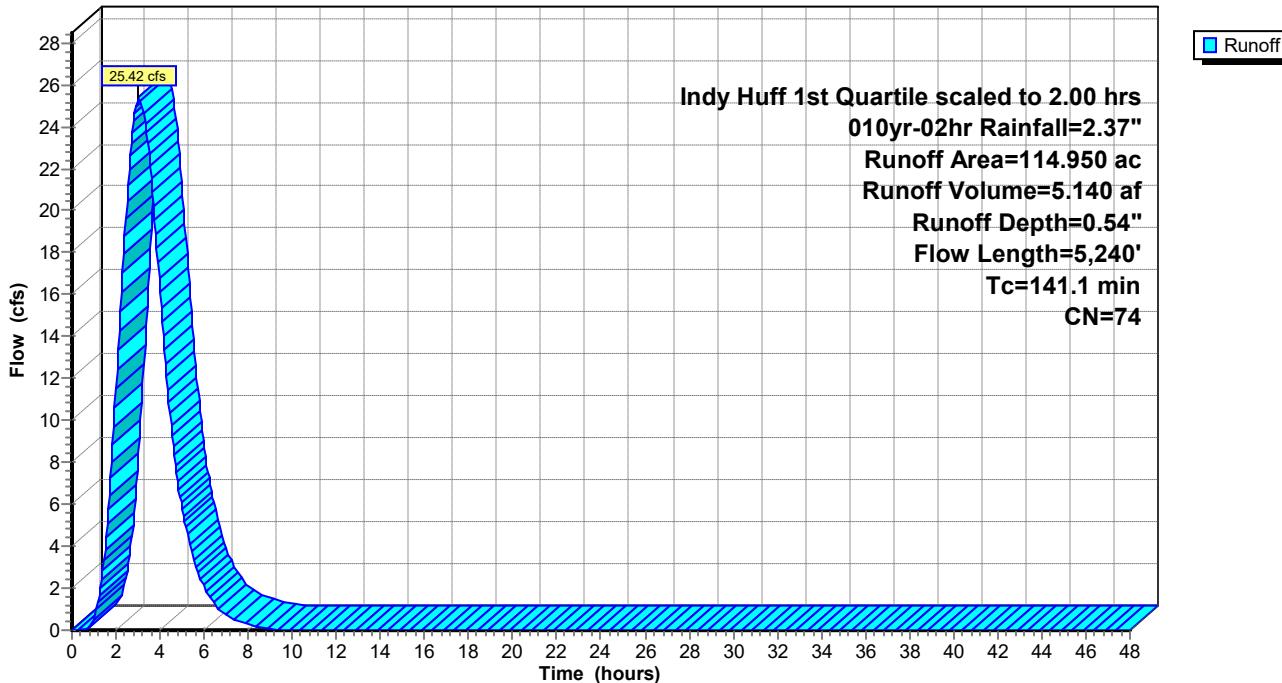
100 YR POST ALLOWABLE RELEASE, PER CITY OF FRANKLIN STORMWATER MANAGEMENT ORDINANCE

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|--------------|------------------|------------------|----------------------|-------------------|---|
| 6.5 | 100 | 0.0100 | 0.26 | | Sheet Flow, Cultivated: Residue<=20% n= 0.060 P2= 2.91" |
| 134.6 | 5,140 | 0.0050 | 0.64 | | Shallow Concentrated Flow, Cultivated Straight Rows Kv= 9.0 fps |
| 141.1 | 5,240 | | | Total | |

+—————
 Subcatchment 11S: Ex Site

Subcatchment 11S: Ex Site

Hydrograph



Events for Pond 7P: Wet Pond 1 (South)

| Event | Inflow (cfs) | Primary (cfs) | Elevation (feet) | Storage (cubic-feet) |
|------------------------|-----------------|------------------|---------------------|-------------------------|
| 002yr-0.17hr | 77.32 | 0.39 | 771.78 | 113,442 |
| 002yr-0.25hr | 88.92 | 0.77 | 771.89 | 161,109 |
| 002yr-0.50hr | 85.69 | 1.72 | 772.11 | 250,002 |
| 002yr-01hr | 78.60 | 2.90 | 772.32 | 336,246 |
| 002yr-02hr | 58.33 | 4.07 | 772.50 | 414,260 |
| 002yr-03hr | 45.55 | 4.59 | 772.58 | 447,984 |
| 002yr-06hr | 34.06 | 6.08 | 772.84 | 555,948 |
| 002yr-12hr | 33.74 | 7.22 | 773.11 | 672,686 |
| 002yr-24hr | 29.60 | 8.28 | 773.40 | 794,865 |
| 10 Yr-SCS 24Hr | 279.53 | 10.98 | 774.28 | 1,180,737 |
| 010yr-0.17hr | 126.46 | 1.00 | 771.95 | 185,933 |
| 010yr-0.25hr | 138.07 | 1.76 | 772.12 | 253,269 |
| 010yr-0.50hr | 144.04 | 3.92 | 772.48 | 404,325 |
| 010yr-01hr | 135.22 | 6.07 | 772.84 | 555,674 |
| 010yr-02hr | 99.99 | 7.34 | 773.14 | 685,508 |
| 010yr-03hr | 78.72 | 7.85 | 773.28 | 743,624 |
| 010yr-06hr | 61.68 | 9.18 | 773.67 | 913,490 |
| 010yr-12hr | 53.80 | 10.12 | 773.99 | 1,050,769 |
| 010yr-24hr | 42.34 | 10.99 | 774.28 | 1,181,693 |
| 100 Yr-SCS 24Hr | 415.48 | 25.10 | 775.31 | 1,645,819 |
| 100yr-0.17hr | 196.32 | 2.24 | 772.20 | 289,482 |
| 100yr-0.25hr | 213.64 | 3.76 | 772.46 | 394,036 |
| 100yr-0.50hr | 239.91 | 6.92 | 773.04 | 641,299 |
| 100yr-01hr | 229.29 | 9.32 | 773.72 | 932,520 |
| 100yr-02hr | 116.08 | 8.26 | 773.39 | 792,174 |
| 100yr-03hr | 142.19 | 12.79 | 774.50 | 1,277,145 |
| 100yr-06hr | 114.70 | 20.14 | 775.03 | 1,517,581 |
| 100yr-12hr | 87.70 | 23.63 | 775.23 | 1,609,230 |
| 100yr-24hr | 61.05 | 24.05 | 775.26 | 1,619,833 |
| WQV-0.17hr | 196.32 | 2.24 | 772.20 | 289,482 |
| WQV-0.25hr | 157.47 | 2.24 | 772.20 | 289,482 |
| WQV-0.50hr | 100.39 | 2.24 | 772.20 | 289,478 |
| WQV-01hr | 66.63 | 2.24 | 772.20 | 289,452 |
| WQV-02hr | 39.18 | 2.23 | 772.20 | 289,305 |
| WQV-03hr | 27.85 | 2.23 | 772.20 | 289,026 |
| WQV-06hr | 15.35 | 2.21 | 772.20 | 287,409 |
| WQV-12hr | 11.85 | 2.16 | 772.19 | 283,695 |
| WQV-24hr | 9.70 | 2.10 | 772.18 | 279,283 |

Summary for Pond 7P: Wet Pond 1 (South)

Inflow Area = 133.238 ac, 0.00% Impervious, Inflow Depth > 3.48" for 010yr-24hr event
 Inflow = 42.34 cfs @ 16.88 hrs, Volume= 38.600 af
 Outflow = 10.99 cfs @ 24.17 hrs, Volume= 25.582 af, Atten= 74%, Lag= 437.4 min
 Primary = 10.99 cfs @ 24.17 hrs, Volume= 25.582 af
 Routed to nonexistent node 20L

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs
 Peak Elev= 774.28' @ 24.17 hrs Surf.Area= 443,271 sf Storage= 1,181,693 cf

Plug-Flow detention time= 942.4 min calculated for 25.582 af (66% of inflow)
 Center-of-Mass det. time= 760.0 min (1,789.6 - 1,029.6)

| Volume | Invert | Avail.Storage | Storage Description |
|---------------------|----------------------|---------------------------|--|
| #1 | 771.50' | 2,921,766 cf | Custom Stage Data (Prismatic) Listed below (Recalc) |
| Elevation (feet) | Surf.Area (sq-ft) | Inc.Store (cubic-feet) | Cum.Store (cubic-feet) |
| 771.50 | 406,211 | 0 | 0 |
| 778.00 | 492,794 | 2,921,766 | 2,921,766 |

| Device | Routing | Invert | Outlet Devices |
|--------|---------|---------|---|
| #1 | Primary | 771.50' | 17.0" Vert. Orifice/Grate C= 0.600 Limited to weir flow at low heads |
| #2 | Primary | 774.25' | 40.0" W x 24.0" H Vert. Orifice/Grate C= 0.600 Limited to weir flow at low heads |

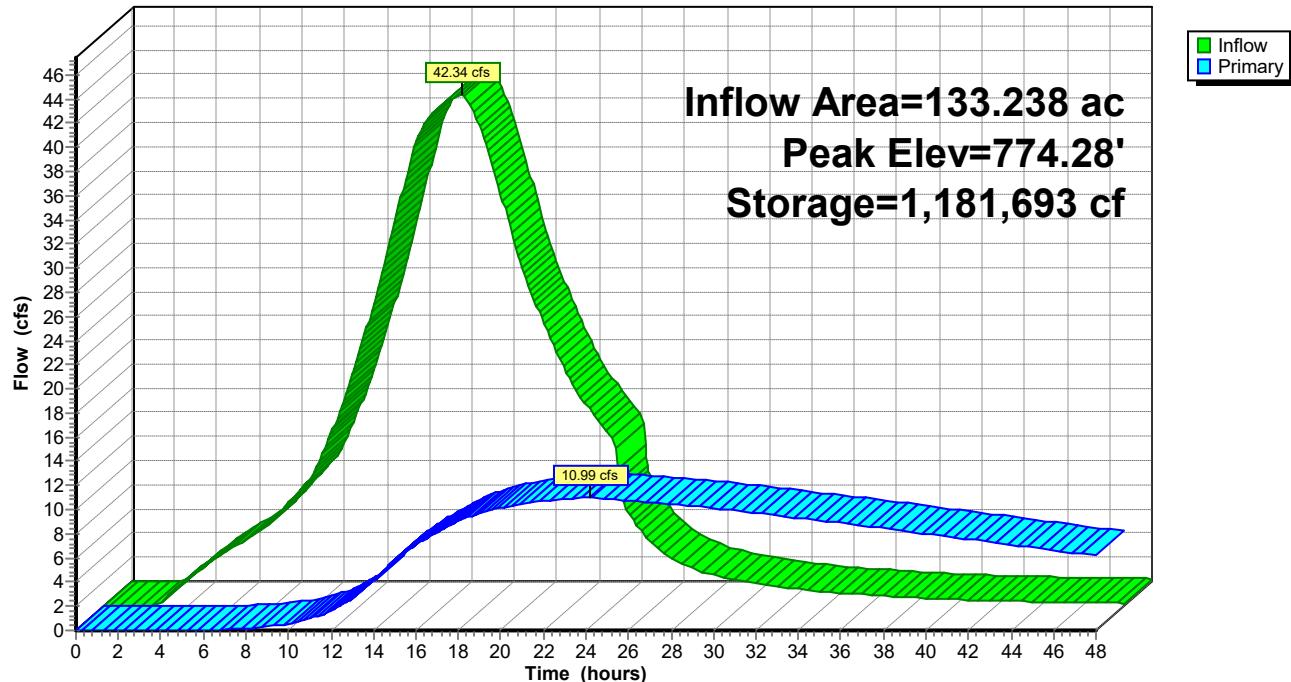
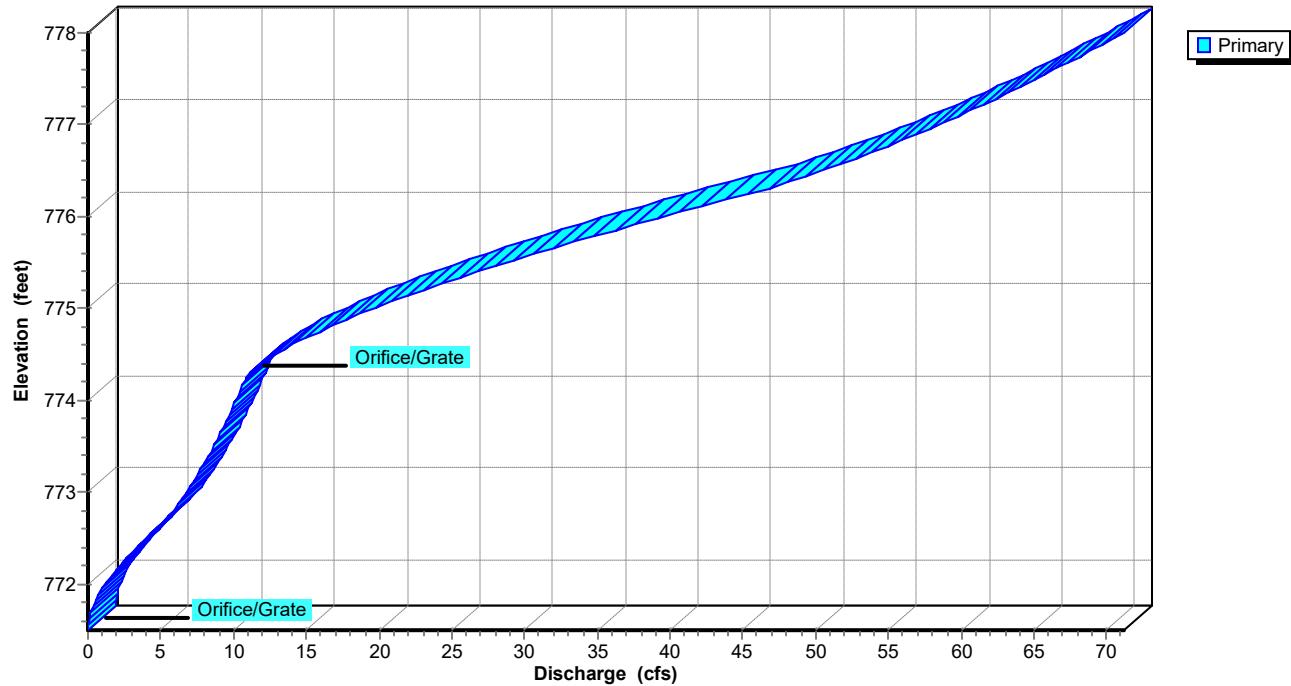
Primary OutFlow Max=10.99 cfs @ 24.17 hrs HW=774.28' (Free Discharge)

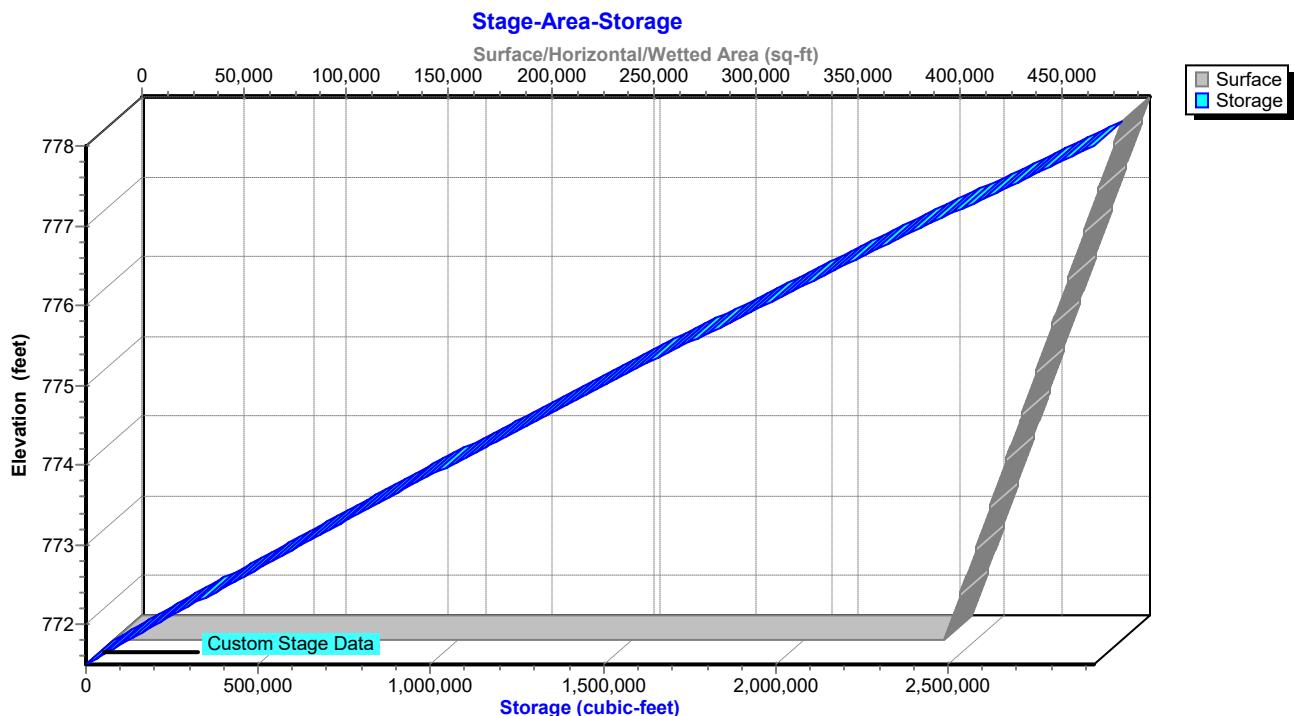
↑ 1=Orifice/Grate (Orifice Controls 10.93 cfs @ 6.93 fps)
 ↓ 2=Orifice/Grate (Orifice Controls 0.06 cfs @ 0.58 fps)

Pond 7P: Wet Pond 1 (South)

Orifice/Grate

Orifice/Grate

Pond 7P: Wet Pond 1 (South)**Hydrograph****Pond 7P: Wet Pond 1 (South)****Stage-Discharge**

Pond 7P: Wet Pond 1 (South)

Summary for Pond 7P: Wet Pond 1 (South)

Inflow Area = 133.238 ac, 0.00% Impervious, Inflow Depth > 5.28" for 100 Yr-SCS 24Hr event

Inflow = 415.48 cfs @ 12.01 hrs, Volume= 58.610 af

Outflow = 25.10 cfs @ 16.74 hrs, Volume= 42.456 af, Atten= 94%, Lag= 283.4 min

Primary = 25.10 cfs @ 16.74 hrs, Volume= 42.456 af

Routed to nonexistent node 20L

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

Peak Elev= 775.31' @ 16.74 hrs Surf.Area= 457,005 sf Storage= 1,645,819 cf

Plug-Flow detention time= 845.4 min calculated for 42.456 af (72% of inflow)

Center-of-Mass det. time= 687.0 min (1,583.3 - 896.3)

| Volume | Invert | Avail.Storage | Storage Description |
|---------------------|----------------------|---------------------------|---|
| # | | | Custom Stage Data (Prismatic) Listed below (Recalc) |
| Elevation (feet) | Surf.Area (sq-ft) | Inc.Store (cubic-feet) | Cum.Store (cubic-feet) |
| 771.50 | 406,211 | 0 | 0 |
| 778.00 | 492,794 | 2,921,766 | 2,921,766 |

| Device | Routing | Invert | Outlet Devices |
|--------|---------|---------|--|
| #1 | Primary | 771.50' | 17.0" Vert. Orifice/Grate C= 0.600 Limited to weir flow at low heads |
| #2 | Primary | 774.25' | 40.0" W x 24.0" H Vert. Orifice/Grate C= 0.600 Limited to weir flow at low heads |

Primary OutFlow Max=25.10 cfs @ 16.74 hrs HW=775.31' (Free Discharge)

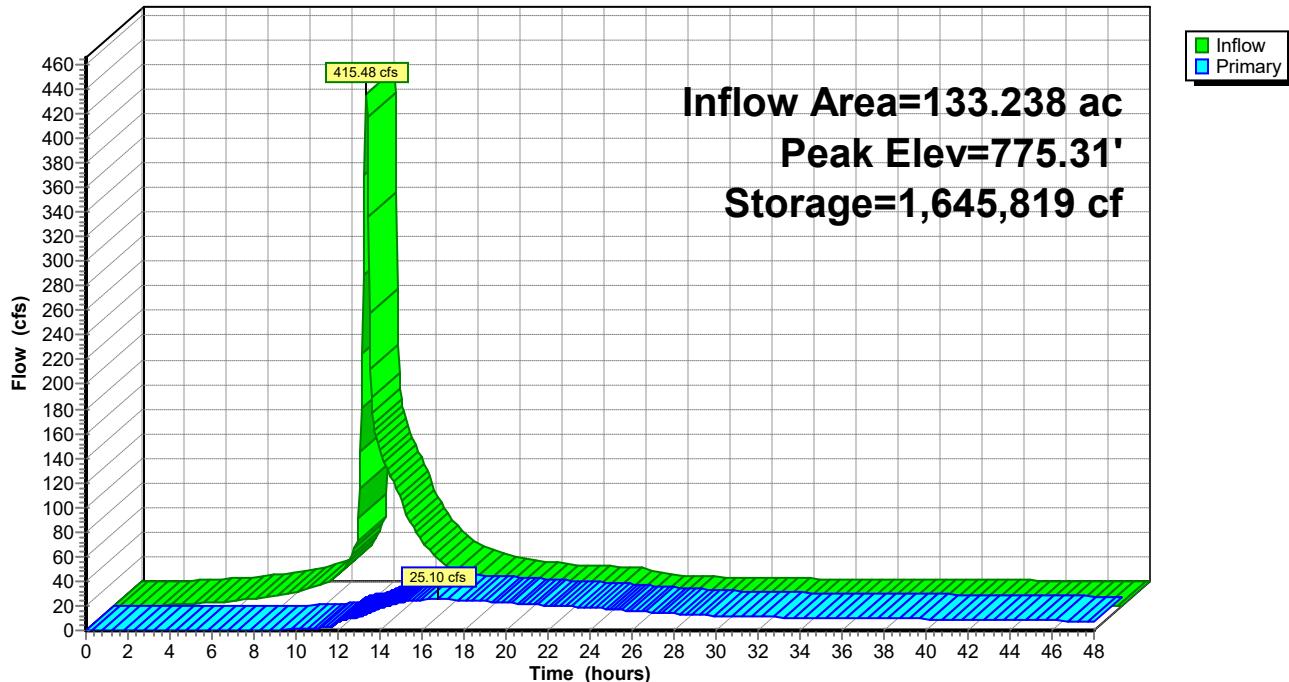
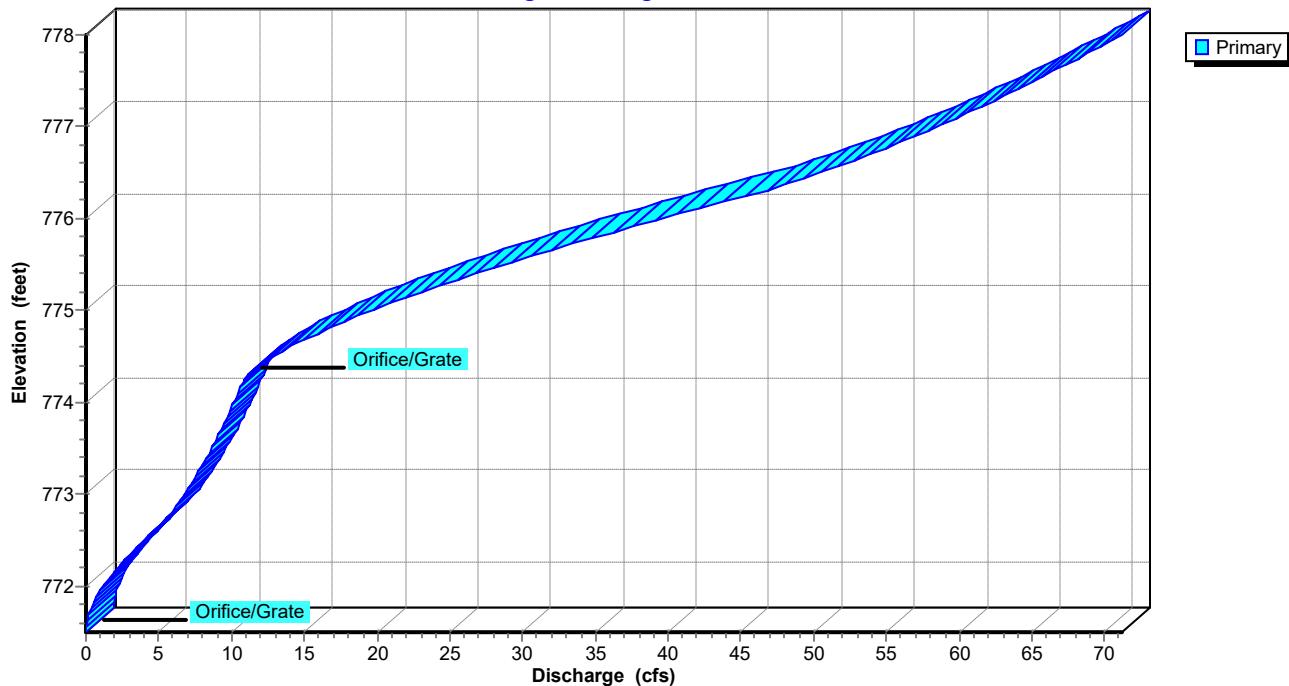
1=Orifice/Grate (Orifice Controls 13.37 cfs @ 8.48 fps)

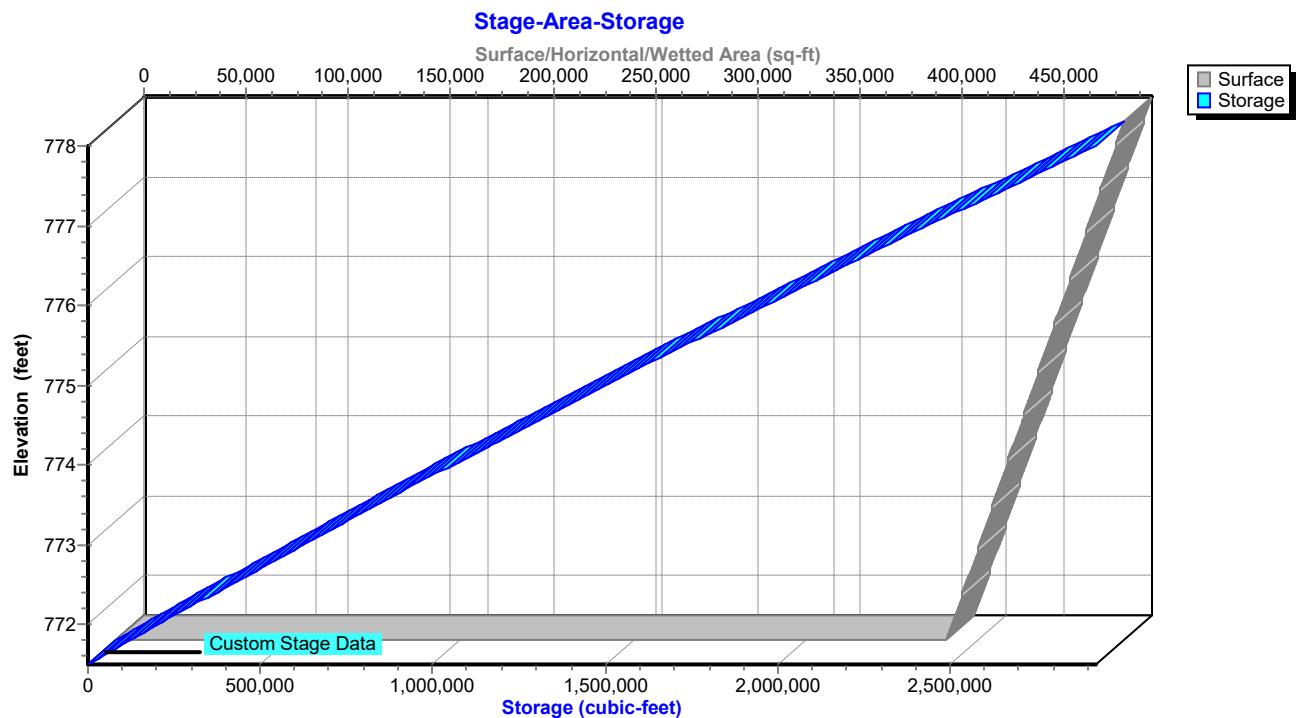
2=Orifice/Grate (Orifice Controls 11.73 cfs @ 3.31 fps)

Pond 7P: Wet Pond 1 (South)

Orifice/Grate

Orifice/Grate

Pond 7P: Wet Pond 1 (South)**Hydrograph****Pond 7P: Wet Pond 1 (South)****Stage-Discharge**

Pond 7P: Wet Pond 1 (South)

Events for Pond 17P: EDDB Pond 2 (Middle)

| Event | Inflow (cfs) | Primary (cfs) | Elevation (feet) | Storage (cubic-feet) |
|------------------------|-----------------|------------------|---------------------|-------------------------|
| 002yr-0.17hr | 19.26 | 7.23 | 773.90 | 9,785 |
| 002yr-0.25hr | 23.47 | 10.89 | 774.10 | 14,647 |
| 002yr-0.50hr | 28.78 | 18.72 | 774.45 | 25,016 |
| 002yr-01hr | 32.40 | 26.02 | 774.72 | 34,119 |
| 002yr-02hr | 29.45 | 27.82 | 774.78 | 36,312 |
| 002yr-03hr | 25.28 | 24.67 | 774.67 | 32,465 |
| 002yr-06hr | 19.55 | 19.32 | 774.47 | 25,789 |
| 002yr-12hr | 21.21 | 20.87 | 774.53 | 27,746 |
| 002yr-24hr | 18.96 | 18.52 | 774.49 | 26,226 |
| 10 Yr-SCS 24Hr | 124.40 | 77.12 | 776.23 | 99,067 |
| 010yr-0.17hr | 32.64 | 13.25 | 774.22 | 17,810 |
| 010yr-0.25hr | 39.55 | 19.81 | 774.49 | 26,413 |
| 010yr-0.50hr | 54.48 | 36.48 | 775.06 | 46,753 |
| 010yr-01hr | 58.98 | 49.54 | 775.45 | 62,555 |
| 010yr-02hr | 51.15 | 49.09 | 775.44 | 62,005 |
| 010yr-03hr | 43.11 | 42.36 | 775.24 | 53,819 |
| 010yr-06hr | 37.03 | 35.12 | 775.02 | 45,118 |
| 010yr-12hr | 34.19 | 33.76 | 774.98 | 43,475 |
| 010yr-24hr | 27.26 | 26.41 | 774.90 | 40,663 |
| 100 Yr-SCS 24Hr | 178.30 | 100.55 | 777.00 | 141,561 |
| 100yr-0.17hr | 54.05 | 24.07 | 774.65 | 31,729 |
| 100yr-0.25hr | 68.55 | 36.47 | 775.06 | 46,733 |
| 100yr-0.50hr | 94.63 | 63.97 | 775.86 | 80,841 |
| 100yr-01hr | 98.40 | 83.65 | 776.42 | 109,075 |
| 100yr-02hr | 59.21 | 56.90 | 775.66 | 71,729 |
| 100yr-03hr | 76.91 | 72.85 | 776.11 | 92,927 |
| 100yr-06hr | 69.63 | 65.92 | 775.91 | 83,432 |
| 100yr-12hr | 56.05 | 54.95 | 775.67 | 72,357 |
| 100yr-24hr | 39.40 | 37.48 | 775.62 | 69,913 |
| WQV-0.17hr | 54.05 | 24.07 | 774.65 | 31,729 |
| WQV-0.25hr | 46.55 | 23.87 | 774.64 | 31,476 |
| WQV-0.50hr | 35.05 | 23.01 | 774.61 | 30,420 |
| WQV-01hr | 26.68 | 21.14 | 774.54 | 28,086 |
| WQV-02hr | 19.25 | 17.64 | 774.40 | 23,631 |
| WQV-03hr | 15.26 | 14.75 | 774.28 | 19,830 |
| WQV-06hr | 9.54 | 9.43 | 774.03 | 12,695 |
| WQV-12hr | 7.07 | 6.95 | 773.88 | 9,406 |
| WQV-24hr | 6.03 | 5.99 | 773.82 | 8,136 |

Summary for Pond 17P: EDDB Pond 2 (Middle)

Inflow Area = 85.762 ac, 0.00% Impervious, Inflow Depth > 5.26" for 100 Yr-SCS 24Hr event

Inflow = 178.30 cfs @ 12.02 hrs, Volume= 37.591 af

Outflow = 100.55 cfs @ 12.42 hrs, Volume= 37.554 af, Atten= 44%, Lag= 23.7 min

Primary = 100.55 cfs @ 12.42 hrs, Volume= 37.554 af

Routed to Pond 7P : Wet Pond 1 (South)

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

Peak Elev= 777.00' @ 12.42 hrs Surf.Area= 59,097 sf Storage= 141,561 cf

Plug-Flow detention time= 49.0 min calculated for 37.554 af (100% of inflow)

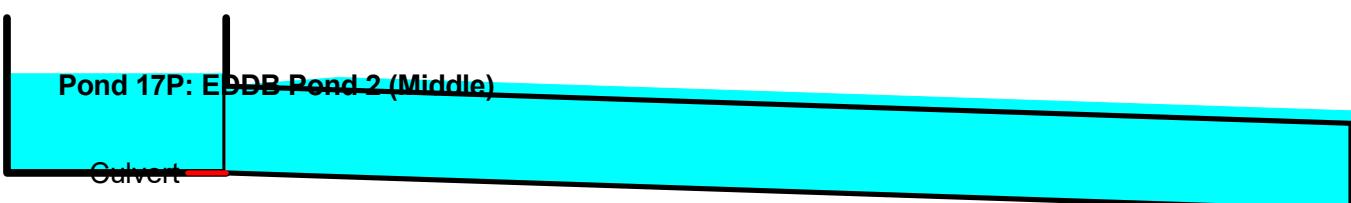
Center-of-Mass det. time= 47.1 min (970.5 - 923.4)

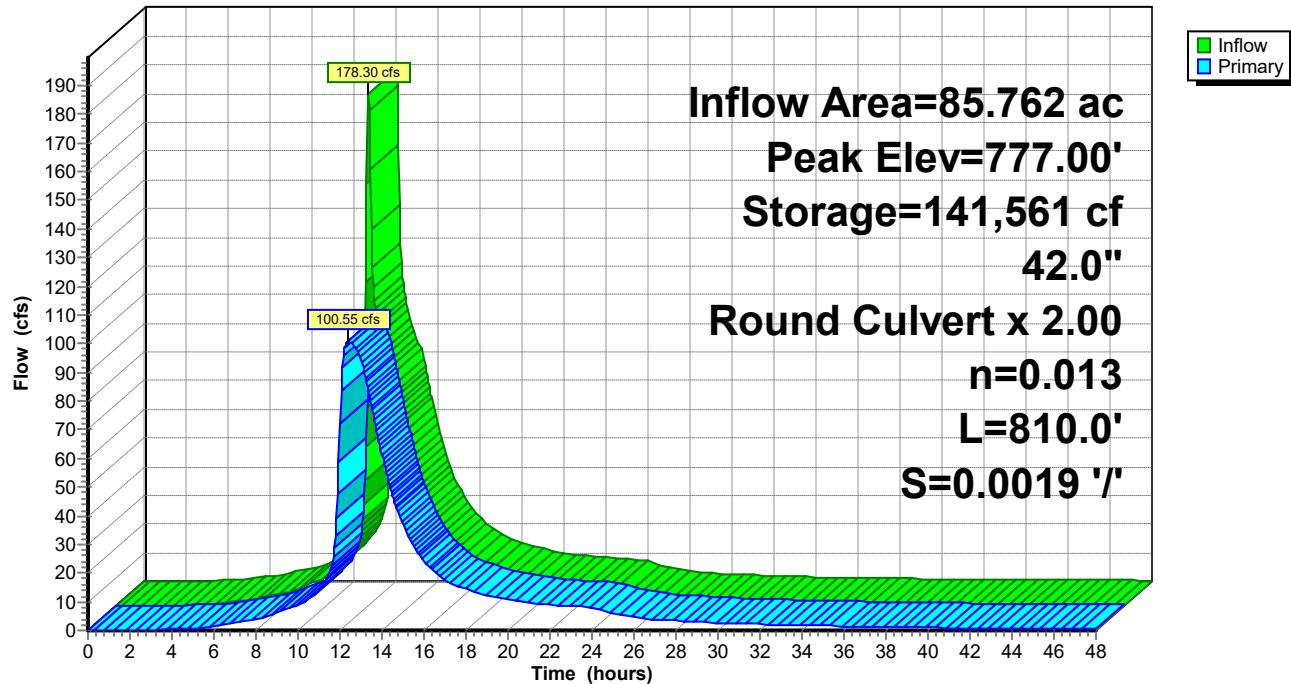
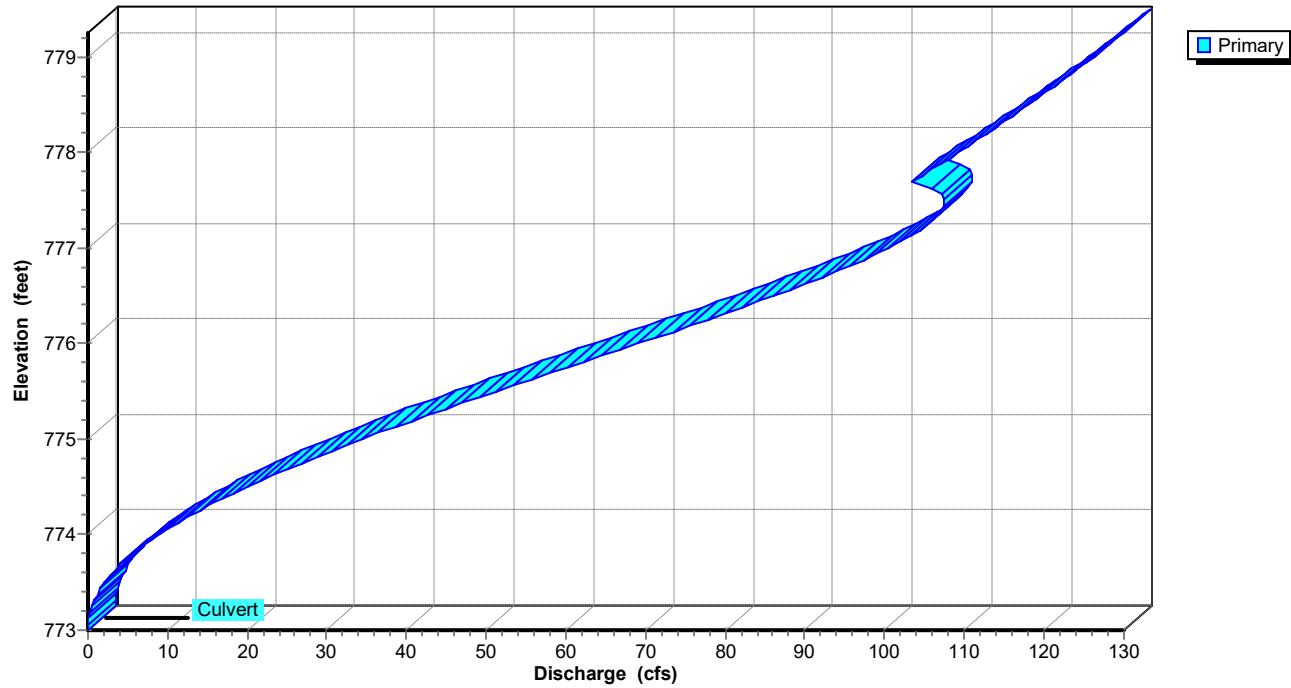
| Volume | Invert | Avail.Storage | Storage Description |
|--------|---------|---------------|--|
| #1 | 773.00' | 296,520 cf | Custom Stage Data (Prismatic) Listed below (Recalc) |

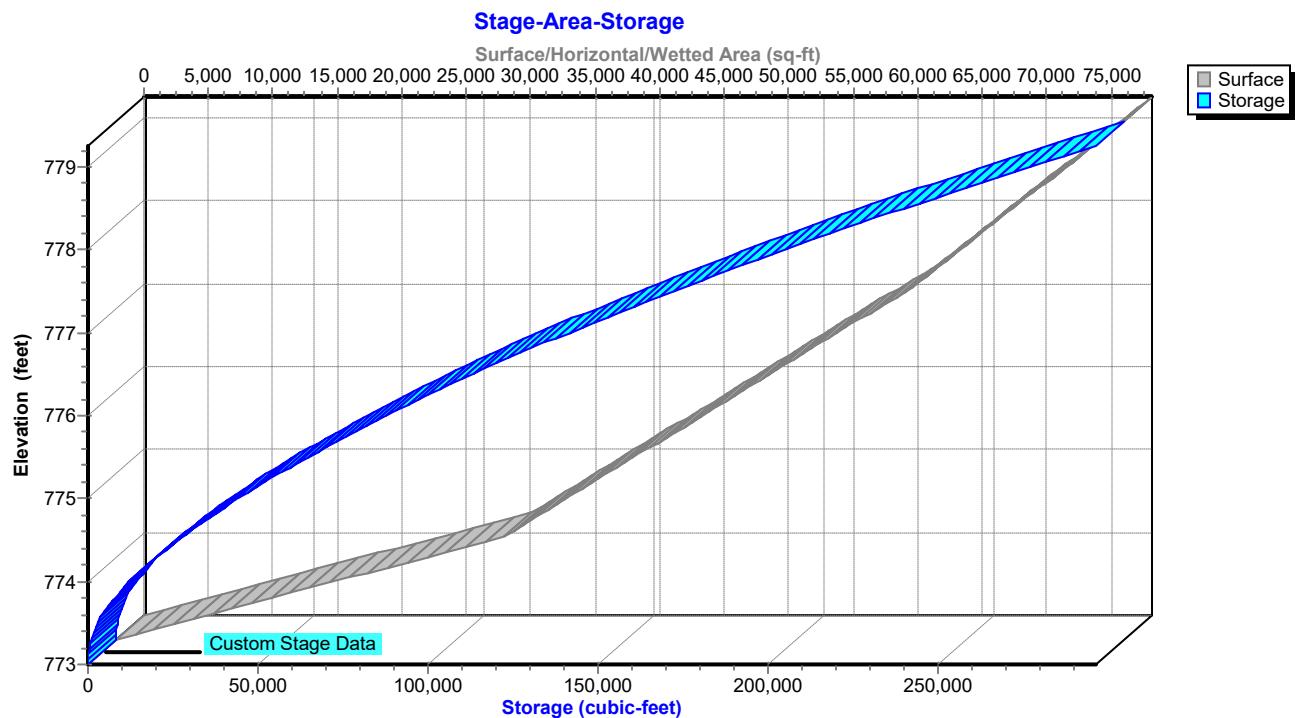
| Elevation (feet) | Surf.Area (sq-ft) | Inc.Store (cubic-feet) | Cum.Store (cubic-feet) |
|---------------------|----------------------|---------------------------|---------------------------|
| 773.00 | 0 | 0 | 0 |
| 774.25 | 30,144 | 18,840 | 18,840 |
| 777.25 | 61,725 | 137,804 | 156,644 |
| 779.25 | 78,151 | 139,876 | 296,520 |

| Device | Routing | Invert | Outlet Devices |
|--------|---------|---------|--|
| #1 | Primary | 773.00' | 42.0" Round Culvert X 2.00 L= 810.0' RCP, groove end projecting, Ke= 0.200 Inlet / Outlet Invert= 773.00' / 771.50' S= 0.0019 '/' Cc= 0.900 n= 0.013, Flow Area= 9.62 sf |

Primary OutFlow Max=100.54 cfs @ 12.42 hrs HW=777.00' TW=773.72' (Dynamic Tailwater)
 ↑1=Culvert (Barrel Controls 100.54 cfs @ 5.73 fps)



Pond 17P: EDDB Pond 2 (Middle)**Hydrograph****Pond 17P: EDDB Pond 2 (Middle)****Stage-Discharge**

Pond 17P: EDDB Pond 2 (Middle)

Events for Pond 18P: Wet Pond 3 (North)

| Event | Inflow (cfs) | Primary (cfs) | Elevation (feet) | Storage (acre-feet) |
|------------------------|-----------------|------------------|---------------------|------------------------|
| 002yr-0.17hr | 115.53 | 4.60 | 774.68 | 1.793 |
| 002yr-0.25hr | 129.97 | 8.64 | 774.94 | 2.493 |
| 002yr-0.50hr | 125.94 | 17.90 | 775.36 | 3.688 |
| 002yr-01hr | 113.79 | 24.75 | 775.64 | 4.506 |
| 002yr-02hr | 81.37 | 24.76 | 775.68 | 4.600 |
| 002yr-03hr | 61.32 | 21.49 | 775.55 | 4.228 |
| 002yr-06hr | 40.32 | 16.77 | 775.34 | 3.632 |
| 002yr-12hr | 23.43 | 18.16 | 775.40 | 3.810 |
| 002yr-24hr | 17.64 | 16.27 | 775.33 | 3.589 |
| 10 Yr-SCS 24Hr | 361.52 | 79.49 | 777.40 | 9.997 |
| 010yr-0.17hr | 187.73 | 11.16 | 775.07 | 2.863 |
| 010yr-0.25hr | 201.69 | 18.97 | 775.40 | 3.810 |
| 010yr-0.50hr | 217.72 | 37.06 | 776.05 | 5.707 |
| 010yr-01hr | 195.02 | 46.75 | 776.44 | 6.907 |
| 010yr-02hr | 138.21 | 43.15 | 776.38 | 6.722 |
| 010yr-03hr | 104.05 | 36.88 | 776.16 | 6.036 |
| 010yr-06hr | 67.23 | 31.02 | 775.92 | 5.334 |
| 010yr-12hr | 35.61 | 29.33 | 775.87 | 5.172 |
| 010yr-24hr | 25.46 | 23.36 | 775.68 | 4.599 |
| 100 Yr-SCS 24Hr | 532.34 | 97.03 | 778.78 | 14.760 |
| 100yr-0.17hr | 290.94 | 23.73 | 775.58 | 4.333 |
| 100yr-0.25hr | 312.23 | 38.09 | 776.06 | 5.744 |
| 100yr-0.50hr | 353.19 | 66.32 | 776.98 | 8.615 |
| 100yr-01hr | 330.96 | 77.87 | 777.62 | 10.703 |
| 100yr-02hr | 159.89 | 49.96 | 776.63 | 7.498 |
| 100yr-03hr | 180.17 | 63.17 | 777.14 | 9.137 |
| 100yr-06hr | 115.46 | 58.23 | 776.92 | 8.427 |
| 100yr-12hr | 56.54 | 48.11 | 776.58 | 7.339 |
| 100yr-24hr | 37.69 | 33.63 | 776.22 | 6.232 |
| WQV-0.17hr | 290.94 | 23.73 | 775.58 | 4.333 |
| WQV-0.25hr | 230.02 | 23.61 | 775.58 | 4.315 |
| WQV-0.50hr | 147.68 | 22.64 | 775.54 | 4.216 |
| WQV-01hr | 96.58 | 20.06 | 775.46 | 3.960 |
| WQV-02hr | 54.92 | 15.90 | 775.29 | 3.485 |
| WQV-03hr | 37.85 | 12.97 | 775.16 | 3.105 |
| WQV-06hr | 19.37 | 8.18 | 774.90 | 2.386 |
| WQV-12hr | 9.79 | 6.02 | 774.76 | 2.013 |
| WQV-24hr | 6.54 | 5.18 | 774.70 | 1.854 |

Summary for Pond 18P: Wet Pond 3 (North)

Inflow Area = 74.111 ac, 0.00% Impervious, Inflow Depth = 5.32" for 100 Yr-SCS 24Hr event

Inflow = 532.34 cfs @ 12.01 hrs, Volume= 32.869 af

Outflow = 97.03 cfs @ 12.10 hrs, Volume= 32.424 af, Atten= 82%, Lag= 5.8 min

Primary = 97.03 cfs @ 12.10 hrs, Volume= 32.424 af

Routed to Pond 17P : EDDB Pond 2 (Middle)

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

Peak Elev= 778.78' @ 12.29 hrs Surf.Area= 3.620 ac Storage= 14.760 af

Plug-Flow detention time= 192.4 min calculated for 32.390 af (99% of inflow)

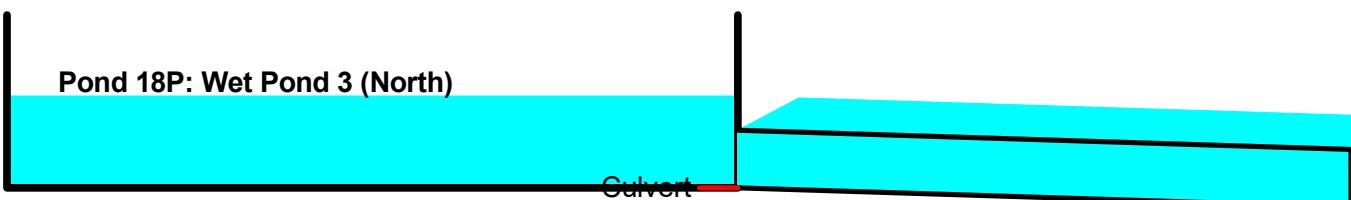
Center-of-Mass det. time= 184.9 min (948.8 - 764.0)

| Volume | Invert | Avail.Storage | Storage Description |
|---------------------|----------------------|--------------------------|--|
| #1 | 774.00' | 32.027 af | Custom Stage Data (Prismatic) Listed below (Recalc) |
| Elevation (feet) | Surf.Area (acres) | Inc.Store (acre-feet) | Cum.Store (acre-feet) |
| 774.00 | 2.558 | 0.000 | 0.000 |
| 783.00 | 4.559 | 32.027 | 32.027 |

| Device | Routing | Invert | Outlet Devices |
|--------|---------|---------|--|
| #1 | Primary | 774.00' | 36.0" Round Culvert X 2.00 L= 211.0' RCP, groove end projecting, Ke= 0.200 Inlet / Outlet Invert= 774.00' / 773.00' S= 0.0047 '/' Cc= 0.900 n= 0.013, Flow Area= 7.07 sf |

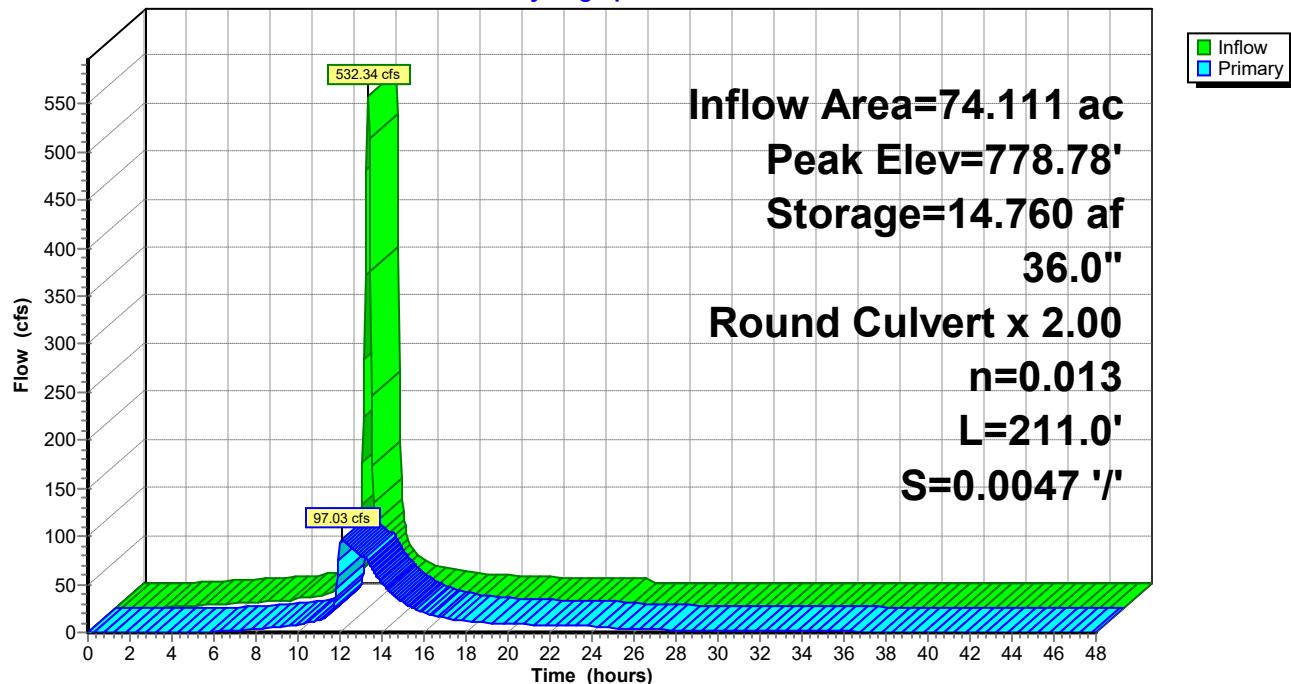
Primary OutFlow Max=90.93 cfs @ 12.10 hrs HW=778.43' TW=776.68' (Dynamic Tailwater)

↑1=Culvert (Outlet Controls 90.93 cfs @ 6.43 fps)

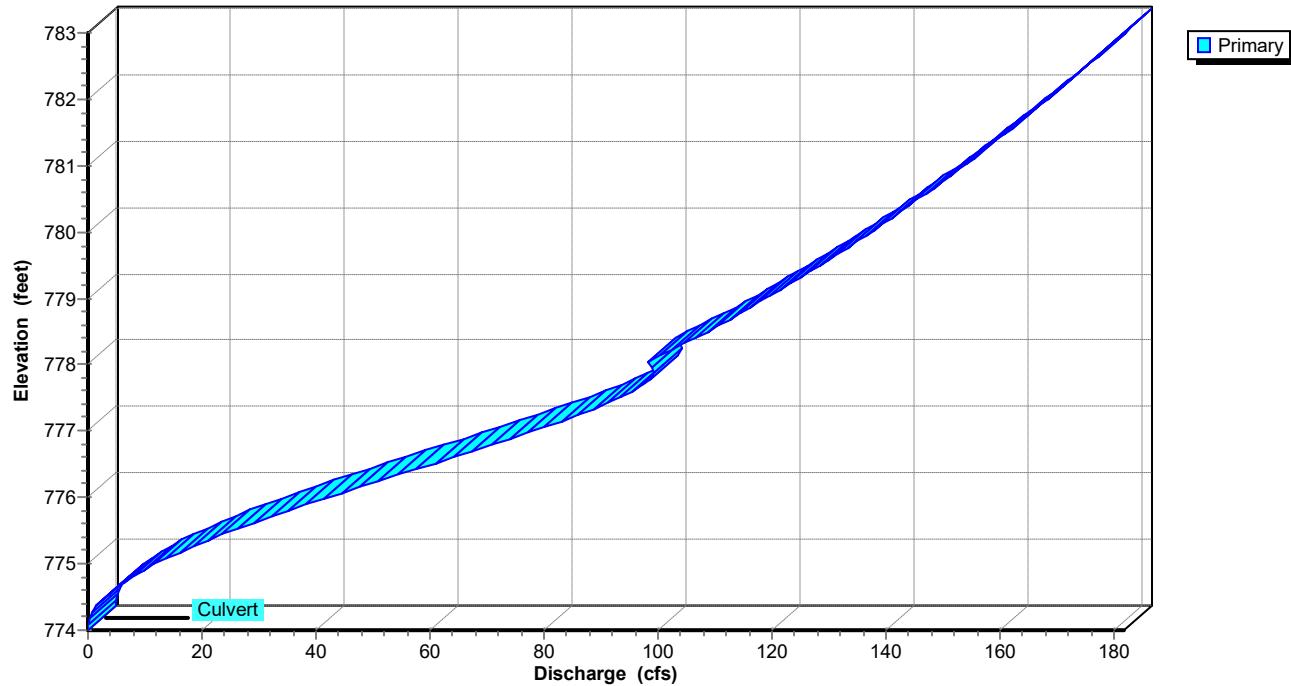


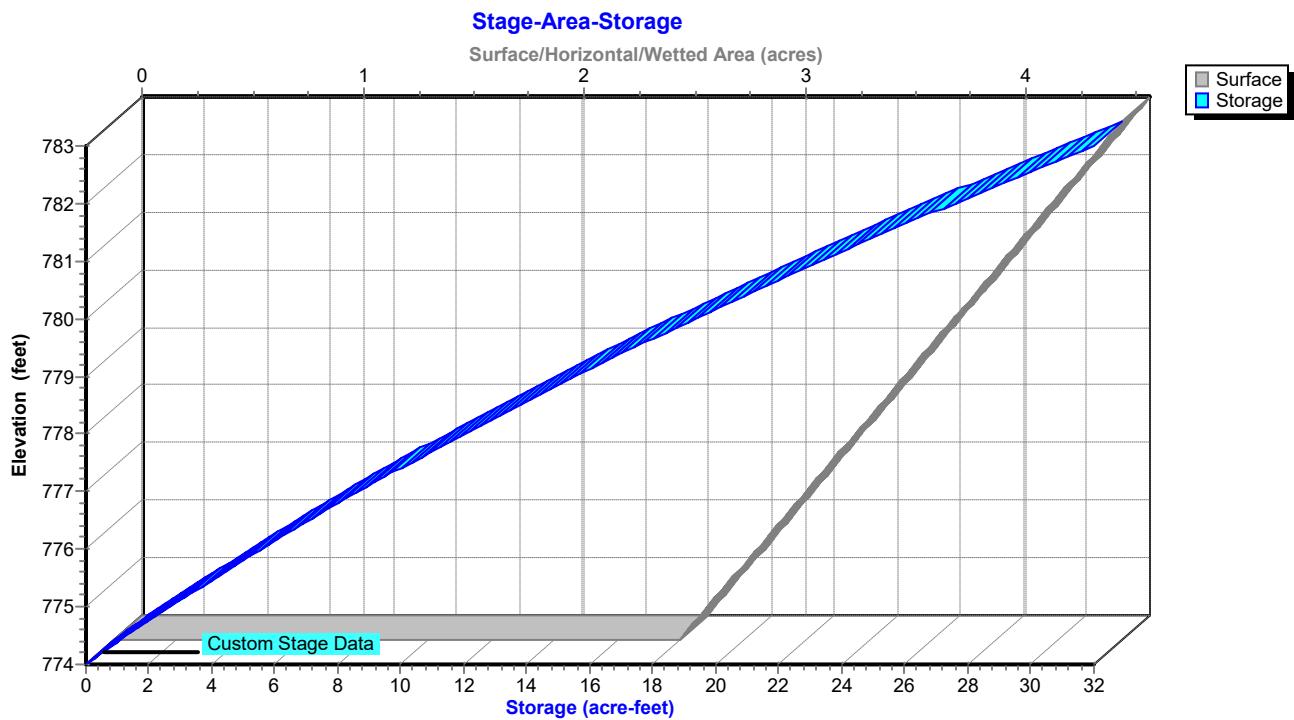
Pond 18P: Wet Pond 3 (North)

Hydrograph

**Pond 18P: Wet Pond 3 (North)**

Stage-Discharge



Pond 18P: Wet Pond 3 (North)

**MODEL/CALCULATIONS
WITH OFFSITE**

Development Site Area
- 114.95 AC

City allowable: 10 to 2,
100 to 10 = 12.28/
25.42



County allowable:
0.1/0.3 = 11.49/ 34.48



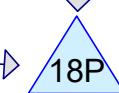
North Offsite



Off-Site Swale



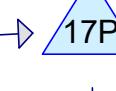
Basin 3 (North)



Wet Pond 3 (North)



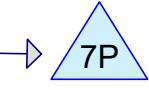
Basin 2 (Middle)



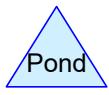
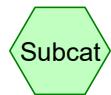
EDDB Pond 2 (Middle)



Basin 1 (South)



Wet Pond 1 (South)



Routing Diagram for Malarkey IND_Huff_R1
Prepared by Kimley-Horn & Associates, Printed 8/7/2024
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Malarkey IND_Huff_R1

Prepared by Kimley-Horn & Associates

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Rainfall Events Listing

| Event# | Event Name | Storm Type | Curve | Mode | Duration (hours) | B/B | Depth (inches) | AMC |
|--------|-----------------|---------------|--------------|---------|------------------|-----|----------------|-----|
| 1 | 002yr-0.17hr | Indy Huff | 1st Quartile | Scale | 0.17 | 1 | 0.69 | 2 |
| 2 | 002yr-0.25hr | Indy Huff | 1st Quartile | Scale | 0.25 | 1 | 0.85 | 2 |
| 3 | 002yr-0.50hr | Indy Huff | 1st Quartile | Scale | 0.50 | 1 | 1.13 | 2 |
| 4 | 002yr-01hr | Indy Huff | 1st Quartile | Scale | 1.00 | 1 | 1.39 | 2 |
| 5 | 002yr-02hr | Indy Huff | 1st Quartile | Scale | 2.00 | 1 | 1.62 | 2 |
| 6 | 002yr-03hr | Indy Huff | 1st Quartile | Scale | 3.00 | 1 | 1.72 | 2 |
| 7 | 002yr-06hr | Indy Huff | 1st Quartile | Scale | 6.00 | 1 | 2.05 | 2 |
| 8 | 002yr-12hr | Indy Huff | 2nd Quartile | Scale | 12.00 | 1 | 2.45 | 2 |
| 9 | 002yr-24hr | Indy Huff | 3rd Quartile | Scale | 24.00 | 1 | 2.92 | 2 |
| 10 | 10 Yr-SCS 24Hr | Type II 24-Hr | | Default | 24.00 | 1 | 4.10 | 2 |
| 11 | 010yr-0.17hr | Indy Huff | 1st Quartile | Scale | 0.17 | 1 | 0.93 | 2 |
| 12 | 010yr-0.25hr | Indy Huff | 1st Quartile | Scale | 0.25 | 1 | 1.14 | 2 |
| 13 | 010yr-0.50hr | Indy Huff | 1st Quartile | Scale | 0.50 | 1 | 1.59 | 2 |
| 14 | 010yr-01hr | Indy Huff | 1st Quartile | Scale | 1.00 | 1 | 2.02 | 2 |
| 15 | 010yr-02hr | Indy Huff | 1st Quartile | Scale | 2.00 | 1 | 2.37 | 2 |
| 16 | 010yr-03hr | Indy Huff | 1st Quartile | Scale | 3.00 | 1 | 2.53 | 2 |
| 17 | 010yr-06hr | Indy Huff | 1st Quartile | Scale | 6.00 | 1 | 3.03 | 2 |
| 18 | 010yr-12hr | Indy Huff | 2nd Quartile | Scale | 12.00 | 1 | 3.52 | 2 |
| 19 | 010yr-24hr | Indy Huff | 3rd Quartile | Scale | 24.00 | 1 | 4.08 | 2 |
| 20 | 100 Yr-SCS 24Hr | Type II 24-Hr | | Default | 24.00 | 1 | 5.91 | 2 |
| 21 | 100yr-0.17hr | Indy Huff | 1st Quartile | Scale | 0.17 | 1 | 1.25 | 2 |
| 22 | 100yr-0.25hr | Indy Huff | 1st Quartile | Scale | 0.25 | 1 | 1.56 | 2 |
| 23 | 100yr-0.50hr | Indy Huff | 1st Quartile | Scale | 0.50 | 1 | 2.25 | 2 |
| 24 | 100yr-01hr | Indy Huff | 1st Quartile | Scale | 1.00 | 1 | 3.01 | 2 |
| 25 | 100yr-02hr | Indy Huff | 1st Quartile | Scale | 2.00 | 1 | 2.65 | 2 |
| 26 | 100yr-03hr | Indy Huff | 1st Quartile | Scale | 3.00 | 1 | 3.94 | 2 |
| 27 | 100yr-06hr | Indy Huff | 1st Quartile | Scale | 6.00 | 1 | 4.78 | 2 |
| 28 | 100yr-12hr | Indy Huff | 2nd Quartile | Scale | 12.00 | 1 | 5.37 | 2 |
| 29 | 100yr-24hr | Indy Huff | 3rd Quartile | Scale | 24.00 | 1 | 5.91 | 2 |
| 30 | WQV-0.17hr | Indy Huff | 1st Quartile | Scale | 0.17 | 1 | 1.25 | 2 |
| 31 | WQV-0.25hr | Indy Huff | 1st Quartile | Scale | 0.25 | 1 | 1.25 | 2 |
| 32 | WQV-0.50hr | Indy Huff | 1st Quartile | Scale | 0.50 | 1 | 1.25 | 2 |
| 33 | WQV-01hr | Indy Huff | 1st Quartile | Scale | 1.00 | 1 | 1.25 | 2 |
| 34 | WQV-02hr | Indy Huff | 1st Quartile | Scale | 2.00 | 1 | 1.25 | 2 |
| 35 | WQV-03hr | Indy Huff | 1st Quartile | Scale | 3.00 | 1 | 1.25 | 2 |
| 36 | WQV-06hr | Indy Huff | 1st Quartile | Scale | 6.00 | 1 | 1.25 | 2 |
| 37 | WQV-12hr | Indy Huff | 2nd Quartile | Scale | 12.00 | 1 | 1.25 | 2 |
| 38 | WQV-24hr | Indy Huff | 3rd Quartile | Scale | 24.00 | 1 | 1.25 | 2 |

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Area Listing (all nodes)

| Area (acres) | CN | Description (subcatchment-numbers) |
|-----------------|-----------|---|
| 133.238 | 95 | (13S, 15S, 16S) |
| 66.930 | 74 | From Paul Hand Drainage Report (Structure 11) (18S) |
| 0.720 | 98 | From Paul Hand Drainage Report (Structure 11) (18S) |
| 114.950 | 74 | Pasture/grassland/range, Good, HSG C (11S) |
| 315.838 | 83 | TOTAL AREA |

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Soil Listing (all nodes)

| Area (acres) | Soil Group | Subcatchment Numbers |
|-----------------|---------------|-------------------------|
| 0.000 | HSG A | |
| 0.000 | HSG B | |
| 114.950 | HSG C | 11S |
| 0.000 | HSG D | |
| 200.888 | Other | 13S, 15S, 16S, 18S |
| 315.838 | | TOTAL AREA |

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Ground Covers (all nodes)

| HSG-A (acres) | HSG-B (acres) | HSG-C (acres) | HSG-D (acres) | Other (acres) | Total (acres) | Ground Cover |
|------------------|------------------|------------------|------------------|------------------|------------------|--|
| 0.000 | 0.000 | 0.000 | 0.000 | 133.238 | 133.238 | |
| 0.000 | 0.000 | 0.000 | 0.000 | 67.650 | 67.650 | From Paul Hand Drainage Report (Structure 11) |
| 0.000 | 0.000 | 114.950 | 0.000 | 0.000 | 114.950 | Pasture/grassland/range, Good |
| 0.000 | 0.000 | 114.950 | 0.000 | 200.888 | 315.838 | TOTAL AREA |

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Pipe Listing (all nodes)

| Line# | Node Number | In-Invert (feet) | Out-Invert (feet) | Length (feet) | Slope (ft/ft) | n | Width (inches) | Diam/Height (inches) | Inside-Fill (inches) | Node Name |
|-------|-------------|---------------------|----------------------|------------------|------------------|-------|-------------------|-------------------------|-------------------------|-----------|
| 1 | 17P | 773.00 | 771.50 | 810.0 | 0.0019 | 0.013 | 0.0 | 42.0 | 0.0 | |
| 2 | 18P | 774.00 | 773.00 | 211.0 | 0.0047 | 0.013 | 0.0 | 36.0 | 0.0 | |

Events for Subcatchment 13S: Basin 3 (North)

| Event | Rainfall (inches) | Runoff (cfs) | Volume (acre-feet) | Depth (inches) |
|-----------------|----------------------|-----------------|-----------------------|-------------------|
| 002yr-0.17hr | 0.69 | 115.53 | 1.901 | 0.31 |
| 002yr-0.25hr | 0.85 | 129.97 | 2.695 | 0.44 |
| 002yr-0.50hr | 1.13 | 125.94 | 4.181 | 0.68 |
| 002yr-01hr | 1.39 | 113.79 | 5.629 | 0.91 |
| 002yr-02hr | 1.62 | 81.37 | 6.943 | 1.12 |
| 002yr-03hr | 1.72 | 61.32 | 7.521 | 1.22 |
| 002yr-06hr | 2.05 | 40.32 | 9.452 | 1.53 |
| 002yr-12hr | 2.45 | 23.43 | 11.826 | 1.91 |
| 002yr-24hr | 2.92 | 17.64 | 14.645 | 2.37 |
| 10 Yr-SCS 24Hr | 4.10 | 361.52 | 21.799 | 3.53 |
| 010yr-0.17hr | 0.93 | 187.73 | 3.109 | 0.50 |
| 010yr-0.25hr | 1.14 | 201.69 | 4.236 | 0.69 |
| 010yr-0.50hr | 1.59 | 217.72 | 6.770 | 1.10 |
| 010yr-01hr | 2.02 | 195.02 | 9.276 | 1.50 |
| 010yr-02hr | 2.37 | 138.21 | 11.349 | 1.84 |
| 010yr-03hr | 2.53 | 104.05 | 12.304 | 1.99 |
| 010yr-06hr | 3.03 | 67.23 | 15.308 | 2.48 |
| 010yr-12hr | 3.52 | 35.61 | 18.273 | 2.96 |
| 010yr-24hr | 4.08 | 25.46 | 21.677 | 3.51 |
| 100 Yr-SCS 24Hr | 5.91 | 532.34 | 32.869 | 5.32 |
| 100yr-0.17hr | 1.25 | 290.94 | 4.843 | 0.78 |
| 100yr-0.25hr | 1.56 | 312.23 | 6.597 | 1.07 |
| 100yr-0.50hr | 2.25 | 353.19 | 10.636 | 1.72 |
| 100yr-01hr | 3.01 | 330.96 | 15.188 | 2.46 |
| 100yr-02hr | 2.65 | 159.89 | 13.023 | 2.11 |
| 100yr-03hr | 3.94 | 180.17 | 20.825 | 3.37 |
| 100yr-06hr | 4.78 | 115.46 | 25.949 | 4.20 |
| 100yr-12hr | 5.37 | 56.54 | 29.560 | 4.79 |
| 100yr-24hr | 5.91 | 37.69 | 32.869 | 5.32 |
| WQV-0.17hr | 1.25 | 290.94 | 4.843 | 0.78 |
| WQV-0.25hr | 1.25 | 230.02 | 4.843 | 0.78 |
| WQV-0.50hr | 1.25 | 147.68 | 4.843 | 0.78 |
| WQV-01hr | 1.25 | 96.58 | 4.843 | 0.78 |
| WQV-02hr | 1.25 | 54.92 | 4.843 | 0.78 |
| WQV-03hr | 1.25 | 37.85 | 4.843 | 0.78 |
| WQV-06hr | 1.25 | 19.37 | 4.843 | 0.78 |
| WQV-12hr | 1.25 | 9.79 | 4.843 | 0.78 |
| WQV-24hr | 1.25 | 6.54 | 4.843 | 0.78 |

Summary for Subcatchment 13S: Basin 3 (North)

Runoff = 532.34 cfs @ 12.01 hrs, Volume= 32.869 af, Depth= 5.32"
Routed to Pond 18P : Wet Pond 3 (North)

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs
Type II 24-Hr 100 Yr-SCS 24Hr Rainfall=5.91"

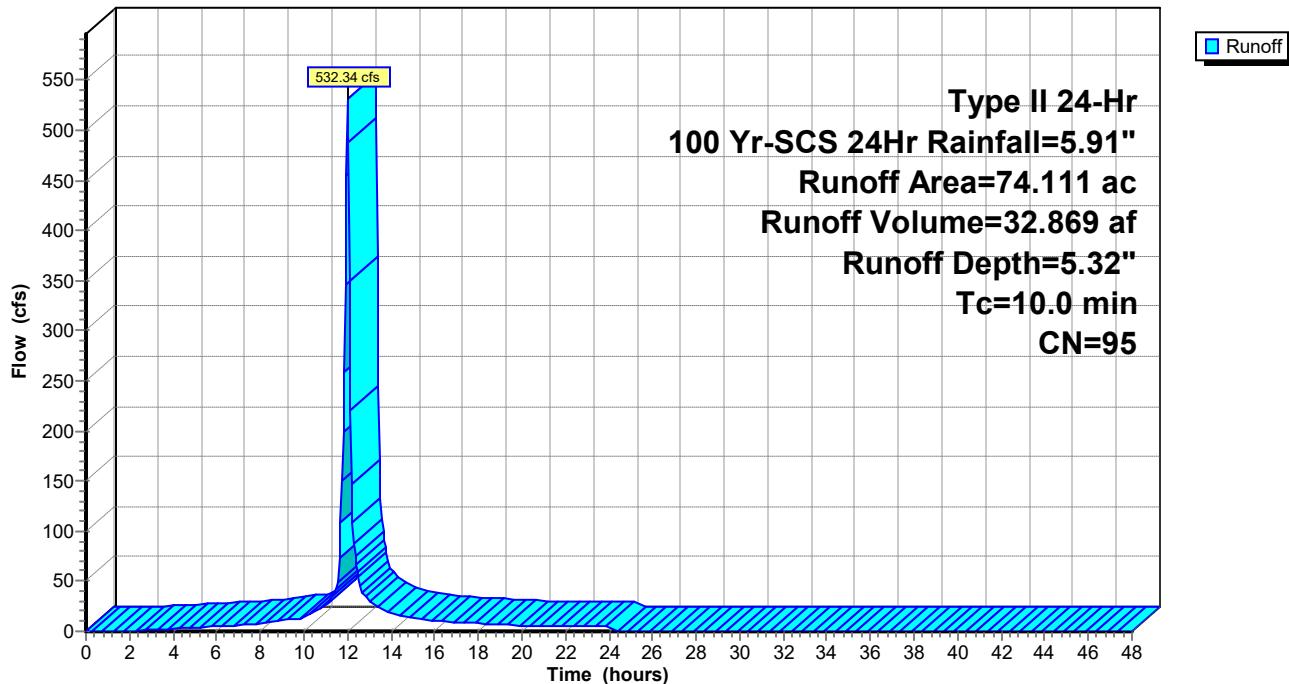
| Area (ac) | CN | Description |
|-----------|----|-------------|
|-----------|----|-------------|

| | | |
|---|--------|----|
| * | 74.111 | 95 |
|---|--------|----|

| | |
|--------|-----------------------|
| 74.111 | 100.00% Pervious Area |
|--------|-----------------------|

| Tc | Length | Slope | Velocity | Capacity | Description |
|-------|--------|---------|----------|----------|-------------|
| (min) | (feet) | (ft/ft) | (ft/sec) | (cfs) | |

| | |
|------|---------------|
| 10.0 | Direct Entry, |
|------|---------------|

Subcatchment 13S: Basin 3 (North)**Hydrograph**

Events for Subcatchment 15S: Basin 2 (Middle)

| Event | Rainfall (inches) | Runoff (cfs) | Volume (acre-feet) | Depth (inches) |
|-----------------|----------------------|-----------------|-----------------------|-------------------|
| 002yr-0.17hr | 0.69 | 18.16 | 0.299 | 0.31 |
| 002yr-0.25hr | 0.85 | 20.43 | 0.424 | 0.44 |
| 002yr-0.50hr | 1.13 | 19.80 | 0.657 | 0.68 |
| 002yr-01hr | 1.39 | 17.89 | 0.885 | 0.91 |
| 002yr-02hr | 1.62 | 12.79 | 1.091 | 1.12 |
| 002yr-03hr | 1.72 | 9.64 | 1.182 | 1.22 |
| 002yr-06hr | 2.05 | 6.34 | 1.486 | 1.53 |
| 002yr-12hr | 2.45 | 3.68 | 1.859 | 1.91 |
| 002yr-24hr | 2.92 | 2.77 | 2.302 | 2.37 |
| 10 Yr-SCS 24Hr | 4.10 | 56.83 | 3.427 | 3.53 |
| 010yr-0.17hr | 0.93 | 29.51 | 0.489 | 0.50 |
| 010yr-0.25hr | 1.14 | 31.71 | 0.666 | 0.69 |
| 010yr-0.50hr | 1.59 | 34.23 | 1.064 | 1.10 |
| 010yr-01hr | 2.02 | 30.66 | 1.458 | 1.50 |
| 010yr-02hr | 2.37 | 21.73 | 1.784 | 1.84 |
| 010yr-03hr | 2.53 | 16.36 | 1.934 | 1.99 |
| 010yr-06hr | 3.03 | 10.57 | 2.407 | 2.48 |
| 010yr-12hr | 3.52 | 5.60 | 2.873 | 2.96 |
| 010yr-24hr | 4.08 | 4.00 | 3.408 | 3.51 |
| 100 Yr-SCS 24Hr | 5.91 | 83.69 | 5.167 | 5.32 |
| 100yr-0.17hr | 1.25 | 45.74 | 0.761 | 0.78 |
| 100yr-0.25hr | 1.56 | 49.09 | 1.037 | 1.07 |
| 100yr-0.50hr | 2.25 | 55.52 | 1.672 | 1.72 |
| 100yr-01hr | 3.01 | 52.03 | 2.388 | 2.46 |
| 100yr-02hr | 2.65 | 25.14 | 2.047 | 2.11 |
| 100yr-03hr | 3.94 | 28.32 | 3.274 | 3.37 |
| 100yr-06hr | 4.78 | 18.15 | 4.079 | 4.20 |
| 100yr-12hr | 5.37 | 8.89 | 4.647 | 4.79 |
| 100yr-24hr | 5.91 | 5.93 | 5.167 | 5.32 |
| WQV-0.17hr | 1.25 | 45.74 | 0.761 | 0.78 |
| WQV-0.25hr | 1.25 | 36.16 | 0.761 | 0.78 |
| WQV-0.50hr | 1.25 | 23.22 | 0.761 | 0.78 |
| WQV-01hr | 1.25 | 15.18 | 0.761 | 0.78 |
| WQV-02hr | 1.25 | 8.63 | 0.761 | 0.78 |
| WQV-03hr | 1.25 | 5.95 | 0.761 | 0.78 |
| WQV-06hr | 1.25 | 3.05 | 0.761 | 0.78 |
| WQV-12hr | 1.25 | 1.54 | 0.761 | 0.78 |
| WQV-24hr | 1.25 | 1.03 | 0.761 | 0.78 |

Summary for Subcatchment 15S: Basin 2 (Middle)

Runoff = 83.69 cfs @ 12.01 hrs, Volume= 5.167 af, Depth= 5.32"
Routed to Pond 17P : EDDB Pond 2 (Middle)

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs
Type II 24-Hr 100 Yr-SCS 24Hr Rainfall=5.91"

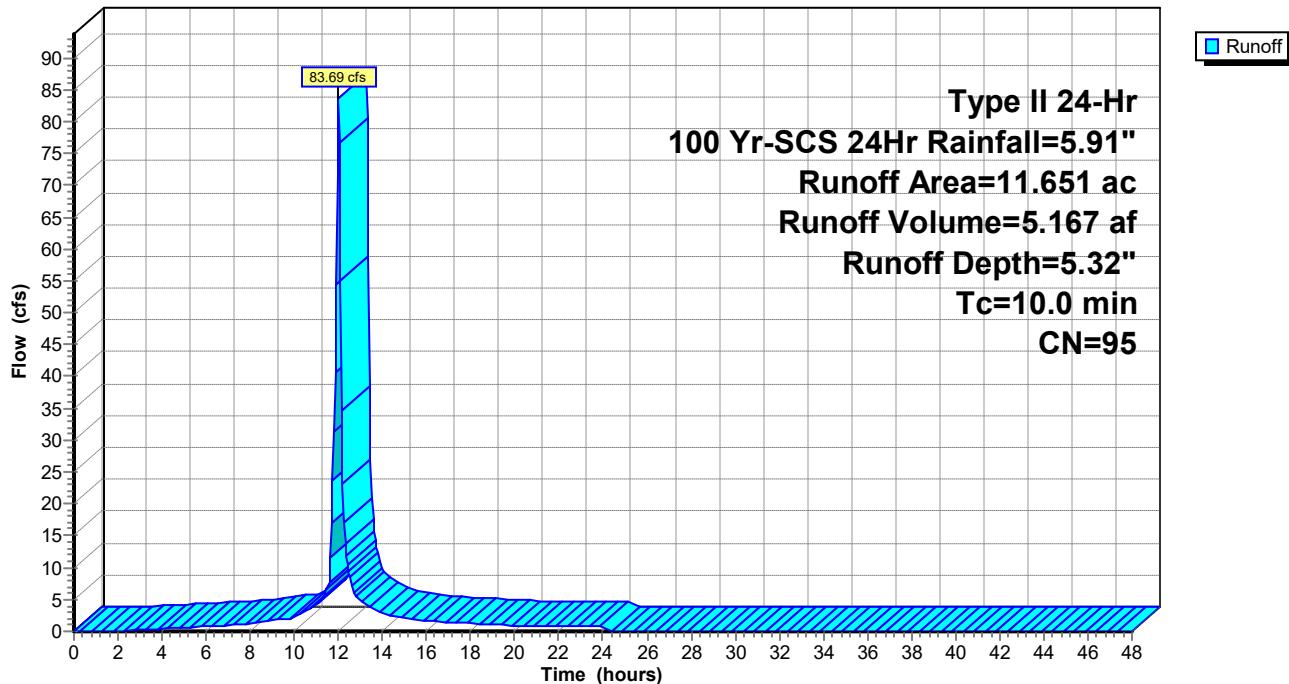
| Area (ac) | CN | Description |
|-----------|----|-------------|
|-----------|----|-------------|

| | | |
|---|--------|----|
| * | 11.651 | 95 |
|---|--------|----|

| | |
|--------|-----------------------|
| 11.651 | 100.00% Pervious Area |
|--------|-----------------------|

| Tc | Length | Slope | Velocity | Capacity | Description |
|-------|--------|---------|----------|----------|-------------|
| (min) | (feet) | (ft/ft) | (ft/sec) | (cfs) | |

| | |
|------|---------------|
| 10.0 | Direct Entry, |
|------|---------------|

Subcatchment 15S: Basin 2 (Middle)**Hydrograph**

Events for Subcatchment 16S: Basin 1 (South)

| Event | Rainfall (inches) | Runoff (cfs) | Volume (acre-feet) | Depth (inches) |
|-----------------|----------------------|-----------------|-----------------------|-------------------|
| 002yr-0.17hr | 0.69 | 74.01 | 1.218 | 0.31 |
| 002yr-0.25hr | 0.85 | 83.26 | 1.726 | 0.44 |
| 002yr-0.50hr | 1.13 | 80.68 | 2.678 | 0.68 |
| 002yr-01hr | 1.39 | 72.89 | 3.606 | 0.91 |
| 002yr-02hr | 1.62 | 52.13 | 4.447 | 1.12 |
| 002yr-03hr | 1.72 | 39.28 | 4.818 | 1.22 |
| 002yr-06hr | 2.05 | 25.83 | 6.055 | 1.53 |
| 002yr-12hr | 2.45 | 15.01 | 7.576 | 1.91 |
| 002yr-24hr | 2.92 | 11.30 | 9.382 | 2.37 |
| 10 Yr-SCS 24Hr | 4.10 | 231.59 | 13.965 | 3.53 |
| 010yr-0.17hr | 0.93 | 120.26 | 1.992 | 0.50 |
| 010yr-0.25hr | 1.14 | 129.20 | 2.714 | 0.69 |
| 010yr-0.50hr | 1.59 | 139.47 | 4.337 | 1.10 |
| 010yr-01hr | 2.02 | 124.93 | 5.942 | 1.50 |
| 010yr-02hr | 2.37 | 88.54 | 7.270 | 1.84 |
| 010yr-03hr | 2.53 | 66.65 | 7.882 | 1.99 |
| 010yr-06hr | 3.03 | 43.07 | 9.807 | 2.48 |
| 010yr-12hr | 3.52 | 22.81 | 11.706 | 2.96 |
| 010yr-24hr | 4.08 | 16.31 | 13.887 | 3.51 |
| 100 Yr-SCS 24Hr | 5.91 | 341.02 | 21.056 | 5.32 |
| 100yr-0.17hr | 1.25 | 186.38 | 3.103 | 0.78 |
| 100yr-0.25hr | 1.56 | 200.02 | 4.226 | 1.07 |
| 100yr-0.50hr | 2.25 | 226.25 | 6.813 | 1.72 |
| 100yr-01hr | 3.01 | 212.02 | 9.729 | 2.46 |
| 100yr-02hr | 2.65 | 102.43 | 8.342 | 2.11 |
| 100yr-03hr | 3.94 | 115.42 | 13.341 | 3.37 |
| 100yr-06hr | 4.78 | 73.96 | 16.623 | 4.20 |
| 100yr-12hr | 5.37 | 36.22 | 18.936 | 4.79 |
| 100yr-24hr | 5.91 | 24.15 | 21.056 | 5.32 |
| WQV-0.17hr | 1.25 | 186.38 | 3.103 | 0.78 |
| WQV-0.25hr | 1.25 | 147.35 | 3.103 | 0.78 |
| WQV-0.50hr | 1.25 | 94.60 | 3.103 | 0.78 |
| WQV-01hr | 1.25 | 61.87 | 3.103 | 0.78 |
| WQV-02hr | 1.25 | 35.18 | 3.103 | 0.78 |
| WQV-03hr | 1.25 | 24.24 | 3.103 | 0.78 |
| WQV-06hr | 1.25 | 12.41 | 3.103 | 0.78 |
| WQV-12hr | 1.25 | 6.27 | 3.103 | 0.78 |
| WQV-24hr | 1.25 | 4.19 | 3.103 | 0.78 |

Summary for Subcatchment 16S: Basin 1 (South)

Runoff = 341.02 cfs @ 12.01 hrs, Volume= 21.056 af, Depth= 5.32"
Routed to Pond 7P : Wet Pond 1 (South)

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs
Type II 24-Hr 100 Yr-SCS 24Hr Rainfall=5.91"

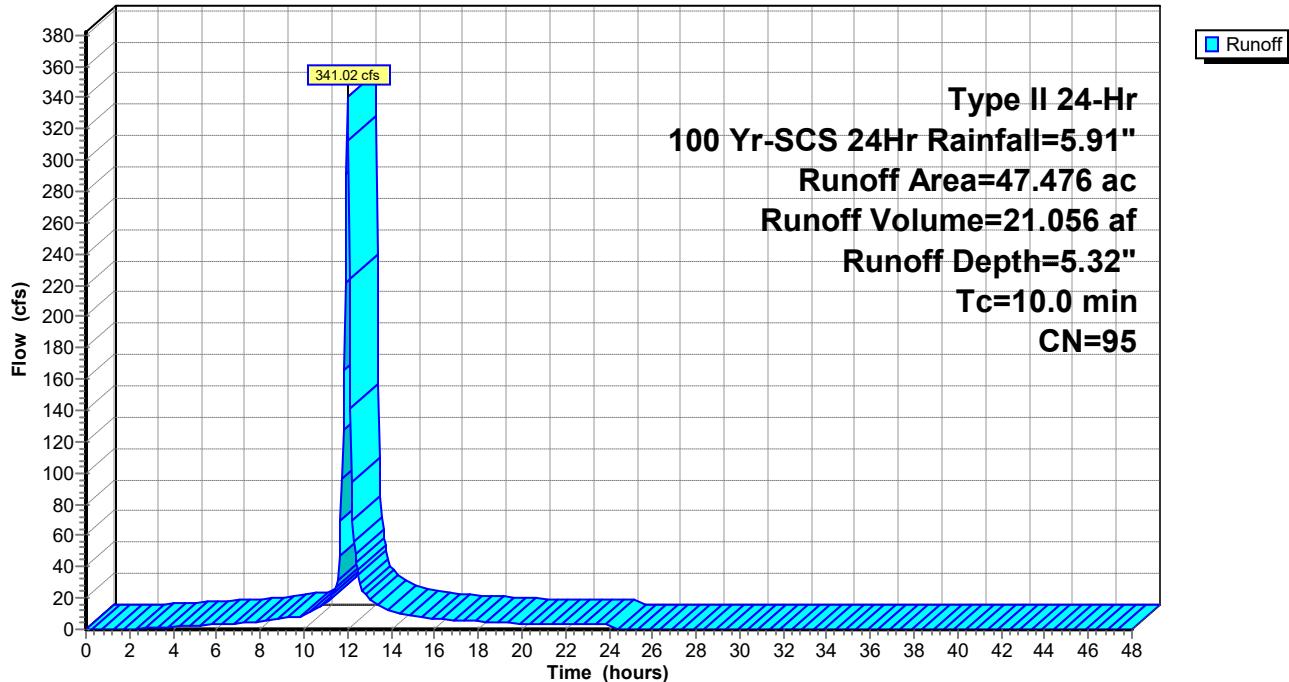
| Area (ac) | CN | Description |
|-----------|----|-------------|
|-----------|----|-------------|

| | | |
|---|--------|----|
| * | 47.476 | 95 |
|---|--------|----|

| | |
|--------|-----------------------|
| 47.476 | 100.00% Pervious Area |
|--------|-----------------------|

| Tc | Length | Slope | Velocity | Capacity | Description |
|-------|--------|---------|----------|----------|-------------|
| (min) | (feet) | (ft/ft) | (ft/sec) | (cfs) | |

| | |
|------|---------------|
| 10.0 | Direct Entry, |
|------|---------------|

Subcatchment 16S: Basin 1 (South)**Hydrograph**

Events for Subcatchment 18S: North Offsite

| Event | Rainfall (inches) | Runoff (cfs) | Volume (acre-feet) | Depth (inches) |
|-----------------|----------------------|-----------------|-----------------------|-------------------|
| 002yr-0.17hr | 0.69 | 0.00 | 0.000 | 0.00 |
| 002yr-0.25hr | 0.85 | 0.33 | 0.033 | 0.01 |
| 002yr-0.50hr | 1.13 | 2.58 | 0.261 | 0.05 |
| 002yr-01hr | 1.39 | 5.91 | 0.634 | 0.11 |
| 002yr-02hr | 1.62 | 8.02 | 1.071 | 0.19 |
| 002yr-03hr | 1.72 | 7.44 | 1.288 | 0.23 |
| 002yr-06hr | 2.05 | 6.24 | 2.105 | 0.37 |
| 002yr-12hr | 2.45 | 6.51 | 3.272 | 0.58 |
| 002yr-24hr | 2.92 | 7.59 | 4.836 | 0.86 |
| 10 Yr-SCS 24Hr | 4.10 | 46.18 | 9.415 | 1.67 |
| 010yr-0.17hr | 0.93 | 0.78 | 0.078 | 0.01 |
| 010yr-0.25hr | 1.14 | 2.70 | 0.273 | 0.05 |
| 010yr-0.50hr | 1.59 | 9.90 | 1.009 | 0.18 |
| 010yr-01hr | 2.02 | 18.22 | 2.025 | 0.36 |
| 010yr-02hr | 2.37 | 20.53 | 3.025 | 0.54 |
| 010yr-03hr | 2.53 | 17.73 | 3.525 | 0.63 |
| 010yr-06hr | 3.03 | 13.22 | 5.228 | 0.93 |
| 010yr-12hr | 3.52 | 14.20 | 7.068 | 1.25 |
| 010yr-24hr | 4.08 | 13.84 | 9.332 | 1.66 |
| 100 Yr-SCS 24Hr | 5.91 | 88.88 | 17.529 | 3.11 |
| 100yr-0.17hr | 1.25 | 4.16 | 0.416 | 0.07 |
| 100yr-0.25hr | 1.56 | 9.36 | 0.948 | 0.17 |
| 100yr-0.50hr | 2.25 | 25.85 | 2.667 | 0.47 |
| 100yr-01hr | 3.01 | 45.38 | 5.156 | 0.91 |
| 100yr-02hr | 2.65 | 25.95 | 3.915 | 0.69 |
| 100yr-03hr | 3.94 | 39.56 | 8.752 | 1.55 |
| 100yr-06hr | 4.78 | 33.95 | 12.346 | 2.19 |
| 100yr-12hr | 5.37 | 29.96 | 15.011 | 2.66 |
| 100yr-24hr | 5.91 | 24.52 | 17.529 | 3.11 |
| WQV-0.17hr | 1.25 | 4.16 | 0.416 | 0.07 |
| WQV-0.25hr | 1.25 | 4.11 | 0.416 | 0.07 |
| WQV-0.50hr | 1.25 | 4.11 | 0.416 | 0.07 |
| WQV-01hr | 1.25 | 3.92 | 0.416 | 0.07 |
| WQV-02hr | 1.25 | 3.43 | 0.416 | 0.07 |
| WQV-03hr | 1.25 | 2.83 | 0.416 | 0.07 |
| WQV-06hr | 1.25 | 1.74 | 0.416 | 0.07 |
| WQV-12hr | 1.25 | 0.95 | 0.416 | 0.07 |
| WQV-24hr | 1.25 | 0.76 | 0.416 | 0.07 |

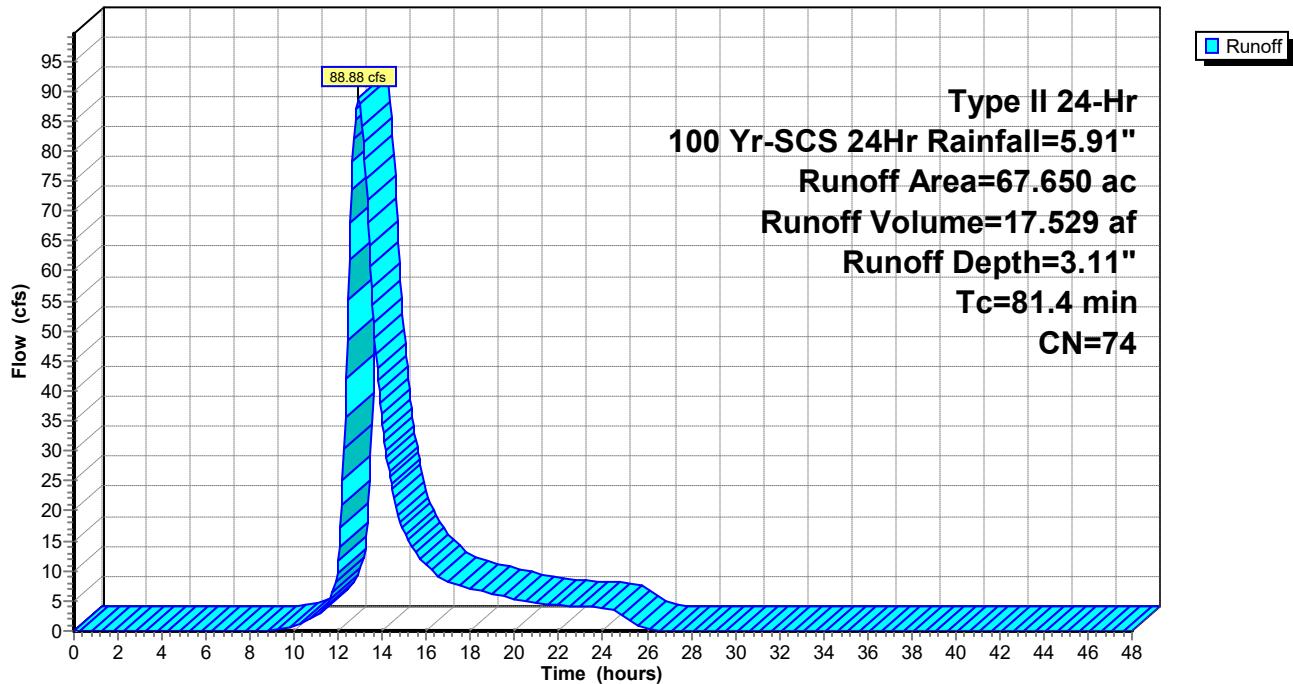
Summary for Subcatchment 18S: North Offsite

Runoff = 88.88 cfs @ 12.92 hrs, Volume= 17.529 af, Depth= 3.11"
Routed to Reach 14R : Off-Site Swale

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs
Type II 24-Hr 100 Yr-SCS 24Hr Rainfall=5.91"

| Area (ac) | CN | Description |
|-----------|----|---|
| * 66.930 | 74 | From Paul Hand Drainage Report (Structure 11) |
| 0.720 | 98 | From Paul Hand Drainage Report (Structure 11) |
| 67.650 | 74 | Weighted Average |
| 66.930 | | 98.94% Pervious Area |
| 0.720 | | 1.06% Impervious Area |

| Tc | Length | Slope | Velocity | Capacity | Description |
|-------|---|---------|----------|----------|-------------|
| (min) | (feet) | (ft/ft) | (ft/sec) | (cfs) | |
| 81.4 | Direct Entry, From Paul Hand Drainage Report (Structure 11) | | | | |

Subcatchment 18S: North Offsite**Hydrograph**

Time span=0.00-48.00 hrs, dt=0.05 hrs, 961 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

| | |
|--|---|
| Subcatchment 11S: Ex Site | Runoff Area=114.950 ac 0.00% Impervious Runoff Depth=3.11" Flow Length=5,240' Tc=141.1 min CN=74 Runoff=98.87 cfs 29.785 af |
| Subcatchment 13S: Basin 3 (North) | Runoff Area=74.111 ac 0.00% Impervious Runoff Depth=5.32" Tc=10.0 min CN=95 Runoff=532.34 cfs 32.869 af |
| Subcatchment 15S: Basin 2 (Middle) | Runoff Area=11.651 ac 0.00% Impervious Runoff Depth=5.32" Tc=10.0 min CN=95 Runoff=83.69 cfs 5.167 af |
| Subcatchment 16S: Basin 1 (South) | Runoff Area=47.476 ac 0.00% Impervious Runoff Depth=5.32" Tc=10.0 min CN=95 Runoff=341.02 cfs 21.056 af |
| Subcatchment 18S: North Offsite | Runoff Area=67.650 ac 1.06% Impervious Runoff Depth=3.11" Tc=81.4 min CN=74 Runoff=88.88 cfs 17.529 af |
| Reach 14R: Off-Site Swale | Avg. Flow Depth=1.67' Max Vel=4.96 fps Inflow=88.88 cfs 17.529 af n=0.022 L=1,260.0' S=0.0054 '/' Capacity=334.55 cfs Outflow=88.47 cfs 17.529 af |
| Pond 7P: Wet Pond 1 (South) | Peak Elev=776.01' Storage=1,965,830 cf Inflow=417.42 cfs 75.981 af Outflow=39.70 cfs 57.333 af |
| Pond 17P: EDDB Pond 2 (Middle) | Peak Elev=777.17' Storage=151,698 cf Inflow=180.22 cfs 55.005 af 42.0" Round Culvert x 2.00 n=0.013 L=810.0' S=0.0019 '/' Outflow=103.62 cfs 54.925 af |
| Pond 18P: Wet Pond 3 (North) | Peak Elev=779.29' Storage=16.646 af Inflow=541.61 cfs 50.398 af 36.0" Round Culvert x 2.00 n=0.013 L=211.0' S=0.0047 '/' Outflow=100.82 cfs 49.838 af |
| Total Runoff Area = 315.838 ac Runoff Volume = 106.407 af Average Runoff Depth = 4.04" 99.77% Pervious = 315.118 ac 0.23% Impervious = 0.720 ac | |

Events for Reach 14R: Off-Site Swale

| Event | Inflow (cfs) | Outflow (cfs) | Elevation (feet) | Storage (cubic-feet) |
|------------------------|-----------------|------------------|---------------------|-------------------------|
| 002yr-0.17hr | 0.00 | 0.00 | 783.07 | 0 |
| 002yr-0.25hr | 0.33 | 0.28 | 783.15 | 410 |
| 002yr-0.50hr | 2.58 | 2.46 | 783.34 | 1,719 |
| 002yr-01hr | 5.91 | 5.76 | 783.50 | 3,094 |
| 002yr-02hr | 8.02 | 7.92 | 783.58 | 3,877 |
| 002yr-03hr | 7.44 | 7.38 | 783.56 | 3,687 |
| 002yr-06hr | 6.24 | 6.23 | 783.52 | 3,273 |
| 002yr-12hr | 6.51 | 6.50 | 783.53 | 3,369 |
| 002yr-24hr | 7.59 | 7.58 | 783.57 | 3,756 |
| 10 Yr-SCS 24Hr | 46.18 | 45.80 | 784.30 | 13,810 |
| 010yr-0.17hr | 0.78 | 0.70 | 783.20 | 746 |
| 010yr-0.25hr | 2.70 | 2.57 | 783.35 | 1,772 |
| 010yr-0.50hr | 9.90 | 9.65 | 783.64 | 4,459 |
| 010yr-01hr | 18.22 | 17.96 | 783.85 | 6,968 |
| 010yr-02hr | 20.53 | 20.40 | 783.90 | 7,644 |
| 010yr-03hr | 17.73 | 17.68 | 783.84 | 6,890 |
| 010yr-06hr | 13.22 | 13.21 | 783.74 | 5,582 |
| 010yr-12hr | 14.20 | 14.18 | 783.76 | 5,876 |
| 010yr-24hr | 13.84 | 13.82 | 783.75 | 5,768 |
| 100 Yr-SCS 24Hr | 88.88 | 88.47 | 784.74 | 22,462 |
| 100yr-0.17hr | 4.16 | 4.03 | 783.42 | 2,411 |
| 100yr-0.25hr | 9.36 | 9.13 | 783.62 | 4,286 |
| 100yr-0.50hr | 25.85 | 25.50 | 784.00 | 8,991 |
| 100yr-01hr | 45.38 | 45.05 | 784.29 | 13,643 |
| 100yr-02hr | 25.95 | 25.85 | 784.00 | 9,081 |
| 100yr-03hr | 39.56 | 39.54 | 784.22 | 12,394 |
| 100yr-06hr | 33.95 | 33.86 | 784.13 | 11,061 |
| 100yr-12hr | 29.96 | 29.92 | 784.07 | 10,105 |
| 100yr-24hr | 24.52 | 24.50 | 783.98 | 8,733 |
| WQV-0.17hr | 4.16 | 4.03 | 783.42 | 2,411 |
| WQV-0.25hr | 4.11 | 3.95 | 783.42 | 2,380 |
| WQV-0.50hr | 4.11 | 3.95 | 783.42 | 2,380 |
| WQV-01hr | 3.92 | 3.80 | 783.41 | 2,314 |
| WQV-02hr | 3.43 | 3.33 | 783.39 | 2,116 |
| WQV-03hr | 2.83 | 2.79 | 783.36 | 1,871 |
| WQV-06hr | 1.74 | 1.73 | 783.29 | 1,353 |
| WQV-12hr | 0.95 | 0.94 | 783.23 | 906 |
| WQV-24hr | 0.76 | 0.75 | 783.21 | 781 |

Summary for Reach 14R: Off-Site Swale

Inflow Area = 67.650 ac, 1.06% Impervious, Inflow Depth = 3.11" for 100 Yr-SCS 24Hr event

Inflow = 88.88 cfs @ 12.92 hrs, Volume= 17.529 af

Outflow = 88.47 cfs @ 12.96 hrs, Volume= 17.529 af, Atten= 0%, Lag= 2.7 min

Routed to Pond 18P : Wet Pond 3 (North)

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

Max. Velocity= 4.96 fps, Min. Travel Time= 4.2 min

Avg. Velocity = 1.85 fps, Avg. Travel Time= 11.3 min

Peak Storage= 22,462 cf @ 12.96 hrs

Average Depth at Peak Storage= 1.67' , Surface Width= 17.36'

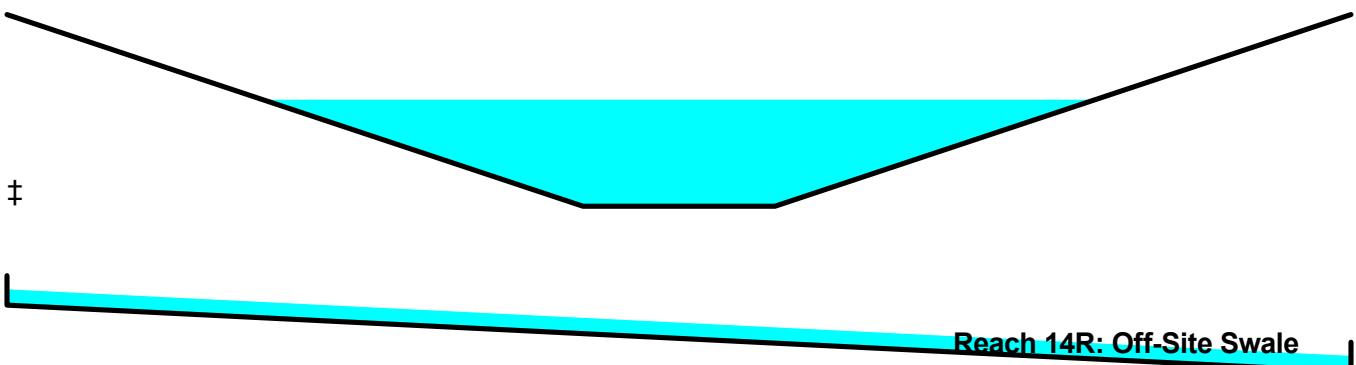
Bank-Full Depth= 3.00' Flow Area= 48.0 sf, Capacity= 334.55 cfs

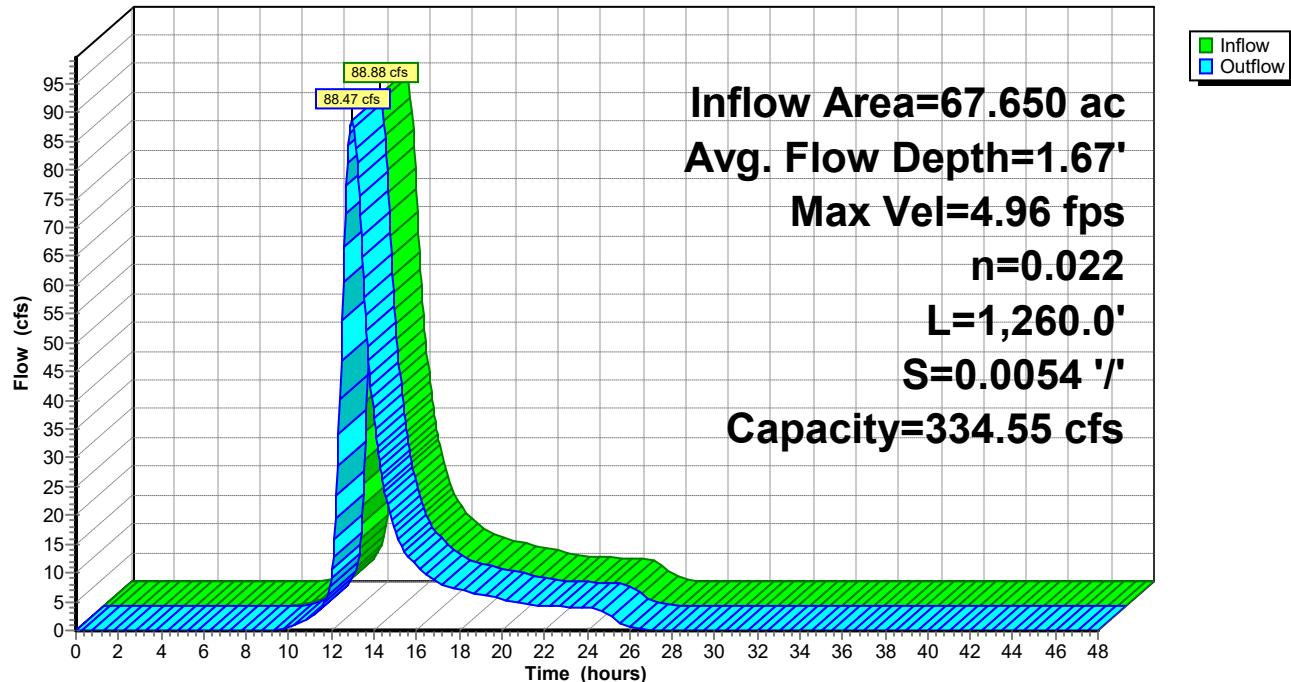
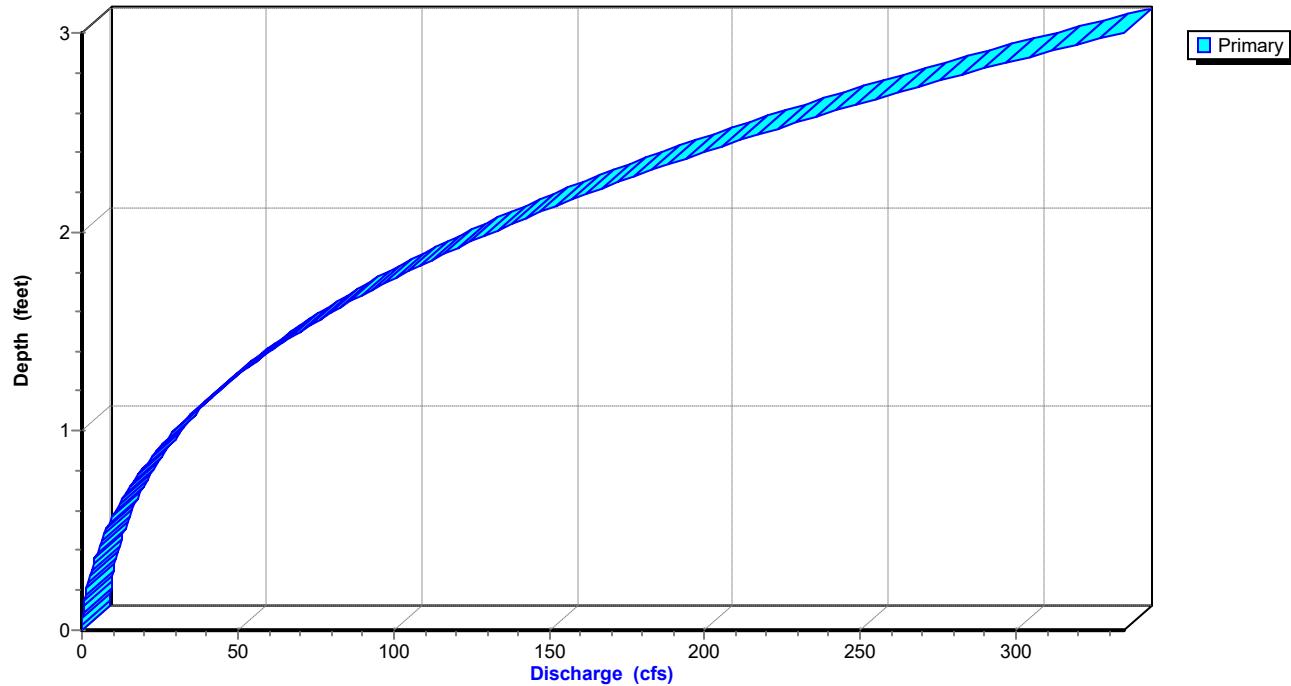
4.00' x 3.00' deep channel, n= 0.022 Earth, clean & straight

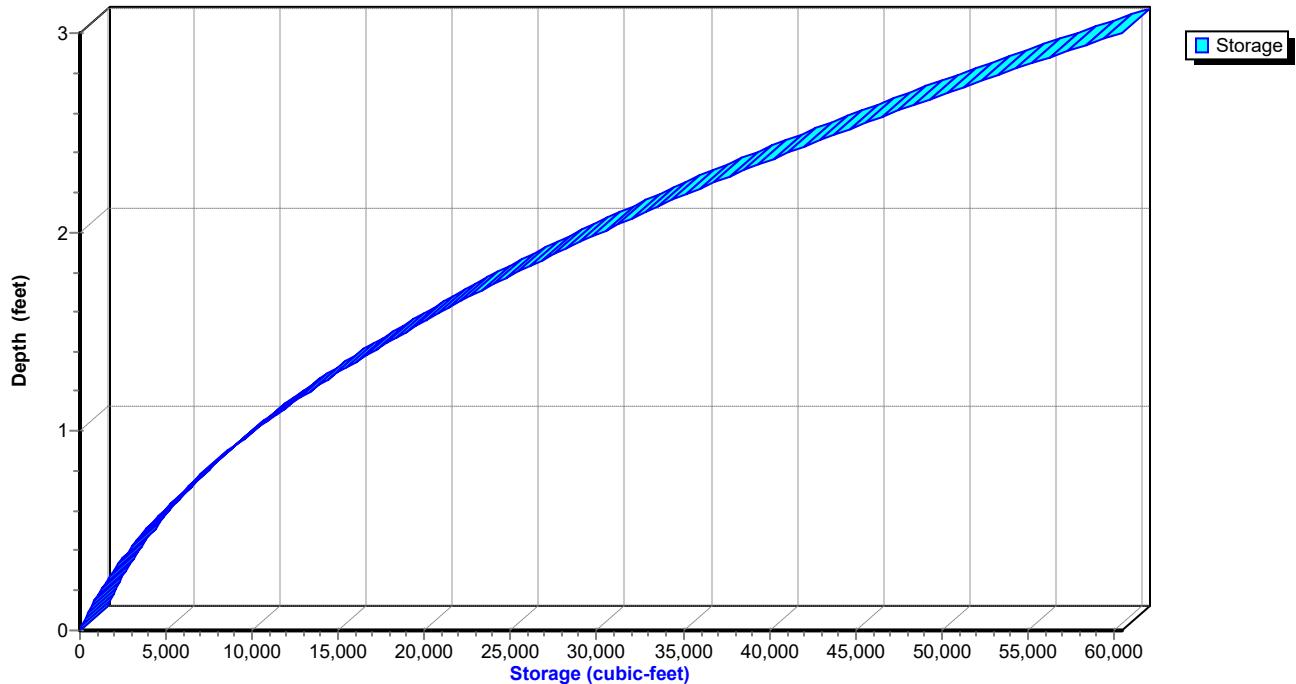
Side Slope Z-value= 4.0 '/' Top Width= 28.00'

Length= 1,260.0' Slope= 0.0054 '/'

Inlet Invert= 783.07', Outlet Invert= 776.30'



Reach 14R: Off-Site Swale**Hydrograph****Reach 14R: Off-Site Swale****Stage-Discharge**

Reach 14R: Off-Site Swale**Stage-Storage**

Events for Pond 7P: Wet Pond 1 (South)

| Event | Inflow (cfs) | Primary (cfs) | Elevation (feet) | Storage (cubic-feet) |
|------------------------|-----------------|------------------|---------------------|-------------------------|
| 002yr-0.17hr | 77.32 | 0.39 | 771.78 | 113,442 |
| 002yr-0.25hr | 88.92 | 0.77 | 771.90 | 162,148 |
| 002yr-0.50hr | 85.69 | 1.82 | 772.13 | 258,010 |
| 002yr-01hr | 78.60 | 3.18 | 772.36 | 355,305 |
| 002yr-02hr | 58.33 | 4.55 | 772.58 | 445,939 |
| 002yr-03hr | 45.55 | 5.15 | 772.67 | 485,631 |
| 002yr-06hr | 34.06 | 6.69 | 772.98 | 617,559 |
| 002yr-12hr | 34.96 | 8.05 | 773.33 | 767,301 |
| 002yr-24hr | 34.14 | 9.34 | 773.72 | 936,131 |
| 10 Yr-SCS 24Hr | 279.86 | 16.14 | 774.77 | 1,398,944 |
| 010yr-0.17hr | 126.46 | 1.03 | 771.96 | 188,366 |
| 010yr-0.25hr | 138.07 | 1.87 | 772.14 | 261,651 |
| 010yr-0.50hr | 144.04 | 4.38 | 772.55 | 434,769 |
| 010yr-01hr | 135.22 | 6.70 | 772.99 | 619,134 |
| 010yr-02hr | 99.99 | 8.17 | 773.37 | 781,431 |
| 010yr-03hr | 78.72 | 8.75 | 773.54 | 854,958 |
| 010yr-06hr | 61.73 | 10.28 | 774.04 | 1,076,628 |
| 010yr-12hr | 58.84 | 12.40 | 774.46 | 1,259,880 |
| 010yr-24hr | 51.78 | 16.66 | 774.81 | 1,415,398 |
| 100 Yr-SCS 24Hr | 417.42 | 39.70 | 776.01 | 1,965,830 |
| 100yr-0.17hr | 196.32 | 2.41 | 772.24 | 302,247 |
| 100yr-0.25hr | 213.64 | 4.20 | 772.52 | 422,738 |
| 100yr-0.50hr | 239.91 | 7.71 | 773.24 | 726,810 |
| 100yr-01hr | 229.29 | 10.44 | 774.10 | 1,101,195 |
| 100yr-02hr | 116.08 | 9.21 | 773.68 | 917,961 |
| 100yr-03hr | 142.19 | 19.87 | 775.01 | 1,510,052 |
| 100yr-06hr | 115.13 | 31.45 | 775.63 | 1,792,643 |
| 100yr-12hr | 101.53 | 36.48 | 775.87 | 1,900,220 |
| 100yr-24hr | 78.02 | 37.62 | 775.92 | 1,923,656 |
| WQV-0.17hr | 196.32 | 2.41 | 772.24 | 302,247 |
| WQV-0.25hr | 157.47 | 2.41 | 772.24 | 302,183 |
| WQV-0.50hr | 100.39 | 2.41 | 772.23 | 302,144 |
| WQV-01hr | 66.63 | 2.41 | 772.23 | 302,028 |
| WQV-02hr | 39.18 | 2.40 | 772.23 | 301,717 |
| WQV-03hr | 27.85 | 2.40 | 772.23 | 301,259 |
| WQV-06hr | 15.45 | 2.37 | 772.23 | 299,122 |
| WQV-12hr | 11.85 | 2.31 | 772.22 | 294,684 |
| WQV-24hr | 9.71 | 2.24 | 772.21 | 289,690 |

PEAK INFLOW FOR
EMERGENCY
SPILLWAY
CALCULATIONS
 $417.42 \times 1.25 = 522$

PEAK ELEVATION
WITH OFFSITE

Summary for Pond 7P: Wet Pond 1 (South)

Inflow Area = 200.888 ac, 0.36% Impervious, Inflow Depth > 4.54" for 100 Yr-SCS 24Hr event

Inflow = 417.42 cfs @ 12.01 hrs, Volume= 75.981 af

Outflow = 39.70 cfs @ 17.13 hrs, Volume= 57.333 af, Atten= 90%, Lag= 306.9 min

Primary = 39.70 cfs @ 17.13 hrs, Volume= 57.333 af

Routed to nonexistent node 20L

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

Peak Elev= 776.01' @ 17.13 hrs Surf.Area= 466,239 sf Storage= 1,965,830 cf

PEAK ELEVATION
WITH OFFSITE

Plug-Flow detention time= 741.8 min calculated for 57.274 af (75% of inflow)

Center-of-Mass det. time= 585.9 min (1,529.2 - 943.4)

| Volume | Invert | Avail.Storage | Storage Description |
|--------|---------|---------------|--|
| #1 | 771.50' | 2,921,766 cf | Custom Stage Data (Prismatic) Listed below (Recalc) |

| Elevation (feet) | Surf.Area (sq-ft) | Inc.Store (cubic-feet) | Cum.Store (cubic-feet) |
|---------------------|----------------------|---------------------------|---------------------------|
| 771.50 | 406,211 | 0 | 0 |
| 778.00 | 492,794 | 2,921,766 | 2,921,766 |

| Device | Routing | Invert | Outlet Devices |
|--------|---------|---------|--|
| #1 | Primary | 771.50' | 17.0" Vert. Orifice/Grate C= 0.600 Limited to weir flow at low heads |
| #2 | Primary | 774.25' | 40.0" W x 24.0" H Vert. Orifice/Grate C= 0.600 Limited to weir flow at low heads |

Primary OutFlow Max=39.70 cfs @ 17.13 hrs HW=776.01' (Free Discharge)

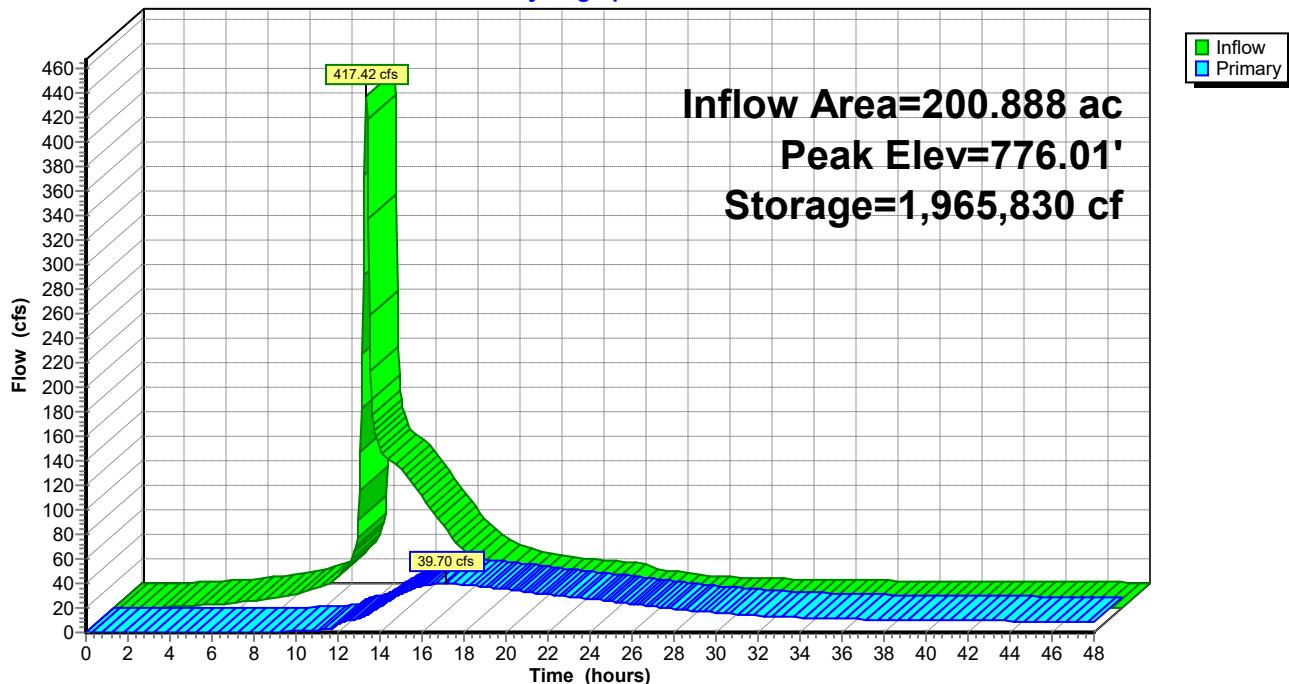
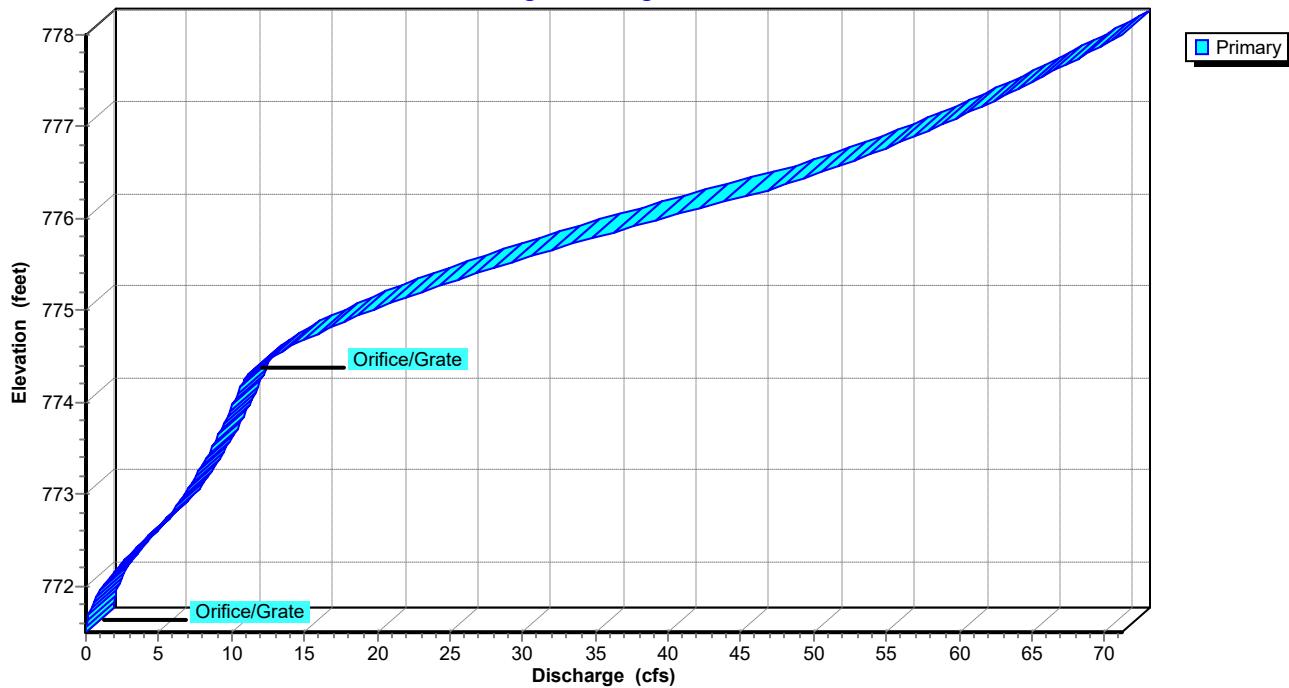
1=Orifice/Grate (Orifice Controls 14.79 cfs @ 9.38 fps)

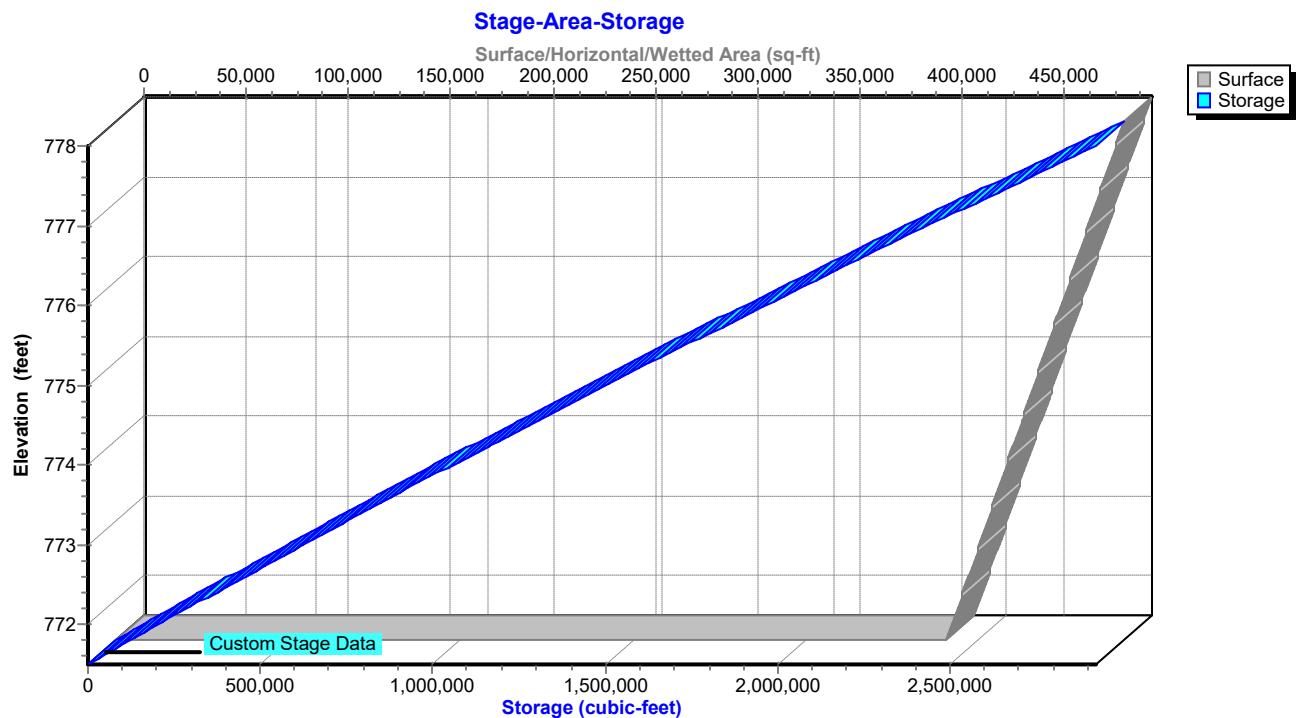
2=Orifice/Grate (Orifice Controls 24.91 cfs @ 4.25 fps)

Pond 7P: Wet Pond 1 (South)

Orifice/Grate

Orifice/Grate

Pond 7P: Wet Pond 1 (South)**Hydrograph****Pond 7P: Wet Pond 1 (South)****Stage-Discharge**

Pond 7P: Wet Pond 1 (South)

Events for Pond 17P: EDDB Pond 2 (Middle)

| Event | Inflow (cfs) | Primary (cfs) | Elevation (feet) | Storage (cubic-feet) |
|------------------------|-----------------|------------------|---------------------|-------------------------|
| 002yr-0.17hr | 19.26 | 7.23 | 773.90 | 9,785 |
| 002yr-0.25hr | 23.47 | 10.89 | 774.10 | 14,647 |
| 002yr-0.50hr | 28.78 | 18.72 | 774.45 | 25,018 |
| 002yr-01hr | 32.44 | 26.06 | 774.72 | 34,169 |
| 002yr-02hr | 30.77 | 28.63 | 774.81 | 37,297 |
| 002yr-03hr | 27.54 | 26.75 | 774.74 | 35,009 |
| 002yr-06hr | 22.94 | 22.76 | 774.60 | 30,104 |
| 002yr-12hr | 23.77 | 23.48 | 774.63 | 31,004 |
| 002yr-24hr | 24.28 | 23.72 | 774.70 | 33,573 |
| 10 Yr-SCS 24Hr | 125.19 | 78.36 | 776.26 | 100,911 |
| 010yr-0.17hr | 32.64 | 13.25 | 774.22 | 17,810 |
| 010yr-0.25hr | 39.55 | 19.81 | 774.49 | 26,415 |
| 010yr-0.50hr | 54.48 | 36.51 | 775.06 | 46,783 |
| 010yr-01hr | 59.72 | 49.93 | 775.46 | 63,034 |
| 010yr-02hr | 56.35 | 53.10 | 775.55 | 66,959 |
| 010yr-03hr | 50.62 | 49.65 | 775.45 | 62,693 |
| 010yr-06hr | 40.99 | 40.57 | 775.26 | 54,547 |
| 010yr-12hr | 41.68 | 41.22 | 775.21 | 52,445 |
| 010yr-24hr | 37.83 | 36.50 | 775.32 | 57,010 |
| 100 Yr-SCS 24Hr | 180.22 | 103.62 | 777.17 | 151,698 |
| 100yr-0.17hr | 54.05 | 24.07 | 774.65 | 31,733 |
| 100yr-0.25hr | 68.55 | 36.48 | 775.06 | 46,750 |
| 100yr-0.50hr | 94.69 | 64.11 | 775.86 | 81,025 |
| 100yr-01hr | 99.91 | 84.77 | 776.45 | 110,867 |
| 100yr-02hr | 66.26 | 62.45 | 775.81 | 78,854 |
| 100yr-03hr | 90.79 | 88.63 | 776.57 | 117,322 |
| 100yr-06hr | 77.61 | 75.67 | 776.56 | 116,601 |
| 100yr-12hr | 74.05 | 70.78 | 776.33 | 104,481 |
| 100yr-24hr | 58.43 | 55.02 | 776.39 | 107,666 |
| WQV-0.17hr | 54.05 | 24.07 | 774.65 | 31,733 |
| WQV-0.25hr | 46.55 | 23.87 | 774.64 | 31,479 |
| WQV-0.50hr | 35.05 | 23.02 | 774.61 | 30,424 |
| WQV-01hr | 26.69 | 21.16 | 774.54 | 28,104 |
| WQV-02hr | 19.52 | 17.76 | 774.41 | 23,784 |
| WQV-03hr | 15.75 | 15.07 | 774.30 | 20,257 |
| WQV-06hr | 10.03 | 9.97 | 774.05 | 13,410 |
| WQV-12hr | 7.08 | 6.97 | 773.88 | 9,441 |
| WQV-24hr | 6.17 | 6.13 | 773.83 | 8,331 |

**PEAK ELEVATION
WITH OFFSITE**

Summary for Pond 17P: EDDB Pond 2 (Middle)

Inflow Area = 153.412 ac, 0.47% Impervious, Inflow Depth > 4.30" for 100 Yr-SCS 24Hr event

Inflow = 180.22 cfs @ 12.02 hrs, Volume= 55.005 af

Outflow = 103.62 cfs @ 13.36 hrs, Volume= 54.925 af, Atten= 43%, Lag= 80.7 min

Primary = 103.62 cfs @ 13.36 hrs, Volume= 54.925 af

Routed to Pond 7P : Wet Pond 1 (South)

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

Peak Elev= 777.17' @ 13.90 hrs Surf.Area= 60,876 sf Storage= 151,698 cf

**PEAK ELEVATION
WITH OFFSITE**

Plug-Flow detention time= 49.2 min calculated for 54.868 af (100% of inflow)

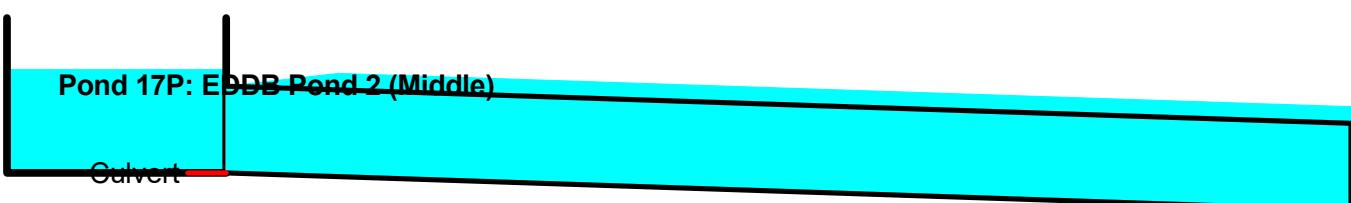
Center-of-Mass det. time= 46.6 min (1,012.1 - 965.5)

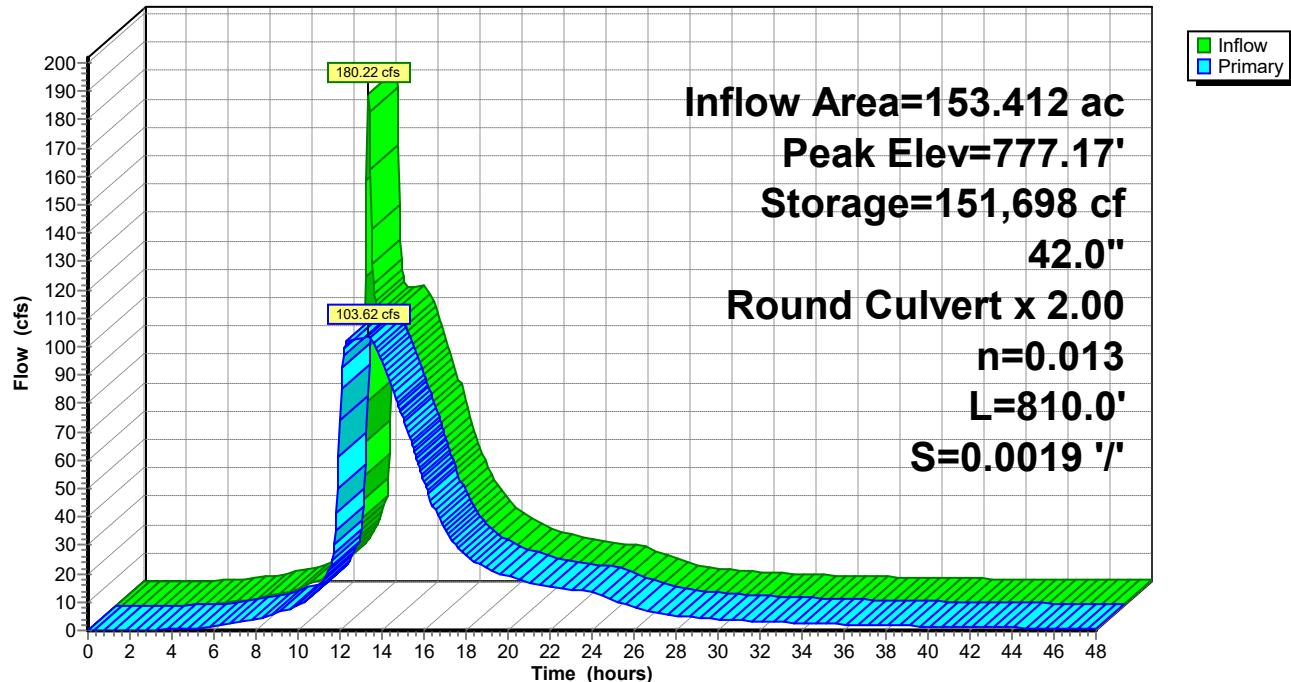
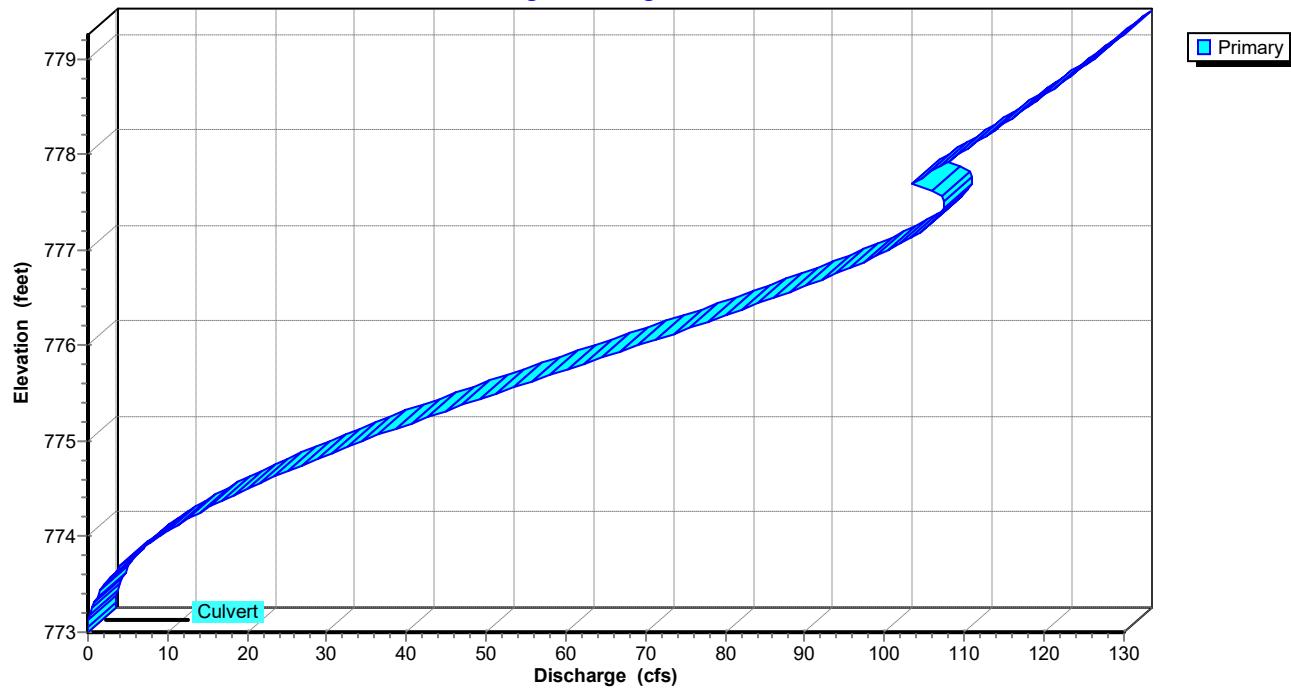
| Volume | Invert | Avail.Storage | Storage Description |
|--------|---------|---------------|--|
| #1 | 773.00' | 296,520 cf | Custom Stage Data (Prismatic) Listed below (Recalc) |

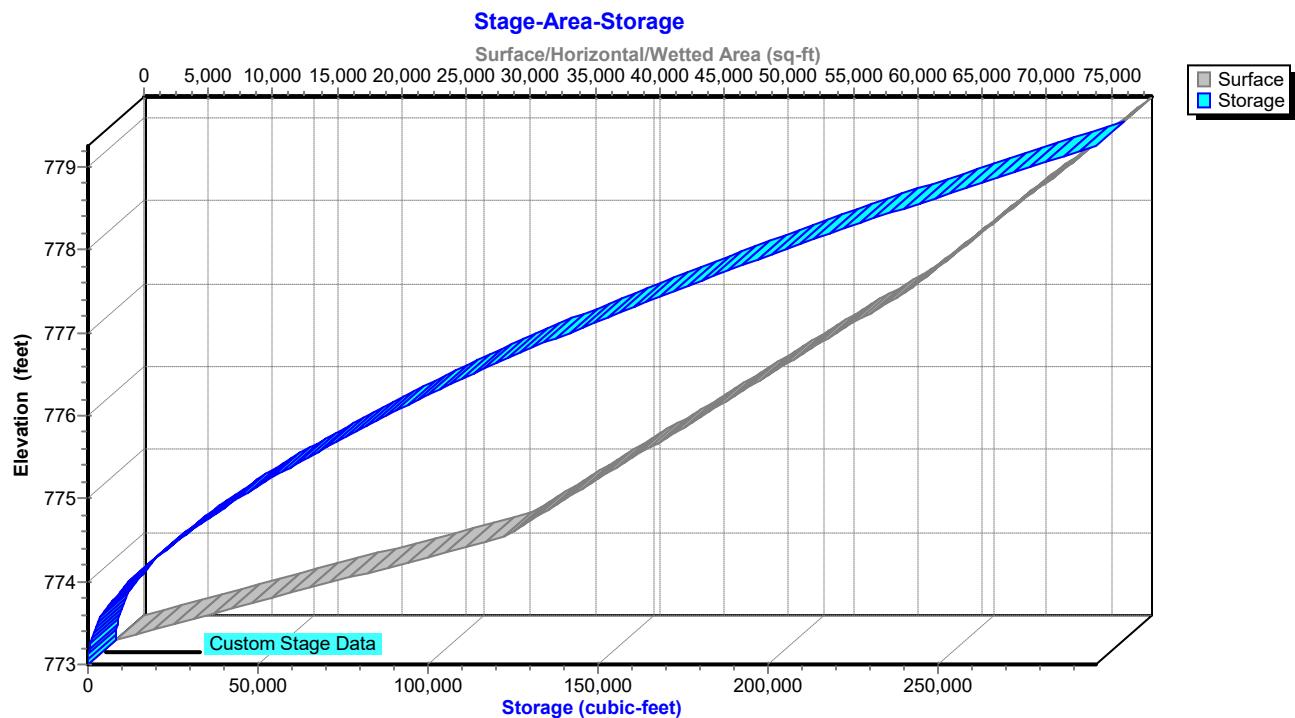
| Elevation (feet) | Surf.Area (sq-ft) | Inc.Store (cubic-feet) | Cum.Store (cubic-feet) |
|---------------------|----------------------|---------------------------|---------------------------|
| 773.00 | 0 | 0 | 0 |
| 774.25 | 30,144 | 18,840 | 18,840 |
| 777.25 | 61,725 | 137,804 | 156,644 |
| 779.25 | 78,151 | 139,876 | 296,520 |

| Device | Routing | Invert | Outlet Devices |
|--------|---------|---------|--|
| #1 | Primary | 773.00' | 42.0" Round Culvert X 2.00 L= 810.0' RCP, groove end projecting, Ke= 0.200 Inlet / Outlet Invert= 773.00' / 771.50' S= 0.0019 '/' Cc= 0.900 n= 0.013, Flow Area= 9.62 sf |

Primary OutFlow Max=103.31 cfs @ 13.36 hrs HW=777.14' TW=774.62' (Dynamic Tailwater)
 ↑=Culvert (Outlet Controls 103.31 cfs @ 5.72 fps)



Pond 17P: EDDB Pond 2 (Middle)**Hydrograph****Pond 17P: EDDB Pond 2 (Middle)****Stage-Discharge**

Pond 17P: EDDB Pond 2 (Middle)

Events for Pond 18P: Wet Pond 3 (North)

| Event | Inflow (cfs) | Primary (cfs) | Elevation (feet) | Storage (acre-feet) |
|------------------------|-----------------|------------------|---------------------|------------------------|
| 002yr-0.17hr | 115.53 | 4.60 | 774.68 | 1.793 |
| 002yr-0.25hr | 129.97 | 8.64 | 774.94 | 2.493 |
| 002yr-0.50hr | 125.94 | 17.90 | 775.36 | 3.689 |
| 002yr-01hr | 113.79 | 24.83 | 775.65 | 4.515 |
| 002yr-02hr | 81.37 | 26.21 | 775.72 | 4.739 |
| 002yr-03hr | 61.32 | 24.30 | 775.65 | 4.531 |
| 002yr-06hr | 40.32 | 20.53 | 775.50 | 4.084 |
| 002yr-12hr | 25.95 | 21.23 | 775.53 | 4.168 |
| 002yr-24hr | 24.28 | 21.85 | 775.57 | 4.278 |
| 10 Yr-SCS 24Hr | 364.26 | 80.48 | 777.45 | 10.148 |
| 010yr-0.17hr | 187.73 | 11.16 | 775.07 | 2.863 |
| 010yr-0.25hr | 201.69 | 18.97 | 775.40 | 3.811 |
| 010yr-0.50hr | 217.72 | 37.09 | 776.05 | 5.711 |
| 010yr-01hr | 195.02 | 47.58 | 776.47 | 6.983 |
| 010yr-02hr | 138.21 | 49.41 | 776.56 | 7.286 |
| 010yr-03hr | 104.05 | 45.63 | 776.44 | 6.910 |
| 010yr-06hr | 67.23 | 36.82 | 776.14 | 5.997 |
| 010yr-12hr | 44.02 | 37.66 | 776.16 | 6.046 |
| 010yr-24hr | 37.96 | 34.22 | 776.11 | 5.888 |
| 100 Yr-SCS 24Hr | 541.61 | 100.82 | 779.29 | 16.646 |
| 100yr-0.17hr | 290.95 | 23.74 | 775.58 | 4.334 |
| 100yr-0.25hr | 312.24 | 38.10 | 776.06 | 5.745 |
| 100yr-0.50hr | 353.19 | 66.50 | 776.98 | 8.626 |
| 100yr-01hr | 330.97 | 80.40 | 777.71 | 11.022 |
| 100yr-02hr | 159.90 | 58.44 | 776.88 | 8.278 |
| 100yr-03hr | 180.19 | 82.04 | 777.92 | 11.740 |
| 100yr-06hr | 115.75 | 70.29 | 777.38 | 9.912 |
| 100yr-12hr | 78.03 | 67.05 | 777.25 | 9.478 |
| 100yr-24hr | 60.38 | 52.90 | 777.03 | 8.787 |
| WQV-0.17hr | 290.95 | 23.74 | 775.58 | 4.334 |
| WQV-0.25hr | 230.03 | 23.62 | 775.58 | 4.315 |
| WQV-0.50hr | 147.68 | 22.64 | 775.54 | 4.216 |
| WQV-01hr | 96.58 | 20.09 | 775.46 | 3.964 |
| WQV-02hr | 54.92 | 16.15 | 775.30 | 3.514 |
| WQV-03hr | 37.85 | 13.53 | 775.18 | 3.173 |
| WQV-06hr | 19.37 | 8.84 | 774.93 | 2.487 |
| WQV-12hr | 9.79 | 6.08 | 774.76 | 2.022 |
| WQV-24hr | 6.66 | 5.38 | 774.72 | 1.891 |

**PEAK ELEVATION
WITH OFFSITE**

Summary for Pond 18P: Wet Pond 3 (North)

[62] Hint: Exceeded Reach 14R OUTLET depth by 1.77' @ 12.20 hrs

Inflow Area = 141.761 ac, 0.51% Impervious, Inflow Depth = 4.27" for 100 Yr-SCS 24Hr event
 Inflow = 541.61 cfs @ 12.01 hrs, Volume= 50.398 af
 Outflow = 100.82 cfs @ 13.24 hrs, Volume= 49.838 af, Atten= 81%, Lag= 73.9 min
 Primary = 100.82 cfs @ 13.24 hrs, Volume= 49.838 af
 Routed to Pond 17P : EDDB Pond 2 (Middle)

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs
 Peak Elev= 779.29' @ 13.29 hrs Surf.Area= 3.734 ac Storage= 16.646 af

**PEAK ELEVATION
WITH OFFSITE**

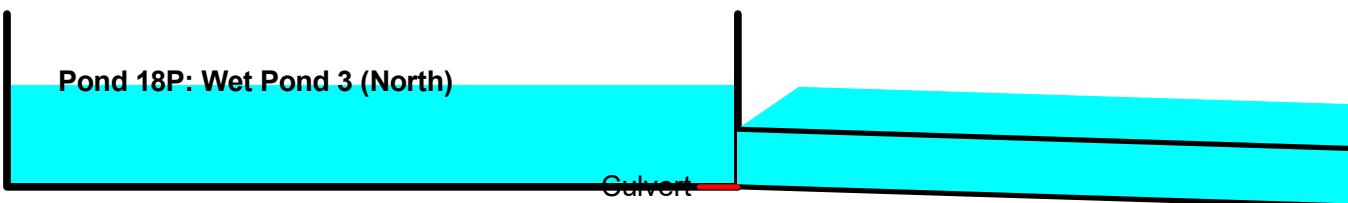
Plug-Flow detention time= 181.8 min calculated for 49.838 af (99% of inflow)
 Center-of-Mass det. time= 174.3 min (986.4 - 812.1)

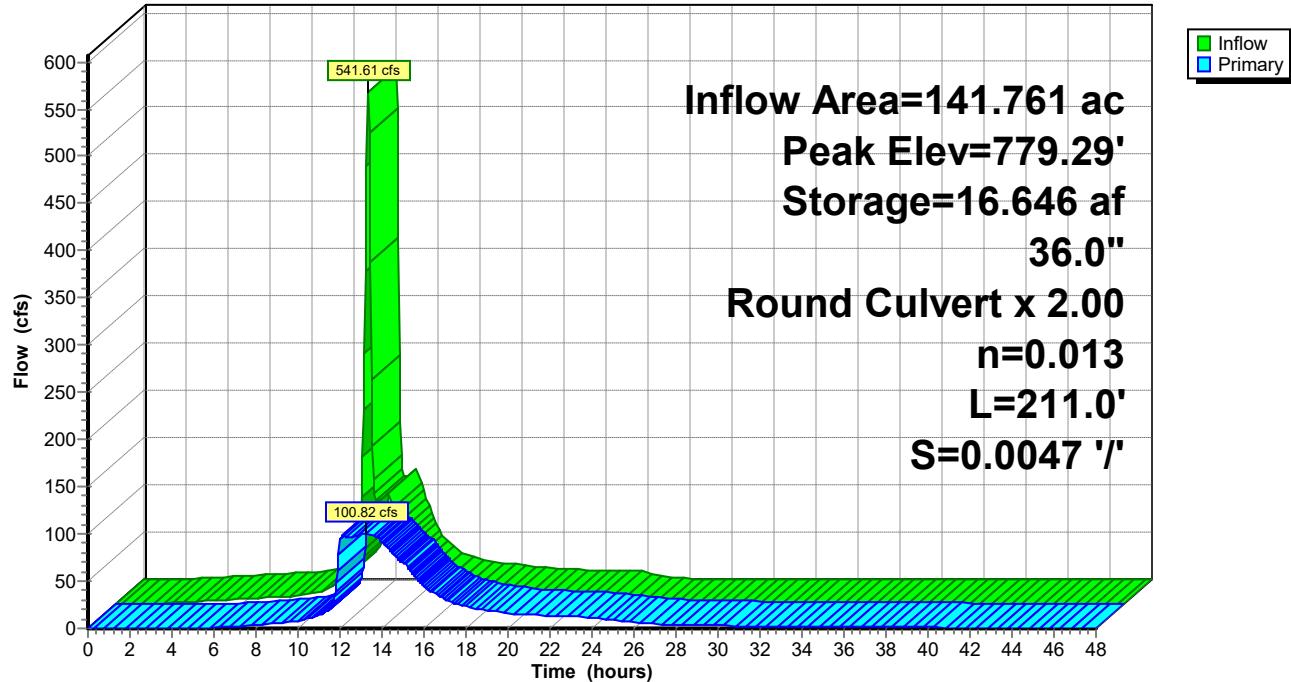
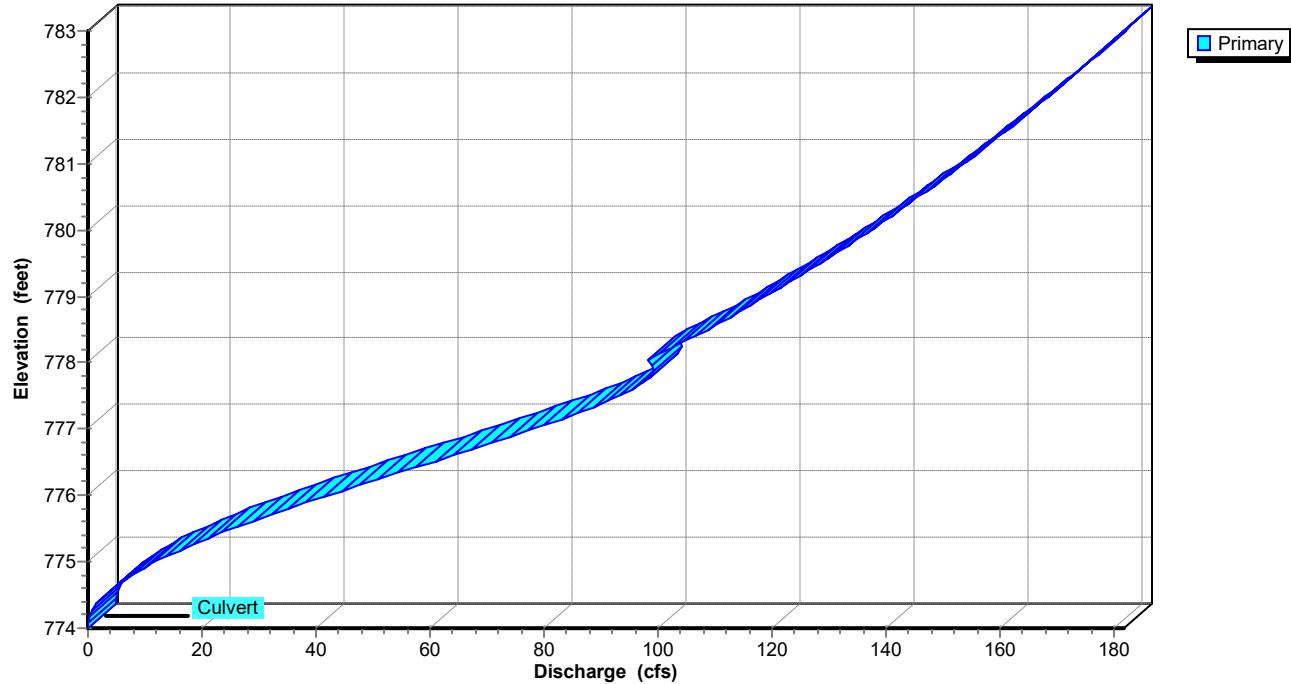
| Volume | Invert | Avail.Storage | Storage Description |
|--------|---------|---------------|--|
| #1 | 774.00' | 32.027 af | Custom Stage Data (Prismatic) Listed below (Recalc) |

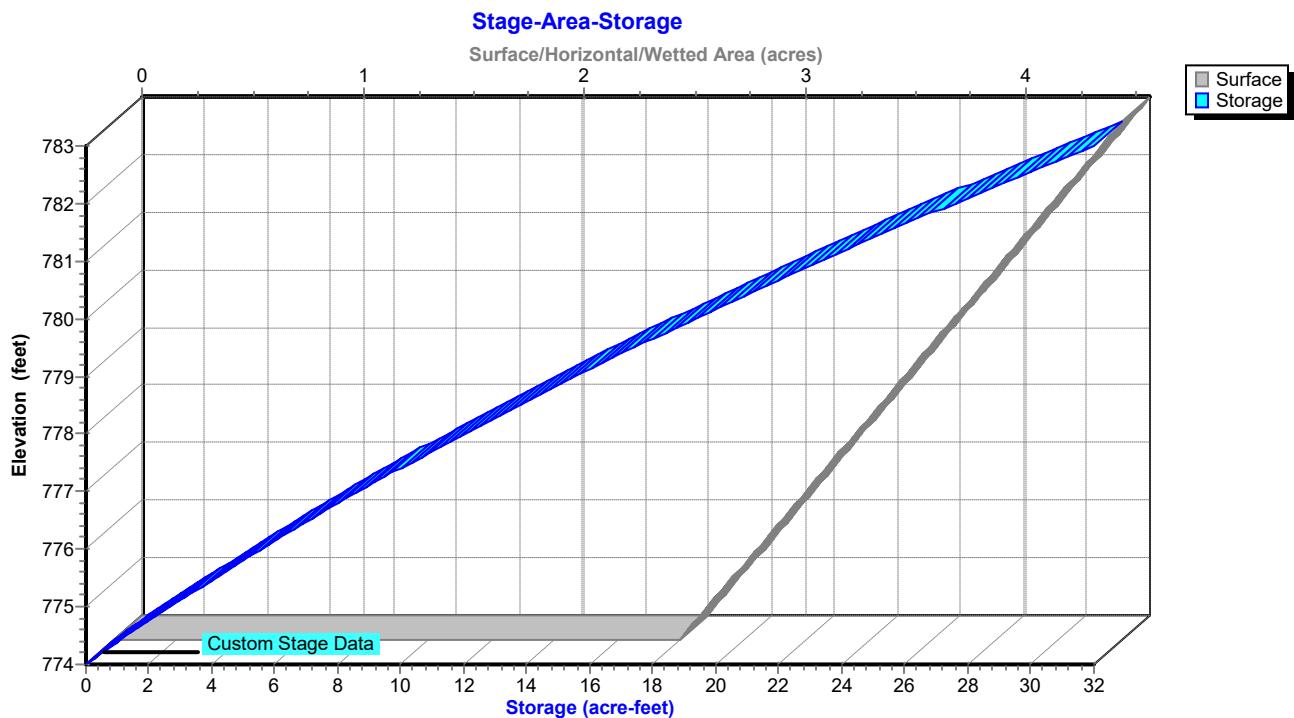
| Elevation (feet) | Surf.Area (acres) | Inc.Store (acre-feet) | Cum.Store (acre-feet) |
|---------------------|----------------------|--------------------------|--------------------------|
| 774.00 | 2.558 | 0.000 | 0.000 |
| 783.00 | 4.559 | 32.027 | 32.027 |

| Device | Routing | Invert | Outlet Devices |
|--------|---------|---------|--|
| #1 | Primary | 774.00' | 36.0" Round Culvert X 2.00 L= 211.0' RCP, groove end projecting, Ke= 0.200 Inlet / Outlet Invert= 774.00' / 773.00' S= 0.0047 '/' Cc= 0.900 n= 0.013, Flow Area= 7.07 sf |

Primary OutFlow Max=100.71 cfs @ 13.24 hrs HW=779.29' TW=777.14' (Dynamic Tailwater)
 ↑=Culvert (Outlet Controls 100.71 cfs @ 7.12 fps)



Pond 18P: Wet Pond 3 (North)**Hydrograph****Pond 18P: Wet Pond 3 (North)****Stage-Discharge**

Pond 18P: Wet Pond 3 (North)

Worksheet for Pond 1 (South) Emergency Spillway

Project Description

| | |
|-----------------|-----------------|
| Friction Method | Manning Formula |
| Solve For | Bottom Width |

Input Data

| | |
|-----------------------|------------|
| Roughness Coefficient | 0.030 |
| Channel Slope | 1.000 % |
| Normal Depth | 6.00 in |
| Left Side Slope | 3.000 H:V |
| Right Side Slope | 3.000 H:V |
| Discharge | 522.00 cfs |

**PEAK 100 YEAR
INFLOW RATE
417.42 X 1.25**

Results

| | |
|------------------|-----------------------|
| Bottom Width | 334.19 ft |
| Flow Area | 167.8 ft ² |
| Wetted Perimeter | 337.4 ft |
| Hydraulic Radius | 5.97 in |
| Top Width | 337.19 ft |
| Critical Depth | 5.07 in |
| Critical Slope | 1.751 % |
| Velocity | 3.11 ft/s |
| Velocity Head | 0.15 ft |
| Specific Energy | 0.65 ft |
| Froude Number | 0.777 |
| Flow Type | Subcritical |

**PROPOSED BTM
WIDTH = 335'**

GVF Input Data

| | |
|------------------|---------|
| Downstream Depth | 0.00 in |
| Length | 0.0 ft |
| Number Of Steps | 0 |

GVF Output Data

| | |
|---------------------|---------------|
| Upstream Depth | 0.00 in |
| Profile Description | N/A |
| Profile Headloss | 0.00 ft |
| Downstream Velocity | Infinity ft/s |
| Upstream Velocity | Infinity ft/s |
| Normal Depth | 6.00 in |
| Critical Depth | 5.07 in |
| Channel Slope | 1.000 % |
| Critical Slope | 1.751 % |

Appendix G: Outfall Design Calculations

Events for Pond 7P: Wet Pond 1 (South)

| Event | Inflow (cfs) | Primary (cfs) | Elevation (feet) | Storage (cubic-feet) |
|------------------------|-----------------|------------------|---------------------|-------------------------|
| 002yr-0.17hr | 77.32 | 0.39 | 771.78 | 113,442 |
| 002yr-0.25hr | 88.92 | 0.77 | 771.90 | 162,148 |
| 002yr-0.50hr | 85.69 | 1.82 | 772.13 | 258,010 |
| 002yr-01hr | 78.60 | 3.18 | 772.36 | 355,305 |
| 002yr-02hr | 58.33 | 4.55 | 772.58 | 445,939 |
| 002yr-03hr | 45.55 | 5.15 | 772.67 | 485,631 |
| 002yr-06hr | 34.06 | 6.69 | 772.98 | 617,559 |
| 002yr-12hr | 34.96 | 8.05 | 773.33 | 767,301 |
| 002yr-24hr | 34.14 | 9.34 | 773.72 | 936,131 |
| 10 Yr-SCS 24Hr | 279.86 | 16.14 | 774.77 | 1,398,944 |
| 010yr-0.17hr | 126.46 | 1.03 | 771.96 | 188,366 |
| 010yr-0.25hr | 138.07 | 1.87 | 772.14 | 261,651 |
| 010yr-0.50hr | 144.04 | 4.38 | 772.55 | 434,769 |
| 010yr-01hr | 135.22 | 6.70 | 772.99 | 619,134 |
| 010yr-02hr | 99.99 | 8.17 | 773.37 | 781,431 |
| 010yr-03hr | 78.72 | 8.75 | 773.54 | 854,958 |
| 010yr-06hr | 61.73 | 10.28 | 774.04 | 1,076,628 |
| 010yr-12hr | 58.84 | 12.40 | 774.46 | 1,259,880 |
| 010yr-24hr | 51.78 | 16.66 | 774.81 | 1,415,398 |
| 100 Yr-SCS 24Hr | 417.42 | 39.70 | 776.01 | 1,965,830 |
| 100yr-0.17hr | 196.32 | 2.41 | 772.24 | 302,247 |
| 100yr-0.25hr | 213.64 | 4.20 | 772.52 | 422,738 |
| 100yr-0.50hr | 239.91 | 7.71 | 773.24 | 726,810 |
| 100yr-01hr | 229.29 | 10.44 | 774.10 | 1,101,195 |
| 100yr-02hr | 116.08 | 9.21 | 773.68 | 917,961 |
| 100yr-03hr | 142.19 | 19.87 | 775.01 | 1,510,052 |
| 100yr-06hr | 115.13 | 31.45 | 775.63 | 1,792,643 |
| 100yr-12hr | 101.53 | 36.48 | 775.87 | 1,900,220 |
| 100yr-24hr | 78.02 | 37.62 | 775.92 | 1,923,656 |
| WQV-0.17hr | 196.32 | 2.41 | 772.24 | 302,247 |
| WQV-0.25hr | 157.47 | 2.41 | 772.24 | 302,183 |
| WQV-0.50hr | 100.39 | 2.41 | 772.23 | 302,144 |
| WQV-01hr | 66.63 | 2.41 | 772.23 | 302,028 |
| WQV-02hr | 39.18 | 2.40 | 772.23 | 301,717 |
| WQV-03hr | 27.85 | 2.40 | 772.23 | 301,259 |
| WQV-06hr | 15.45 | 2.37 | 772.23 | 299,122 |
| WQV-12hr | 11.85 | 2.31 | 772.22 | 294,684 |
| WQV-24hr | 9.71 | 2.24 | 772.21 | 289,690 |

**PEAK ELEVATION
WITH OFFSITE**

Worksheet for OCS Outfall Pipe

Project Description

| | |
|-----------------|--------------------|
| Friction Method | Manning Formula |
| Solve For | Channel Slope |

Input Data

| | |
|-----------------------|-----------|
| Roughness Coefficient | 0.013 |
| Normal Depth | 36.00 in |
| Diameter | 36.0 in |
| Discharge | 39.70 cfs |

Results

| | |
|-------------------|---------------------|
| Channel Slope | 0.354 % |
| Flow Area | 7.1 ft ² |
| Wetted Perimeter | 9.4 ft |
| Hydraulic Radius | 9.00 in |
| Top Width | 0.00 ft |
| Critical Depth | 24.62 in |
| Percent Full | 100.0 % |
| Critical Slope | 0.538 % |
| Velocity | 5.62 ft/s |
| Velocity Head | 0.49 ft |
| Specific Energy | 3.49 ft |
| Froude Number | (N/A) |
| Maximum Discharge | 42.71 cfs |
| Discharge Full | 39.70 cfs |
| Slope Full | 0.354 % |
| Flow Type | Subcritical |

GVF Input Data

| | |
|------------------|---------|
| Downstream Depth | 0.00 in |
| Length | 0.0 ft |
| Number Of Steps | 0 |

GVF Output Data

| | |
|-----------------------------|---------------|
| Upstream Depth | 0.00 in |
| Profile Description | N/A |
| Profile Headloss | 0.00 ft |
| Average End Depth Over Rise | 0.0 % |
| Normal Depth Over Rise | 100.0 % |
| Downstream Velocity | Infinity ft/s |
| Upstream Velocity | Infinity ft/s |
| Normal Depth | 36.00 in |
| Critical Depth | 24.62 in |
| Channel Slope | 0.354 % |
| Critical Slope | 0.538 % |

Appendix H: Stormwater Quality Calculations

Events for Pond 7P: Wet Pond 1 (South)

| Event | Inflow (cfs) | Primary (cfs) | Elevation (feet) | Storage (cubic-feet) |
|-----------------|-----------------|------------------|---------------------|-------------------------|
| 002yr-0.17hr | 77.32 | 0.39 | 771.78 | 113,442 |
| 002yr-0.25hr | 88.92 | 0.77 | 771.89 | 161,109 |
| 002yr-0.50hr | 85.69 | 1.72 | 772.11 | 250,002 |
| 002yr-01hr | 78.60 | 2.90 | 772.32 | 336,246 |
| 002yr-02hr | 58.33 | 4.07 | 772.50 | 414,260 |
| 002yr-03hr | 45.55 | 4.59 | 772.58 | 447,984 |
| 002yr-06hr | 34.06 | 6.08 | 772.84 | 555,948 |
| 002yr-12hr | 33.74 | 7.22 | 773.11 | 672,686 |
| 002yr-24hr | 29.60 | 8.28 | 773.40 | 794,865 |
| 10 Yr-SCS 24Hr | 279.53 | 10.98 | 774.28 | 1,180,737 |
| 010yr-0.17hr | 126.46 | 1.00 | 771.95 | 185,933 |
| 010yr-0.25hr | 138.07 | 1.76 | 772.12 | 253,269 |
| 010yr-0.50hr | 144.04 | 3.92 | 772.48 | 404,325 |
| 010yr-01hr | 135.22 | 6.07 | 772.84 | 555,674 |
| 010yr-02hr | 99.99 | 7.34 | 773.14 | 685,508 |
| 010yr-03hr | 78.72 | 7.85 | 773.28 | 743,624 |
| 010yr-06hr | 61.68 | 9.18 | 773.67 | 913,490 |
| 010yr-12hr | 53.80 | 10.12 | 773.99 | 1,050,769 |
| 010yr-24hr | 42.34 | 10.99 | 774.28 | 1,181,693 |
| 100 Yr-SCS 24Hr | 415.48 | 25.10 | 775.31 | 1,645,819 |
| 100yr-0.17hr | 196.32 | 2.24 | 772.20 | 289,482 |
| 100yr-0.25hr | 213.64 | 3.76 | 772.46 | 394,036 |
| 100yr-0.50hr | 239.91 | 6.92 | 773.04 | 641,299 |
| 100yr-01hr | 229.29 | 9.32 | 773.72 | 932,520 |
| 100yr-02hr | 116.08 | 8.26 | 773.39 | 792,174 |
| 100yr-03hr | 142.19 | 12.79 | 774.50 | 1,277,145 |
| 100yr-06hr | 114.70 | 20.14 | 775.03 | 1,517,581 |
| 100yr-12hr | 87.70 | 23.63 | 775.23 | 1,609,230 |
| 100yr-24hr | 61.05 | 24.05 | 775.26 | 1,619,833 |
| WQV-0.17hr | 196.32 | 2.24 | 772.20 | 289,482 |
| WQV-0.25hr | 157.47 | 2.24 | 772.20 | 289,482 |
| WQV-0.50hr | 100.39 | 2.24 | 772.20 | 289,478 |
| WQV-01hr | 66.63 | 2.24 | 772.20 | 289,452 |
| WQV-02hr | 39.18 | 2.23 | 772.20 | 289,305 |
| WQV-03hr | 27.85 | 2.23 | 772.20 | 289,026 |
| WQV-06hr | 15.35 | 2.21 | 772.20 | 287,409 |
| WQV-12hr | 11.85 | 2.16 | 772.19 | 283,695 |
| WQV-24hr | 9.70 | 2.10 | 772.18 | 279,283 |

WQV Event